

**APPENDIX I**

**NUMERICAL MODEL FOR  
SIMULATION OF GROUNDWATER FLOW AND SULFATE TRANSPORT  
IN THE VICINITY OF THE PHELPS DODGE SIERRITA TAILING IMPOUNDMENT**

**TASK 4 OF AQUIFER CHARACTERIZATION PLAN**

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#### **TASK 4 OF AQUIFER CHARACTERIZATION PLAN MITIGATION ORDER ON CONSENT DOCKET NO P-50-06**

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## **1. INTRODUCTION**

A numerical groundwater flow and sulfate transport model was developed for the region surrounding the Phelps Dodge Sierrita, Inc. (PDSI) Tailing Impoundment (PDSTI) (Figure I.1). The model, referred to as the PDSI Regional-Scale Model (PDSIRM), was developed for Task 4 of the Work Plan (Hydro Geo Chem, Inc. [HGC], 2006) and represents basin fill aquifer conditions in the vicinity of the PDSTU for the period from 1940 to 2006. The model will be used to predict future conditions associated with potential mitigation actions being considered in the Feasibility Study to develop a Mitigation Plan pursuant to the Work Plan. The goals of the PDSIRM are to:

- Calibrate to measured groundwater levels and sulfate distributions within the model domain (1940 to 2006).
- Understand the current groundwater flow and sulfate transport dynamics at different locations near the PDSTI.
- Predict future groundwater levels and sulfate distributions in the vicinity of the PDSTI under various mitigation alternatives.

The PDSIRM is a tool for evaluating potential mitigation alternatives for the sulfate plume, where the sulfate plume is defined by aqueous sulfate concentrations in excess of 250 milligrams per liter (mg/L) that result from seepage from the PDSTI. Any use of the PDSIRM outside of this objective may require additional aquifer characterization and model refinement.

This report describes the model development and calibration. Section 2 discusses model code selection; Section 3 provides details on model construction, including model discretization,

boundary conditions, sources and sinks, and initial model parameterization; Section 4 discusses model calibration for the steady state (1940) and transient (1941 to 2006) simulations; Section 5 discusses the results of a sensitivity analysis; and Section 6 discusses the strengths and limitations of the PDSIRM. Predictive simulations using the PDSIRM will be conducted as part of the Feasibility Study.

## **2. NUMERICAL MODEL SELECTION**

MODFLOW-SURFACT version 3.0 (HydroGeologic, Inc., 1996) is the numerical code used for the PDSIRM groundwater flow and sulfate transport simulations. MODFLOW-SURFACT is based on the widely used United States Geological Survey modeling program, MODFLOW (McDonald and Harbaugh, 1988). The MODFLOW-SURFACT program incorporates several additional modules into the MODFLOW framework that are designed to increase model robustness and improve its ability to simulate complex hydrologic processes. Some advantages of MODFLOW-SURFACT that are particularly beneficial for a three-dimensional model such as the PDSIRM include:

- Improved ability to manage cell wetting and drying using a variably saturated formulation with “pseudo-soil functions”. This feature is essential in a transient, multi-layer model where upper layers may de-saturate, then re-wet, as the result of pumping and recharge.
- Automatic allocation of pumping withdrawals from each layer in wells that are screened over multiple layers. This feature provides for a more correct representation of pumping.
- Automatic and adaptive time-stepping and output control. This feature increases the flexibility and efficiency of the numerical solver by adjusting the solver time stepping based on the complexity of the problem.
- Improved matrix solver. This feature adds efficiency and robustness over the standard MODFLOW solvers.

Sulfate transport was simulated in MODFLOW-SURFACT using the Total Variation Diminishing (TVD) implicit scheme. The TVD scheme constrains the solution domain of a system of partial differential equations so that values of local minima do not decrease and values

of local maxima do not increase with time. This ensures that numerical solutions are physically correct and mass conserving.

Model construction and the execution of the MODFLOW-SURFACT code were performed using Groundwater Vistas, Version 4 (Environmental Simulations, Inc., 2000) software package. Groundwater Vistas provides a visual interface for assembly, execution, and viewing of the MODFLOW family of codes.

### **3. MODEL CONSTRUCTION**

The PDSIRM is designed to simulate the major hydrogeologic processes that influence groundwater flow and sulfate transport in the region of the PDSTI. These include regional groundwater flow, groundwater pumping, natural and artificial recharge, and evapotranspiration. A variety of sources were consulted during model development to quantify these processes. Principal sources of information included the following:

- Reports of previous groundwater flow and transport models in the vicinity of PDSTI (Travers and Mock, 1984; Hanson and Benedict, 1994; Mason and Bota, 2006, Errol L Montgomery and Associates [ELMA], 1994, 2007a).
- Arizona Department of Water Resources (ADWR).
- Water providers in the vicinity of PDSTI (e.g., Community Water Company [CWC], Farmers Investment Company [FICO]).
- Hydrogeologic information collected or compiled by HGC as part of the Aquifer Characterization Plan.
- Hydrogeologic information assembled and/or reevaluated from prior investigations (e.g., ELMA, 1987, 1995, 2007b).
- Information provided by PDSI, including sulfate concentration and groundwater level databases.

All information was synthesized under the context of the site conceptual model, discussed in Section 3 of the main body of the Aquifer Characterization Report (ACR). The conceptual model and the modeling objectives provided the basis for the construction of the PDSIRM, including the spatial and temporal extents; discretization and layering of the model domain; boundary conditions; groundwater and sulfate sources and sinks; and initial aquifer properties.

### **3.1 Spatial and Temporal Extents**

The active portion of the PDSIRM domain covers an area of approximately 100 square miles (260 square kilometers [ $\text{km}^2$ ]) (Figure I.2). The active model region extends from just above West Arivaca Road on the south (Universal Transverse Mercator [UTM] 3510500) to just below Pima Mine Road on the north (UTM 3540000). From the PDSTI this region extends east about 8.5 miles (13.5 km). The area of primary emphasis for the PDSIRM is the area in the vicinity of PDSTI, including the areas surrounding the current extent of the sulfate plume. This area of primary interest is depicted as the rectangle within the lateral model boundaries shown in Figure I.2. The area of primary interest corresponds to other modeling efforts for the PDSTI (e.g., ELMA, 1994, 2007a) and has been the focus of the aquifer characterization conducted as part of the Work Plan. Aquifer characteristics, including hydraulic properties and hydrogeologic units, outside of the area of emphasis are less characterized and, therefore, are less certain. The domain outside of the area of emphasis has less significance to simulation of sulfate plume migration because it is distant from the plume and potential mitigation actions that will be simulated to develop the Mitigation Plan. The aquifer region outside the area of primary emphasis is included in the model to reduce the sensitivity of flow and transport simulations within the area of emphasis on assumed boundary conditions.

The temporal domain of the PDSIRM is divided into three simulation periods: steady-state (1940), historic (1941 – 2007), and predictive (2007 and beyond). The steady-state simulation of the year 1940 establishes initial groundwater levels for the PDSIRM. During and prior to 1940, the Upper Santa Cruz Basin is believed to have been in a state of “dynamic equilibrium” (Mason and Bota, 2006), meaning that groundwater withdrawals matched

groundwater inflows, and water levels had no long-term fluctuations. Groundwater levels from the steady-state simulation were used as the initial heads for a transient simulation of groundwater flow and sulfate transport for the period from 1941 to 2006 (historic simulation). The final heads from the historic simulation will be used as the initial heads for the predictive simulations.

### **3.2 Discretization**

The model domain is discretized into 215 rows, 162 columns, and 3 layers (Figure I.3). Rows are oriented west to east and columns are oriented north to south. Grid cell widths and lengths range from 100 meters [m] to 400 m. The coarsest grid cell spacing occurs in the southern, northern, and eastern positions of the model domain, peripheral to the area of emphasis. The finest grid cell spacing is centered in the area of emphasis surrounding the PDSTI (Figure I.2).

A three-layer model was used to represent the upper, middle, and lower zones of the basin-fill aquifer that were identified during aquifer characterization (ACR, Section 3.2.1). The three model layers are of equal thickness at a given location, with the thickness of each layer varying according to the aquifer thickness at each location. Information collected as part of the Aquifer Characterization Plan shows a coarser-grained, higher permeability zone at intermediate depths in several locations (ACR, Appendices D, E, G, and F). Results of pumping tests at nested wells (ACR, Appendix E) and depth-specific inflow velocity profiling at ESP-2 and ESP-4 wells (ACR, Appendix C) also suggest an intermediate-depth zone of relatively higher

hydraulic conductivities. Layer 2 of the model generally corresponds to what was identified as the intermediate-depth zone during aquifer characterization. The top of the upper model layer (Layer 1) corresponds to the ground surface, and the bottom of the lower layer (Layer 3) corresponds to the bedrock elevation, as estimates during aquifer characterization (Section 3.3.1 and ACR, Appendix A).

### **3.3 Boundary Conditions**

The model has two types of boundary conditions: no flow and specified head and concentration (Figure I.4). No flow cells are inactive grid cells that do not permit groundwater flow or solute transport into, or out of, the cell. Specified head and concentration boundaries are grid cells that are maintained at specified values during a stress period (defined as one year for the PDSIRM) but can vary from one stress period to another.

#### **3.3.1 No Flow Boundaries**

No flow conditions are assigned along the model boundary at locations that represent the outer edges of the basin fill aquifer (Figure I.4) and along the bottom of the lowermost layer, representing the bedrock surface. No flow cells are considered to be outside of the model domain. No flow boundaries specified at the southeastern portion of the domain correspond to the pinching out of the aquifer against the Santa Rita Mountains; those specified at the western edge of the model domain correspond to the pinching out of the aquifer against the Sierrita Mountains. The no flow cells on the western edge of the model also included the pit areas of the

Asarco Mission Mine and the Twin Buttes Mine which are mainly located in bedrock and which are not of primary interest for this modeling effort. Although the Twin Buttes Mine pit area was not included in the active model domain, groundwater flow into the Twin Buttes Mine pit was accounted for by specifying a constant negative groundwater flux in active cells immediately adjacent to the Twin Buttes Mine pit (Section 3.4.3).

The no-flow boundary representing the aquifer bedrock surface was created from the bedrock elevation database that was developed as part of the Aquifer Characterization Plan (ACR, Appendix A). This database includes drilling data from boreholes that are located in the southern Tucson basin and that either penetrated bedrock or deep basin fill. Information sources for borehole data were the ADWR 35 and 55 imaged records databases, the PDSI well database, PDSI borehole data, and a report by Steffen, Robertson, and Kirsten [SRK] (1985b). Bedrock elevation data were translated into a bedrock surface grid using the software package Surfer®. For the purpose of model stability, the total thickness of each layer of the PDSIRM was kept to a minimum of 30 meters (98 feet). This stipulation required depressing the estimated bedrock elevation along portions of the model boundaries; however, it did not affect the estimated bedrock elevations under the IW wellfield.

### 3.3.2 Specified Head and Concentration Boundaries

Specified head and concentration boundaries are located along the south, north, and eastern boundaries of the model (Figure I.4). These boundaries occur within, rather than at the margins of, the basin-fill aquifer. Very little groundwater level data exists along these domain

boundaries. Therefore, for the period from 1940 to 1999, the values of the specified heads were initially based on a regional groundwater flow model constructed by Mason and Bota (2006) (referred to hereafter as the ADWR model). Although the ADWR model heads are simulated rather than measured, they provide a reasonable starting point for the calibration of the specified head values because they are based on a large-scale, calibrated, model of the Tucson Basin.

The initial specified boundary heads were created by digitizing the AWDR model results from each stress period (1940 to 1999). Because the ADWR model uses 0.5 mile (approximately 805 meter) grid spacing, boundary heads between the ADWR grid cells were interpolated. For the period from 2000 to 2006, specified boundary heads along the north boundary were projected from groundwater level measurements made during the first and third quarters of 2007 and from the hydraulic gradients inferred from those measurements (ACR, Appendix B). The values of the specified boundary heads were adjusted during model calibration to better match historic groundwater levels measured near the specified head boundary locations.

Sulfate concentrations are also prescribed along the specified head boundaries. The specified concentration boundaries conditions prescribe the sulfate concentration for groundwater flowing into the model domain. Any prescribed concentrations at outflow boundaries are ignored, and concentrations at outflow cells are determined by the code. The boundary concentrations were estimated using data from recent water quality sampling events (ACR, Appendix B). Sulfate concentrations ranging from three to 100 mg/L are specified along the southern boundary, with the highest concentrations along the Santa Cruz River channel, and the lowest concentrations near the western mountain front. A sulfate concentration of 30 mg/L is

specified along the eastern boundary, and a concentration 75 mg/L is specified along the northern boundary. A water quality survey conducted in the early 1980s by the Pima Association of Governments shows a similar spatial distribution of sulfate concentrations (PAG, 1983); therefore, the specified boundary concentrations are constant during the simulation.

### **3.4 Groundwater Sources and Sinks**

Sources of groundwater in the PDSIRM domain are mountain front recharge, river and agricultural recharge, seepage from tailing impoundments, and artificial recharge. Groundwater sinks include pumping wells, evapotranspiration (ET), and the Twin Buttes mine pit. All sources and sinks were modeled as transient processes, meaning that values of a specified source or sink could change throughout the simulation. MODFLOW-SURFACT uses the stress period concept for transient simulations. All processes are constant during a user-specified stress period, but can change step-wise between stress periods. The constant stress period time in the PDSIRM is one year. Sources or sinks are modeled using annual averages. Figures I.5 and I.6 show the spatial distribution of recharge sources for two representative years, 1980 and 2006, respectively.

#### **3.4.1 Mountain Front Recharge**

Mountain front recharge is the contribution from mountains to the groundwater recharge in the basin fill aquifer, including infiltration from surface sources (i.e. precipitation, streamflow) and subsurface inflow from adjacent bedrock. Mountain front recharge is included along the

western edge of the PDSIRM domain (Sierrita Mountains) and along the southeastern corner of the domain (Santa Rita Mountains). Initial estimates of mountain front recharge were taken from the ADWR model, which is based on recharge estimates from Hanson and Benedict (1994). The ADWR model assumed mountain front recharge to be constant in time. The volumetric recharge rates in the ADWR model corresponding to the southeastern recharge zone in the PDSIRM and the western recharge zones north and south of the PDSTI are 2,100 acre-feet per year (ac-ft/yr) along the southeastern mountain front (Santa Rita Mountains) and 7,900 (ac-ft/yr) along the western portion of the domain (Sierrita Mountains) (Table I.1). These volumetric rates are equivalent to approximately 200 gallons per minute per mile (gpm/mi). The mountain front recharge is uniformly distributed as areal recharge rates (volume/area/time) to the grid cells in Layer 1 (uppermost model layer) that are immediately inside the no flow boundary cells along the respective west and southeast fronts. A mass balance for the simulated mountain front recharge was computed to verify that the sum of the areal rates totaled the volumetric rates applied in the ADWR model.

Spatially uniform mountain front recharge rates are unlikely along the entire range of the Sierrita Mountains. The pits at the Twin Buttes and PDSI mines likely capture some mountain front recharge. Farther south, the Demetrie Wash, which runs southeast from the PDSI mill area across the southwest side of the PDSTI, likely provides greater recharge rates near the area of PDSTI than the uniform rates based on the estimates of Hanson and Benedict (1994). Little information is available to quantify the capture in the Twin Buttes pit or the contribution from the Demetrie Wash; however, consideration of these features was used to guide model calibration. For example, mountain front recharge was removed along the mountain front

adjacent to and to the north of Twin Buttes Mine and was increased in the proximity of Demetrie Wash (Section 4.4 and Table I.1).

### 3.4.2 River and Agricultural Recharge

River recharge is defined as infiltration from the Santa Cruz River that replenishes the basin-fill aquifer, and agricultural recharge is defined as water that is applied to crops in excess of consumptive use and evaporation demand. The rates and spatial distribution of river and agricultural recharge in the PDSIRM were taken from the ADWR model. River recharge in the ADWR model is based on reports by Gallagher (1979), Keith (1981), and Webb and Betancourt (1990) as compiled in Hanson and Benedict (1994). Agricultural recharge in the ADWR model was estimated as the product of the total volume of water used for irrigation and an irrigation inefficiency coefficient. Mason and Bota (2006) determined the spatial distribution of agricultural recharge from a number of sources, including the location of irrigation grandfathered rights and crop survey data. The ADWR model lumps the rates for river recharge and agricultural recharge because agricultural land use is centered along the Santa Cruz River. Therefore, these two sources of inflow are not distinguished from each other.

Annual river and agricultural recharge in the ADWR model increases during the period from 1940 to 1960 from about 15,000 acre-feet (ac-ft) to about 30,000 ac-ft. The increase in recharge rates generally corresponds to a decline in groundwater levels due to pumping. After 1960, annual river and agricultural recharge gradually decreases to between about 15,000 and 20,000 ac-ft/yr. The decrease is reflective of increased irrigation efficiency and urbanization of

farmland (Mason and Bota, 2006). River and agricultural recharge from the ADWR model was apportioned in the PDSIRM by rediscretizing the spatial distribution of recharge in the ADWR model to match the finer grid cell spacing in the PDSIRM. The refined distribution for each stress period was then imported into the PDSIRM. The extents of recharge are much wider than the channel widths of the Santa Cruz River (Figures I.5 and I.6). The wide extent accounts for the agricultural recharge component.

The ADWR model runs only through 1999. The value of river and agricultural recharge in the PDSIRM after 1999 was set at about 15,400 ac-ft/yr, which is near the recharge volumes in the mid-1990's. A comparison of the ADWR model annual recharge volumes and the recharge volumes used in the calibrated PDSIRM is shown in Figure I.7.

### 3.4.3 Seepage from Tailing Impoundments

Recharge due to seepage from tailing impoundments is included for the PDSTI, Esperanza Tailing Impoundment (ETI), and the Twin Buttes Tailing Impoundment (TBTI) (Figures I.5 and I.6). Seepage from Asarco Mission Mine Tailing Impoundments 7 and 8, for which estimates were not readily available, was not included in the model. Because these impoundments are adjacent to the northern model boundary, the affects of seepage from these impoundments were assumed to be accounted for in the adjacent specified head boundary to the north.

### *3.4.3.1 Phelps Dodge Sierrita Tailing Impoundment*

PDSTI has been in operation since 1970 (Reed & Associates, 1986). Initial seepage rates for the PDSTI were taken from a water budget study conducted for the PDSTI (ELMA, 2007b). The water budget estimates the historical hydraulic loading to, and seepage from, the PDSTI using PDSI milling and slurry composition data; yearly satellite images of tailing impoundment extent and wetness; on-site pan evaporation correlated with pan evaporation estimates from nearby weather stations (to extend the period of record); historical climatological data; and moisture retention characteristics measured from soil cores taken at PDSTI. The estimated seepage rates, reported in Table I.2 and Figure I.8, show initially high seepage rates (about 10,000 ac-ft/yr) that gradually decrease through the late 1980s and then increase again in the early 1990s. The total estimated seepage volume through 2006 is 252,406 ac-ft, with the highest estimated seepage rate (11,507 ac-ft/yr) in 1972, and the lowest seepage rate (2,241 ac-ft/yr) in 1988. Adjustments to the seepage rate estimates were allowed during model calibration, and seepage rates in the calibrated model were about 30 to 35 percent higher than the estimates in ELMA (2007b) (Section 4.4, Table I.2). The need to increase the estimated PDSTI seepage rates for calibration does not necessarily indicate that seepage is higher, but that flow beneath the PDSTI from all the water sources needed to be increased to calibrate to measured groundwater levels and sulfate concentrations. Uncertainties in several hydrologic parameters and processes may have contributed to the need to increase the PDSTI seepage rates in the calibrated model. These parameters and processes may include mountain front recharge, bedrock underflow, aquifer and/or bedrock permeability's, and seepage from the PDSTI and ETI.

The modeled areal extent of seepage from the PDSTI increases with time, consistent with the growth of the PDSTI as shown in images used in the development of the water budget for the PDSTI (ELMA, 2007b). These images indicate that the seepage area in the early stages of PDSTI development was concentrated toward the southeastern portion of the present-day impoundment, and gradually grew to encompass the full north-south extent of the PDSTI. The tailings construction and drainage is represented in the model by gradually increasing the recharge area of the PDSTI with time, with recharge focused on the lower half of the impoundment during the 1970's and early 1980's. After 1985, the majority of the present-day impoundment was developed, and the modeled recharge area of the PDSTI is constant after 1985. Based on the analysis of tailing samples taken from the PDSTI (ELMA, 2007b), the physical and hydrologic properties of the tailing material at the PDSTI have no substantial spatial variations. Therefore, recharge rates for the PDSTI recharge areas are spatially uniform in the model.

PDSI data show that sulfate concentrations in samples collected from the PDSTI reclaim pond between 1980 and 2006 range from less than 1600 mg/L to as high as about 2,800 mg/L, with an average concentration of 1,956 mg/L (ELMA, 2007b). The upper concentration of sulfate in seepage is limited by its solubility, which can vary over a wide range depending on the factors such as the water temperature and other ions present in the groundwater (Snoeyink and Jenkins, 1980; Hendry et al., 1986). Nevertheless, the average sulfate concentration in the samples from the reclaim pond provides a reasonable starting estimate of the average sulfate concentration in the PDSTI seepage. The sulfate concentrations measured from samples taken from the reclaim pond have no apparent trend with time, and a constant concentration of

1,956 mg/L was specified in the PDSTI seepage water. Adjustments of this parameter were allowed during model calibration; although, a concentration of 1,956 mg/L is used in the calibrated model (Table I.1).

#### *3.4.3.2 Esperanza Tailing Impoundment*

The ETI was in operation from 1959 to 1981. High and low estimates for seepage from the ETI were estimated using a water budget methodology similar to that used for the PDSTI (ELMA, 2007c). The high and low values account for uncertainties in evaporation estimates. The calibrated model uses the high seepage estimates. These seepage volumes range from about 2,200 ac-ft/yr to about 1,000 ac-ft/yr. No water was delivered to the ETI during 1972 and between September, 30, 1977 and February 1, 1978 (Reed & Associates, Inc., 1986). Consequently, the water balance shows no seepage for the years 1972 and 1978 (Table I.2, Figure I.8), although some seepage from the ETI probably did occur during these years due to drain-down from the previous years' applications. Drain-down seepage was not estimated in the water budget for the ETI. Therefore, the water allocation for the 1971 to 1972 and 1977 to 1978 will have some inaccuracies; although, the total water applied and total seepage over these periods balances the water budget. Any inaccuracies in the timing of water allocation during the two years do not impact the model results (Section 5).

The model recharge area for the ETI is 250 acres and is assumed to be constant with time. The ETI recharge area is positioned in the model slightly south of the actual ETI location to account for the appearance of a southeasterly overland drainage pattern that is visible in historic

images and that may have channeled some infiltration to the south of the ETI. No water quality samples from ETI seepage are available, and the concentration of the seepage in ETI is specified to be the same as for the PDSTI.

#### *3.4.3.3 Twin Buttes Tailing Impoundment*

The Twin Buttes Mine operated from 1965 to 1983. Seepage rates from the TBTI are taken from a groundwater flow and transport model of the PDSTI vicinity (ELMA, 1994, 2007a), which was based on estimates given by SRK (1986). These seepage estimates are 4,100 ac-ft/yr from 1970 through 1976, 7,900 ac-ft/yr from 1977 though 1979, 4,720 ac-ft/yr from 1980 through 1982, and 1,360 from 1983 through 1985. The model assumes that no seepage occurs after 1985 (Figure I.8). The seepage area for the TBTI was specified as 1,900 acres and was constant with time. Seepage rates from the TBTI were not adjusted in the calibrated model.

Solute transport from the TBTI was not considered because the focus of the model is the sulfate plume from the PDSTI. Sufficient information was unavailable to provide a reliable calibration of sulfate transport from TBTI.

#### 3.4.4 Artificial Recharge

Artificial recharge in the PDSIRM domain includes infiltration basins operated by Robson-Ranch Quail Creek (RRQC). The RRQC underground storage facility (ADWR facility

number 71-58139.001) includes twelve basins, nine of which are currently in operation (Pima County, 2007). The facility is located directly south of the Green Valley Waste Water Treatment Plant (GVWWTP) and receives effluent from GVWWTP as its source for recharge water (Pima County, 2007). The RRQC facility is permitted to store up to 2,240 acre-feet annually (ADWR, 2006). In 2006, RRQC recharged an estimated 1,619 acre-feet. Recharge rates for years prior to 2006 are based on estimates of annual recharge rates using RRQC recharge reports and population projections (ELMA, 2007a). The modeled recharge rates from the RRQC facility linearly increase from 100 acre-feet in 1970 to 1,619 ac-ft by 2006. These recharge estimates were not adjusted during model calibration.

### 3.4.5 Pumping

Groundwater withdrawal by pumping is the major groundwater sink in the PDSTI region. Pumping information was taken from several sources: the ADWR model, information reported in ELMA (2007a), ADWR databases, well surveys, and local water providers. These sources are explained below, and tables of well locations and pumping volumes used in the model are provided in Appendix I.1.

The AWDR model provides pumping estimates for the entire Tucson AMA during the period from 1940 to 1999. Between 1940 and 1960, few pumping records exist, and the pumping rates for this period are based on power consumption records and crop distribution surveys (Anderson, 1972). Because these pumping estimates are not based on user records, their accuracy is uncertain (Dale Mason, personal communication, August 6, 2007). Between 1960

and 1984 more user records exist; however, many of the pumping rates and locations are still based on the estimates of Anderson (1972) using energy and crop data as well as on estimates made by Travers and Mock (1984). Pumping estimates for the period from 1940 to 1984 are assigned cadastral coordinates, but do not necessarily correspond to individual well locations. Beginning in 1984, all non-exempt well owners (i.e., well owners pumping more than 35 gallons per minute [gpm]) have been required to report annual pumping amounts to ADWR. Therefore estimates of pumping rates and locations are more accurate after 1984.

Pumping information for the period from 1971 to 2003 for PDSI wells and other wells located within the area of emphasis was obtained from pumping files used in a prior model (ELMA, 2007a). These pumping data were developed using ADWR databases, PDSI databases, and pumping rates reported by SRK (1986). Prior to 1979, few records were available, and pumping rates for 1971 to 1978 were estimated from the 1979 pumping rates.

ADWR records that were consulted to obtain pumping information were the Groundwater Site Inventory (GWSI) database, the ADWR 55 Well Registry, and annual pumping reports submitted to ADWR by water rights owners. In these databases, and other sources of pumping records, only the annual total is reported. The average daily pumping rate was estimated by dividing the total pumping amount by the number of days in the year.

Well locations were determined from a variety of sources. Locations for Community Water Company wells were provided by Community Water Company, and locations for wells GV-01 and GV-02 at the GVWWTP were provided by Pima County. Other well locations

within the area of emphasis, except for wells imported from the ADWR model, were determined from surveys conducted in 2007 by AMEC Infrastructure, Inc., or by AZTEC Land Surveying, Inc. Spatial coordinates for wells located on the periphery of the model domain were obtained from the ADWR GWSI database and the 55 Well Registry.

Pumping information from the various sources was incorporated into the PDSIRM as follows:

- For the period from 1940 to 1970, pumping estimates from the ADWR model were applied exclusively. Well locations were converted from ADWR row and column coordinates to equivalent coordinates in the PDSIRM. Because the ADWR model used a 0.5 mile grid spacing, wells could only be located to the nearest 0.5 mile (2640 feet).
- For the period from 1971 to 1983, pumping rates from ELMA (2007a) were applied in the PDSIRM. Locations for the wells were taken from the HGC well location database. For wells not included in ELMA (2007a), locations and pumping rates were taken from the ADWR model, as was done for the period from 1940 to 1960.
- For the period from 1984 to 2006, pumping rates were applied from ELMA (2007a) or from the ADWR database for wells and/or years not included in the ELMA (2007a).

Figure I.9 shows the annual pumping totals for all the wells in the PDSIRM domain using the above pumping data. Pumping increases from about 12,500 ac-ft/yr in 1940 to a maximum of nearly 133,500 ac-ft/yr in 1976. After 1976 pumping totals begin to decrease to between 60,000 ac-ft/yr and 75,000 ac-ft/yr by 1985. Reduced agricultural pumping is the primary reason for the decrease in pumping after the mid 1970s (Mason and Bota, 2006). Pumping rates were not adjusted during model calibration.

MODFLOW-SURFACT can automatically allocate flow from each layer penetrated by a well based on aquifer properties and well screened intervals. For pumping obtained from the ADWR model, no information on screened intervals is available, and these wells are assumed to be fully screened over all three layers. Information on screened-intervals is taken from ELMA (2007a) for the wells included in that model. For all other wells, well-construction data is taken from the ADWR 55 Well Registry. Some of the registry records contained detailed well construction information, while other records provided few details other than the total well depth. If screened intervals were not given in the image records, the screened interval is assumed to equal the total depth of well penetration into the aquifer.

### 3.4.6 Evapotranspiration

ET estimates are taken from the ADWR model, which are based on the rates and spatial distribution of Hanson and Benedict (1994). The spatial distribution of the ET zones in the AWDR model was digitized and imported into the PDSIRM. These ET zones are located near the Santa Cruz River. The potential ET rates range from 0.0023 ft/d to 0.03 ft/d with a uniform extinction depth of 25 ft. The potential ET rate is constant throughout the simulation period; although, the actual ET rate decreased with time due to the decline in groundwater levels. ET rates were not adjusted during model calibration.

### **3.4.7 Twin Buttes Pit**

The Twin Buttes Mine pit is not expected to have a major influence on the hydraulics of the basin-fill aquifer, although it may function as a weak groundwater sink (SRK, 1985a). A constant inflow of approximately 250 gpm is estimated to enter the east face of the pit at the intersection of the bedrock and the basin fill (Harold Metz [Twin Buttes Properties, Inc.], personal communication with Ned Hall [PDSI], November 16, 2007). This observation suggests that the pit does act as a sink for groundwater from the basin fill aquifer. The influence of the Twin Buttes pit is represented in the PDSIRM by including a constant negative groundwater flux at the west model boundary near the area of the pit with a total outflow rate of approximately 250 gpm.

## **3.5 Initial Aquifer Parameterization**

Aquifer parameters include saturated hydraulic conductivity, storage coefficient, specific yield, effective porosity, and dispersivity. Initial estimates of these parameters, with the exception of dispersivity, were based on the calibrated parameters in the ADWR model and field measurements or data evaluations made as part of the Aquifer Characterization Plan. Dispersivity was estimated by model calibration. Initial and final aquifer parameters and ranges are summarized in Table I.1.

### 3.5.1 Saturated Hydraulic Conductivity

The saturated hydraulic conductivity ( $K_{sat}$ ) describes the rate at which groundwater can flow under a given hydraulic gradient. Within the area of emphasis, the initial estimates of  $K_{sat}$  were based on information collected during the Aquifer Characterization Plan, including lithologic logs from drilling activities, pumping tests, and depth-specific sampling and inflow profiling. In addition to pumping tests conducted as part of the Aquifer Characterization Plan, hydraulic properties data for previous pumping and slug tests were compiled and evaluated (ACR, Appendix A and E). These previous tests were conducted in the IW, BW, PZ, MH, Duval, FICO, and GV wells. The evaluation of the pumping tests show a wide range in horizontal  $K_{sat}$  values, from less than 1 ft/d to over 100 ft/d. Estimated horizontal  $K_{sat}$  values were relatively higher (approximately 30 to 118 ft/d) in the area northeast of PDSTI (wells MO-2007-1, MO-2007-2, M-25, MH-26, and CW-7); whereas estimated horizontal  $K_{sat}$  values were relatively low (less than 1 ft/d) in the deepest wells of the well nests located east of the south half of PDSTI (MH-13, MO-2007-5, MO-2007-6). The drilling activities, pumping tests, and inflow profiling conducted as part of the Aquifer Characterization Plan do provide evidence that the aquifer is more permeable at intermediate depths in the vicinity of Green Valley; however, the increase in permeability is small (ACR, Appendix E and H). Vertical  $K_{sat}$  values were typically estimated to be less than 1 ft/d in hydraulic tests conducted as part of the Aquifer Characterization Plan (ACR, Appendix E). Initial values of vertical  $K_{sat}$  in the PDSIRM were set at 0.2 ft/d.

In the area outside the focus of the Aquifer Characterization Plan, the initial  $K_{sat}$  values were based on the calibrated  $K_{sat}$  values used in the ADWR model. Although the layer

elevations in the ADWR model do not coincide with those of the PDSIRM the differences in layer thicknesses were neglected for the estimate of initial Ksat values. The calibrated Ksat values from the ADWR model are vertically stratified, with the highest Ksat values in the upper layer (Layer 1) and the lowest values in lowest layer (Layer 3). Because only a transmissivity is specified for Layer 3 of the ADWR model, an equivalent Ksat was calculated based on the bedrock in the PDSIRM and the top of the Layer 3 in the ADWR model. Ksat values in the ADWR model range from 2 ft/d to about 300 ft/d in Layer 1, 1 ft/d to 139 ft/d in Layer 2, and from less than 1 ft/d to about 15 ft/d in Layer 3. The distribution of ADWR Ksat value was condensed into several representative intervals ranging from 1 ft/d to 50 ft/d (Values greater than 50 ft/d in the ADWR model were typically in isolated areas and were assigned values equal to the adjacent cells.) Vertical Ksat for each of the zones was assigned a value equal to about 10 to 30 percent of the horizontal Ksat value. The resulting Ksat distribution was then rediscretized to match the PSDIRM domain and imported into the PSDIRM. The initial Ksat values and distributions were varied during model calibration to improve the match between simulated and measured groundwater levels (Section 4.4 and Table I.1).

### 3.5.2 Storage Coefficient and Specific Yield

The storage coefficient ( $S$ ) and specific yield ( $S_y$ ) define how changes in hydraulic head affect aquifer storage of groundwater. In particular, the value of  $S_y$  describes the drainability of an unconfined aquifer and is of more importance for the PDSIRM. Initial values for  $S$  and  $S_y$ , are taken from the ADWR model. The value of  $S$  for was uniform at 0.0001. The values for  $S_y$  are spatially variable, ranging from 0.05 to 0.16. During model calibration, the values for  $S_y$

were allowed to vary between 0.02 and 0.22. This range of values for Sy is consistent with the range reported in Fetter (2001). The range of Sy values in the calibrated model was from 0.08 to 0.20. The value of S was not adjusted during model calibration (Table I.1).

### 3.5.3 Effective Porosity

The effective porosity ( $\theta_s$ ) is the fraction of the total pore volume of aquifer matrix through which groundwater actively flows. Therefore, the solute transport velocity is influenced by the effective porosity. The initial value for  $\theta_s$  was 0.25 and was spatially uniform throughout the model domain. Values of  $\theta_s$  were adjusted between 0.2 and 0.3 during model calibration (Table I.1).

### 3.5.4 Dispersivity

Dispersivity ( $\alpha$ ) is a parameter that accounts for hydrodynamic dispersion. As a result of hydrodynamic dispersion, some groundwater travels faster, and some slower, than the average groundwater velocity at a particular location. This causes “spreading” of a solute at the margins of a plume by allowing some solute to travel faster and some slower than the average transport velocity. Values of  $\alpha$  increase with increasing media heterogeneity and have been observed to be “scale-dependent”, generally increasing with solute transport distance (Gelhar, 1993). Evaluation of the sulfate plume morphology, especially for the margins of the plume, based on water quality sampling data for the first and third quarters of 2007 (ACR, Appendix B) indicates very little plume dispersion has occurred. Therefore, with the exception of directly underneath

the PDSTI, the values of longitudinal, transverse, and vertical dispersivity were initially set to zero in the PDSIRM and did not need to be adjusted for calibration. This allows all modeled plume dispersion to be accounted for by the variation in aquifer properties and by any numerical dispersion inherent in the transport solution. Under the PDSTI, the vertical dispersivity is 65 feet, while longitudinal and transverse dispersivities are zero. This high vertical dispersivity beneath the PDSTI is used to facilitate movement of sulfate in the PDSTI recharge to the lower model layers, consistent with the conceptual model of sulfate migration in the PDSTI.

### **3.6 Initial Conditions**

The initial groundwater levels for the transient (1941 to 2006) model were taken from the calibrated steady-state model. Initial sulfate concentrations were specified to follow the trends observed in the 2007 water quality sampling events (ACR, Appendix B): lower concentrations (> 5 mg/L to 30 mg/L) near the basin margin and a higher concentration (80 mg/L) in the middle of the basin, along the Santa Cruz River.



## **4. MODEL CALIBRATION**

Model calibration is the process of adjusting the model input parameters to achieve reasonable matches between simulated groundwater levels and sulfate concentrations with measured values. Model calibration of groundwater levels was first conducted for a steady-state model representing conditions in 1940. Calibration of groundwater levels and sulfate concentrations was then performed for a transient model representing the period from 1941 to 2006. The calibration methodology and calibration results for the steady-state and transient simulations are discussed below.

### **4.1 Calibration Criteria**

During model calibration, input parameters were systematically adjusted to improve the match between measured and simulated groundwater levels and sulfate concentrations. Improvement was judged both quantitatively and qualitatively. The differences between measured and simulated values (referred to as residuals) provided a quantitative evaluation of model calibration at specific “target” locations (i.e. locations were data of measured values existed). For the 1940 steady-state simulation and for the transient simulation for years 1960, and 1983, calibration targets were taken from those used to calibrate the ADWR model. Calibration targets for the years from 1941 through 2005 were taken from the PDSI database, ELMA (2007a), PAG (1983), and ERC (1996). Calibration targets for the end of the year 2006 were taken from groundwater levels measured by HGC for groundwater sampling during the first and third quarters of 2007.

A qualitative assessment of model calibration was conducted by mapping the spatial distribution of residuals and by comparing groundwater level and sulfate concentration contours created from the simulated and from measured values. Mapping residuals helped to detect spatial bias in errors, and the contour maps helped to evaluate how well the simulated groundwater levels and sulfate concentrations compared to field measurements on a large scale.

The historic groundwater levels sometimes showed variations of several feet or more within a given year and from one year to the next. Groundwater levels measured by HGC between first quarter and third quarter, 2007 could also vary several feet between measurements taken at the same location. The intra-annual variations possibly reflect increased pumping during the summer months. Simulation of these intra-annual water level fluctuations was not practical because pumping information could only be obtained as annual totals and because sub-annual stress periods would further increase simulation processing times. Therefore, simulated groundwater levels that were between target values for a given year were taken as a satisfactory match.

## 4.2 Calibration Methodology

Model calibration initially began for the 1940 steady-state simulation. The 1940 simulation had relatively little pumping and few calibration targets compared to the calibration years in the transient simulation. Therefore, many of the stresses and groundwater level measurements that aid in the calibration of aquifer parameters were not present in the steady-state simulation and much of the parameter estimation could only be accomplished during

the calibration of the transient model. Consequently model calibration proceeded iteratively between the steady-state model and the transient model until the most satisfactory solution was reached for both.

### **4.3 Calibration Results**

Both the initial values of parameters and their spatial distributions were varied during model calibration to better match measured groundwater levels and sulfate concentrations. The final calibrated parameter values and ranges are provided in Table I.1. Figures I.10 to I.12 show the spatial distribution of Ksat values in the three model layers, and Figure I.13 shows the spatial distribution of Sy values, which is the same in all layers.

#### 4.3.1 Groundwater Calibration

A good agreement was achieved between measured groundwater levels and the simulated groundwater level contours for the steady-state (1940) calibration (Figure I.14), and no spatial bias is apparent in the residuals between measured and simulated values (Figure I.15). Therefore, the calibrated steady-state model is believed to provide a reasonable initial condition for the transient groundwater flow simulation.

Simulated groundwater level contours are compared with the measured groundwater levels from the first and third quarter 2007 sampling events in Figure I.16 and Figure I.17. Contour maps of measured water level elevations for the final and third quarters of 2007 are in

Appendix B and Figure 5 of the ACR, respectively. The simulated groundwater level contours demonstrate several important features of the potentiometric field estimated from measured groundwater levels, including:

- The steep hydraulic gradient emanating westward from the PDSTI, and the abrupt turn to the north of the flow field immediately downgradient (east) of the PDSTI.
- The curvature of the groundwater contours across the center of the basin.
- The groundwater level trough and flattening of the hydraulic gradient in the northwest portion of the model domain and the groundwater level rise in the northeast portion of the model domain.

Simulated groundwater contours and measured water levels show the greatest differences in the north part of the model domain in the vicinity of the apparent groundwater level trough east of the Twin Buttes Mine. The trough is defined by water levels that dip easterly from the Twin Buttes Mine, westerly from the vicinity of the Santa Cruz River near and north of Duval Mine Road, and northerly from Green Valley. The trough is evident in both the first and third quarter groundwater sampling events and appears to be a persistent feature shown to varying degrees by groundwater level maps for 1966 (Davidson, 1973) and 1982 (PAG, 1983 and Murphy and Hedley, 1984). The trough in water level contours implies a zone of convergent groundwater flow toward the northwest portion of the model domain. The differences between simulated and measured water levels in the northern portion of the model could be due to differences between assumed and actual values for hydraulic properties, groundwater pumping, or recharge. Improved simulation of the groundwater levels in northern model areas would require further aquifer characterization and refinement of the conceptual model beyond the area of emphasis.

Simulated versus measured groundwater levels for all groundwater level targets used in the transient simulation are shown in Figure I.18. Highlighted in the figure are the targets for the 2007 sampling events. A similar comparison is made in Figure I.19 for the area of emphasis (inner rectangle in Figure I.2). Overall, the simulated versus measured points follow the one-to-one line, showing the ability of simulated results to match measured groundwater levels across the entire model domain. The upward deviation from the one-to-one line at the lower groundwater elevations is due to the difficulty in simulating the groundwater level depression in the northwest part of the model domain.

Appendix I.2 includes hydrographs of measured and simulated groundwater levels at several wells (refer to Figure I.2 for well locations). These hydrographs are representative of the calibration at different areas of the model domain and provide the following observations:

- Although measured groundwater levels in the southern part of the model domain show large fluctuations, the simulated results approximate the median behavior and show a particular good match with recent measurements (Appendix I.2, Figures I.2.1 to I.2.4).
- Groundwater level time-series for wells immediately down-gradient of the PDSTI, along the IW-wellfield, show a general agreement between simulated and measured, although the absolute values can differ by several feet (Appendix I.2, Figures I.2.5 to I.2.7). Most discrepancies appear to be caused by the inability of the model to simulate steep hydraulic gradients at sub-grid locations.
- About one mile east of the PDSTI, the simulated results match the average behavior of measured points; however, individual wells can have periods where the simulated results deviate from the measured points (Appendix I.2, Figures I.2.8 to I.2.12). The reasons for the deviations are uncertain, but because the deviations at different wells show no systematic variations, they do not indicate a modeling bias in the area east of the PDSTI.

#### 4.3.2 Sulfate Concentration Calibration

Simulated sulfate concentration contours are compared with measured sulfate concentrations from the third quarter 2007 sampling events in Figure I.20. The third quarter 2007 sampling event is used for comparison even though the model simulation was conducted only through the end of 2006 because the third quarter event provides sulfate concentration measurements at several key locations surrounding the PDSTI that were not obtainable in previous sampling events. The simulated sulfate concentration contours shown in Figure I.20 represent concentrations averaged over the upper and middle layers. These layers represent the primary flow and transport zones near the PDSTI because the permeabilities in these layers are generally higher than in the lowermost layer. The simulated sulfate concentrations in each of the three layers are shown in Figure I.21. In general, the extent of the sulfate plume is greater in the upper layer than in the lowermost layer. Chemographs of the simulated (averaged over the upper two layers) and measured sulfate concentrations at several key locations are provided in Appendix I.3. The data in these chemographs includes measurements through the third quarter of 2007, which is beyond the simulation period. Measurements outside of the simulation period are shown as solid symbols.

The sulfate contours in Figure I.20 and the chemographs in Appendix I.3 illustrate the strengths of the transport model in representing several important features of the plume as inferred from the following water quality measurements:

- The general shape of the sulfate plume is represented, including a broad base near the PDSTI and a thinner leading edge (Figure I.20).
- The arrival time of the plume is accurately simulated at several key locations along the eastern edge of the plume (Appendix I.3, Figures I.3.1 and I.3.2).
- The northward advance of the plume is represented (Appendix I.3, Figures I.3.3 to I.3.4).
- Concentrations in the plume interior are generally well represented (Appendix I.3, Figures I.3.5 to I.3.7).

While the model reproduces the general characteristics of the sulfate plume, it is unable to match measured concentrations at every location. For example, the simulated sulfate distribution does not match the higher sulfate concentrations measured at the deeper wells at MO-2007-5 located at the southeastern portion of the sulfate plume. The simulated plume extends farther to the southeast during earlier years, but contracts after the increase in pumping at the PDSI Interceptor Wellfield during the mid-1990s. The model simulation suggests that the high sulfate concentrations measured in MO-2007-5 may represent residual concentrations from a retreating plume rather than an advancing plume. The model also slightly over predicts the northern extent of the plume as determined by water quality measurements. The over prediction results from the model's difficulty in simulating the sharpness of the sulfate plume at its northern extent, where sulfate concentrations rapidly decrease from about 1,400 mg/L at M-20 to 100 mg/L and less at MO-2007-1. This may lead to a conservative prediction (i.e., earlier arrival of predicted than measured) at the northern extent of the plume.

The inability of the model to match the sharpness of the plume front and concentrations at some point locations is likely due to aquifer heterogeneities that cannot be adequately captured in the model. Because the model cannot incorporate all of the aquifer heterogeneities and

processes that vary at spatial and temporal scales finer than the model discretization, there are practical limits on the model's capability to predict concentrations at point locations and where rates of sources and sinks for groundwater and sulfate can change quickly, such as near the PDSTI (Section 6). However, the calibration results demonstrate that the PDSIRM accurately simulates the key trends and attributes of groundwater flow and sulfate migration, giving confidence that the model can be used as a predictive tool for evaluating mitigation alternatives.

#### **4.4 Adjustments During Model Calibration**

Several adjustments to initial parameters were made during model calibration to achieve better matches between simulated and measured groundwater levels and sulfate concentrations. Table I.1 provides a comparison of initial and final parameters and ranges. The major adjustments that were made during model calibration include the following:

- A higher Ksat zone ( $K_{sat} = 36$  to  $89 \text{ ft/d}$ ) was created in the western portion of the model domain, extending north of PDSTI, and the specified heads along the northern boundary were lowered where the boundary intersects the higher Ksat zone.
- Mountain front recharge along the northwestern portion of the model domain (beginning at approximately the Twin Buttes Mine) was decreased and the mountain front recharge within the area of the PDSTI was increased (Section 3.4.1).
- Seepage rates in the PDSTI were increased approximately 30 to 35 percent from the rates estimated in ELMA (2007b). The need to increase the PDSTI seepage rates does not necessarily indicate that seepage is higher, but that flow beneath the PDSTI from all the water sources needed to be increased for model calibration.

The area east of the Twin Buttes Mine has a persistent zone of depressed groundwater levels, indicative of convergent groundwater flow. The means selected to simulate the depressed groundwater levels was to increase Ksat values in a zone trending north from the Twin Buttes

Mine area to the northern model boundary (Figures I.11 to I.13). The K<sub>sat</sub> values in this zone range from 36 ft/d to 89 ft/d. Although the K<sub>sat</sub> values of the higher K<sub>sat</sub> zone are consistent with measured K<sub>sat</sub> values at several locations north and northeast of the PDSTI (e.g., MO-2007-02, CW-7, MH-26), the northern extent of this zone is unknown. Estimated K<sub>sat</sub> values at some wells in the area do not corroborate (e.g., K<sub>sat</sub> values at many of the Twin Buttes wells range from about 10 to 20 ft/d; ELMA (1987, 1995)). Therefore, establishing the higher K<sub>sat</sub> zone in the model and extending it to the northern model boundary is speculative, but was needed to match water level measurements in the area (PAG, 1983; ACR, Appendix B).

Mountain front recharge was adjusted as a means of lowering groundwater levels in the northwest portion of the model domain and increasing groundwater levels in the southern portion of the model domain. The changes are consistent with hydrologic features. The Twin Buttes pit likely intercepts much of the mountain front recharge in the Twin Buttes area, and mountain front recharge was set to zero after 1970 from about the Twin Buttes area to the north boundary. The Demetrie Wash may increase mountain front recharge in the vicinity of the PDSTI, and mountain front recharge was increased from about 195 ac-ft/yr/mile to about 280 ac-ft/yr/mile for about a four-mile in the general vicinity of the PDSTI.

The increases in the PDSTI seepage rates were necessary to better match groundwater levels and sulfate concentrations. As stated in Section 3.4, the increases may reflect inherent uncertainties in the seepage estimates and/or uncertainties in the model conceptualization and parameterization of other hydraulic properties and processes that contribute to flow beneath the PDSTI.



## **5. SENSITIVITY ANALYSIS**

A sensitivity analysis was conducted for the transient (1941 to 2006) model. The objective of the sensitivity analysis was to understand the relative influence that the calibrated values of model parameters have on the simulation results.

### **5.1 Sensitivity Analysis Procedure**

The sensitivity of the simulation results to changes in the values of model input parameters was evaluated by systematically varying parameter values and comparing the ensuing simulation results with those of the calibrated model. The values of the following parameters were adjusted as part of the sensitivity analysis:

- Saturated hydraulic conductivity (horizontal and vertical)
- Storage Coefficient
- Specific yield and Porosity (varied simultaneously)
- Evapotranspiration
- River Recharge
- Mountain front recharge
- Seepage from the PDSTI (rate and concentration)
- Seepage from the ETI (rate and concentration)

Model sensitivity simulations were performed by varying the values of the parameter being tested while keeping the values of the other parameters constant at their final calibration

values. For the parameter being tested, a simulation was run with the parameter values uniformly increased by 25 percent, followed by a simulation run with the parameter values uniformly decreased by 25 percent. The sensitivity analysis was limited to uniformly adjusting a single input parameter (i.e., multiple parameters were not simultaneously varied and a parameter was adjusted by the same percentage at all locations). For each simulation, the root mean square residual (RMSR) and mean arithmetic residual (MAR) between measured and simulated target values for the first quarter 2007 sampling event were computed and compared with the RMSR and MAR for the final calibration simulation. MAR and RMSR are defined as follows:

$$MAR = \frac{\sum_{i=1}^n (C_i - T_i)}{n} \quad [1]$$

$$RMSR = \sqrt{\frac{\sum_{i=1}^n (C_i - T_i)^2}{n}} \quad [2]$$

Where:

- $C_i$  = residual between the calibrated model simulation and measure values for target i
- $T_i$  = residual between the test simulation and measure values for target i
- $n$  = number of targets

Sensitivity was then evaluated as the arithmetic difference between the MAR ( $\Delta MAR$ ) for the calibration and test simulations, and the relative percent difference in the root mean square error ( $\Delta RMSE$ ) between the two simulations. The value (positive or negative) of  $\Delta MAR$  indicates the average direction that the parameter change moved the groundwater levels

and sulfate concentrations. The value of  $\Delta$ RMSE indicates the average magnitude of that change and provides a relative measure of the least to the most sensitive parameter.

## 5.2 Sensitivity Analysis Results

Table I.3 summarizes the results of the sensitivity analysis. For groundwater levels at the 2007 target locations, the model is most sensitive to changes in Ksat and increases in the seepage rate in the PDSTI. Groundwater levels at target locations are influenced more by decreases in the PDSTI seepage rate than by increases in the seepage rate. Groundwater levels at target locations are moderately influenced by changes in specific yield, river recharge, and mountain front recharge. Changes in the storage coefficient, evapotranspiration, and the seepage rate in the ETI have relatively little influence on groundwater levels at the 2007 target locations.

Sulfate concentrations at the 2007 target locations are most sensitive to increases in the concentration of the seepage in the PDSTI. The sulfate concentrations are also moderately to highly sensitive to increases in the seepage rate in the PDSTI and decreases in the specific yield/porosity because these parameters affect the mass loading of sulfate and/or the rate of the sulfate plume migration. Seepage in the ETI has a modest influence on simulated sulfate concentrations. The sulfate concentrations at the 2007 target locations are less sensitive to changes in other parameters.



## **6. SUMMARY AND CONCLUSIONS**

The results of the model calibration for the historic simulation of groundwater levels and sulfate concentrations show the abilities of the PDSIRM to simulate the groundwater flow and sulfate plume migration within the vicinity of the PDSTI. The simulated groundwater level trends and the overall shape of the simulated groundwater levels are similar to observed trends, indicating the essential components of the aquifer hydraulics are represented. Likewise, the general shape and extents of the simulated sulfate plume matches the observed plume, demonstrating that the factors influencing plume movement are incorporated in the model construction. The time-series data (Appendices I.3) indicate that the model is capable of matching the sulfate concentrations and sulfate plume arrival at key locations.

The calibration results provide confidence in the ability of the PDSIRM to serve as a tool for predicting groundwater flow and sulfate transport in the vicinity of the PDSTI. To appropriately use this tool, however, the strengths and limitations of the model should be understood. For example, although the bulk migration of the sulfate plume is well represented, the time-series data (Appendix I.3) show that the model cannot be expected to perfectly match all measurements at particular locations. This limitation is inherent to numerical models constructed from finite characterization data and that simplify process complexities and spatial/temporal heterogeneities. Some of the strengths and limitations of the PDSIRM are discussed below.

## **6.1 Strengths**

For the purposes of developing alternatives for sulfate plume mitigation down-gradient of PDSTI, this model provides several advantages over other groundwater flow and transport models developed for the region near the PDSTI. These advantages include the following:

- Large spatial extents of the model domain that reduce the influence of boundary conditions within the area of the plume.
- Long temporal extent, beginning in 1940 when the aquifer is considered to be in “dynamic equilibrium”, minimizes the influence of initial aquifer conditions on future simulations.
- Integration of the most comprehensive datasets on aquifer characteristics (e.g., K<sub>sat</sub> values and bedrock elevations).
- Calibration to both groundwater level and sulfate concentration measurements, including measurements taken as part of the Aquifer Characterization Plan.

The strengths of the PDSRIM provide confidence in simulated predictions for groundwater levels and sulfate distributions in the area surrounding PDSTI.

## **6.2 Limitations**

Numerical models are an approximation of reality. As with all numerical models, the applicability and predictive ability of the PDSIRM has limits. These limitations should be understood when using the PDSIRM. Important limitations of the PDSIRM include: spatial and temporal uncertainty and spatial and temporal averaging.

### 6.2.1 Spatial and Temporal Uncertainty

Information on aquifer characteristics and groundwater levels used for conceptual model development and model calibration decreases away from the area of emphasis. The specified-head boundaries at the north, east, and south of the model are supported by relatively few measurements. Measurements of aquifer properties and hydrogeologic units are also sparse near the model boundaries, and projection of layer elevations outside the area of emphasis is uncertain. Consequently, the confidence in model predictions decreases away from the area of emphasis, the area immediately downgradient of the PDSTI.

The model's predictive ability farther forward in time will be partly dependent on the accuracy of projected sources and sinks. Forecasts of aquifer stresses such as pumping and recharge rates and their spatial distributions can be uncertain the farther they are projected, and differences between the forecast and actual conditions can lead to inaccuracies in model predictions.

### 6.2.2 Spatial and Temporal Averaging

All finite-difference and finite-element codes discretize heterogeneous and continuous processes and parameters into blocks (or nodes) of constant values. For aquifer systems of relatively uniform properties and for finely discretized models, the effect of discretization will be minimal. For heterogeneous systems with time-variable processes (pumping, river and agricultural recharge, artificial recharge, etc.), model predictions will be increasingly unable to match point-scale values even though they may satisfactorily represent average behavior. The

discrepancies between point measured values and the model block averages may be important in areas of steep gradients, such as across the PDSI Interceptor Wellfield and at the margin of the plume.

The model also averages continuously changing or episodic temporal processes into discrete constant-in-time values. Such processes included seasonal river recharge and pumping that are simulated as average daily values based on a yearly total. Closely matching groundwater levels may be difficult due to temporal averaging, although simulated values should be within, or near, the range of measured values for a given simulation time period (one year for the PDSIRM).

### **6.3 Conclusion**

The PDSIRM is capable of meeting objectives identified in the Work Plan (HGC, 2006). It is calibrated to measured groundwater levels and sulfate distributions, and, when appropriately used, the PDSIRM can be an effective tool to evaluate future groundwater flow and sulfate transport in the vicinity of the PDSTI, and predict the effects of various mitigation actions to be considered in the Feasibility Study.

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## **TABLES**

**TABLE I.1**  
**Initial and Calibrated Model Parameters**

| Parameter or Process                               | Unit                             | Initial Value or Range | Final Value or Range | Sources for Initial Values                  |
|--|----------------------------------|------------------------|----------------------|---|
| Horizontal Saturated Hydraulic Conductivity (Ksat) | ft/d                             | 1.0 - 50               | 1.3 - 89             | Mason and Bota (2006), ACR, Appendices A, E |
| Vertical Ksat                                      | ft/d                             | 0.2 - 3.0              | 0.2 - 4.1            | ACR, Appendices E                           |
| Storage Coefficient (S)                            | ft/ft                            | 0.0001                 | 0.0001               | Mason and Bota (2006)                       |
| Specific Yield (Sy)                                | ft/ft                            | 0.1                    | 0.08 - 0.20          | Fetter (2001)                               |
| Effective Porosity ( $\theta_{se}$ )               | ft <sup>3</sup> /ft <sup>3</sup> | 0.25                   | 0.20 - 0.30          | Fetter (2001)                               |
| Dispersivity, $\alpha_L$ , $\alpha_T$ , $\alpha_V$ | ft                               | 0, 0, 0                | 0, 0, 0 - 65         | ACR, Appendix B, model calibration          |
| Total River + Agricultural Recharge                | ac-ft/yr                         | 14,400 - 29,900        | 14,600 - 37,600      | Mason and Bota (2006)                       |
| Western Mountain Front Recharge                    | ac-ft/yr                         | 7,900                  | 7,700                | Mason and Bota (2006)                       |
| Southeastern Mountain Front Recharge               | ac-ft/yr                         | 2,100                  | 2,600                | Mason and Bota (2006)                       |
| Concentration in PDSTI Seepage                     | mg/L                             | 1,956                  | 1,956                | ELMA (2007b)                                |

Notes:

ft/d = feet per day

ft/ft = feet per feet

ft<sup>3</sup>/ft<sup>3</sup> = cubic feet per cubic feet

ac-ft/yr = acre-feet per year

mg/L = milligrams per liter

**TABLE I.2**  
**Seepage Estimates for Tailing Impoundments**

| YEAR         | SEEPAGE (ac-ft/yr)                           |   |
|--------------|--|---|
|              | Sierrita Tailing<br>Impoundment <sup>a</sup> | Esperanza Tailing<br>Impoundment <sup>b</sup> |
| 1959         | ---  | 1,735   |
| 1960         | ---  | 2,312   |
| 1961         | ---  | 1,920   |
| 1962         | ---  | 1,906   |
| 1963         | ---  | 1,817   |
| 1964         | ---  | 1,548   |
| 1965         | ---  | 1,481   |
| 1966         | ---  | 1,639   |
| 1967         | ---  | 2,190   |
| 1968         | ---  | 2,155   |
| 1969         | ---  | 2,013   |
| 1970         | ---  | 1,738   |
| 1971         | 9,389  | 1,499   |
| 1972         | 11,507                                       | 0   |
| 1973         | 10,470                                       | 1,363   |
| 1974         | 9,388  | 2,556   |
| 1975         | 7,873  | 1,542   |
| 1976         | 9,114  | 1,457   |
| 1977         | 8,823  | 1,009   |
| 1978         | 10,664                                       | 0   |
| 1979         | 5,852  | 1,422   |
| 1980         | 6,149  | 2,273   |
| 1981         | 7,095  | 2,720   |
| 1982         | 2,482  | ---   |
| 1983         | 6,599  | ---   |
| 1984         | 5,131  | ---   |
| 1985         | 6,051  | ---   |
| 1986         | 2,508  | ---   |
| 1987         | 2,498  | ---   |
| 1988         | 2,241  | ---   |
| 1989         | 3,341  | ---   |
| 1990         | 10,664                                       | ---   |
| 1991         | 10,507                                       | ---   |
| 1992         | 9,271  | ---   |
| 1993         | 9,987  | ---   |
| 1994         | 7,587  | ---   |
| 1995         | 6,601  | ---   |
| 1996         | 5,327  | ---   |
| 1997         | 5,119  | ---   |
| 1998         | 6,072  | ---   |
| 1999         | 7,893  | ---   |
| 2000         | 9,356  | ---   |
| 2001         | 10,024                                       | ---   |
| 2002         | 2,859  | ---   |
| 2003         | 6,065  | ---   |
| 2004         | 4,655  | ---   |
| 2005         | 5,777  | ---   |
| 2006         | 7,467  | ---   |
| <b>Total</b> | <b>252,406</b>                               | <b>38,294</b>                                 |

Notes:

<sup>a</sup> Errol L. Montgomery & Associates [ELMA] (2007b)

<sup>b</sup> High seepage estimates from ELMA (2007c)

ac-ft/yr = acre-feet per year

**TABLE I.3**  
**Results of Sensitivity Analysis**

| Parameter                         | Parameter Adjustment | Groundwater Levels |           | Sulfate Concentration |           |
|-----------------------------------|----------------------|--------------------|-----------|-----------------------|-----------|
|                                   |                      | ΔMAR (ft)          | ΔRMSR (%) | ΔMAR (mg/L)           | ΔRMSR (%) |
| Horizontal Hydraulic Conductivity | + 25                 | -9.60              | 10.6%     | -11.7                 | 2.92%     |
|                                   | - 25                 | 13.1               | 13.4%     | 19.2                  | 2.92%     |
| Vertical Hydraulic Conductivity   | + 25                 | 0.15               | 0.08%     | 1.89                  | 0.31%     |
|                                   | - 25                 | -0.04              | -0.08%    | -3.08                 | -0.16%    |
| Storage Coefficient               | + 25                 | -0.01              | -0.01%    | 0.01                  | 0.00%     |
|                                   | - 25                 | 0.01               | 0.01%     | 0.00                  | 0.00%     |
| Specific Yield/Porosity           | + 25                 | -5.33              | 0.18%     | 64.1                  | -0.76%    |
|                                   | - 25                 | 4.83               | 5.18%     | -68.6                 | 13.2%     |
| Evapotranspiration                | + 25                 | 0.00               | 0.00%     | -0.03                 | 0.01%     |
|                                   | - 25                 | -0.04              | -0.05%    | 0.03                  | 0.0%      |
| River Recharge                    | + 25                 | -4.12              | 2.08%     | 2.63                  | -0.25%    |
|                                   | - 25                 | 6.46               | 4.15%     | -5.21                 | 4.15%     |
| Mountain Front Recharge           | + 25                 | -5.54              | 3.23%     | 5.03                  | -1.60%    |
|                                   | - 25                 | -5.55              | 3.23%     | 5.02                  | -1.60%    |
| PDSTI Seepage Rate                | + 25                 | -9.29              | 1.31%     | -49.1                 | 10.7%     |
|                                   | - 25                 | 9.15               | 18.6%     | 56.9                  | 0.53%     |
| Concentration in PDSTI Seepage    | + 25                 | 0.00               | 0.00      | -80.4                 | 41.2%     |
|                                   | - 25                 | 0.00               | 0.00      | 80.3                  | -4.72%    |
| ETI Seepage Rate                  | + 25                 | -0.33              | -0.08%    | -7.85                 | 3.36%     |
|                                   | - 25                 | 0.39               | 0.12%     | 7.93                  | -3.26%    |
| Concentration in ETI Seepage      | + 25                 | 0.00               | 0.00%     | 61.0                  | 7.96%     |
|                                   | - 25                 | 0.00               | 0.00%     | 9.33                  | -4.84%    |

Notes:

ΔMAR = Change in Mean Arithmetic Error between calibrated model and sensitivity simulation

ΔRMSR = Change in Root Mean Square Error between calibrated model and sensitivity simulation

PDSTI = Phelps Dodge Sierrita Tailing Impoundment

ETI = Esperanza Tailing Impoundment

ft = feet

mg/L = milligrams per liter

% = percent

## **FIGURES**

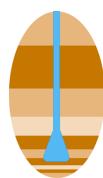
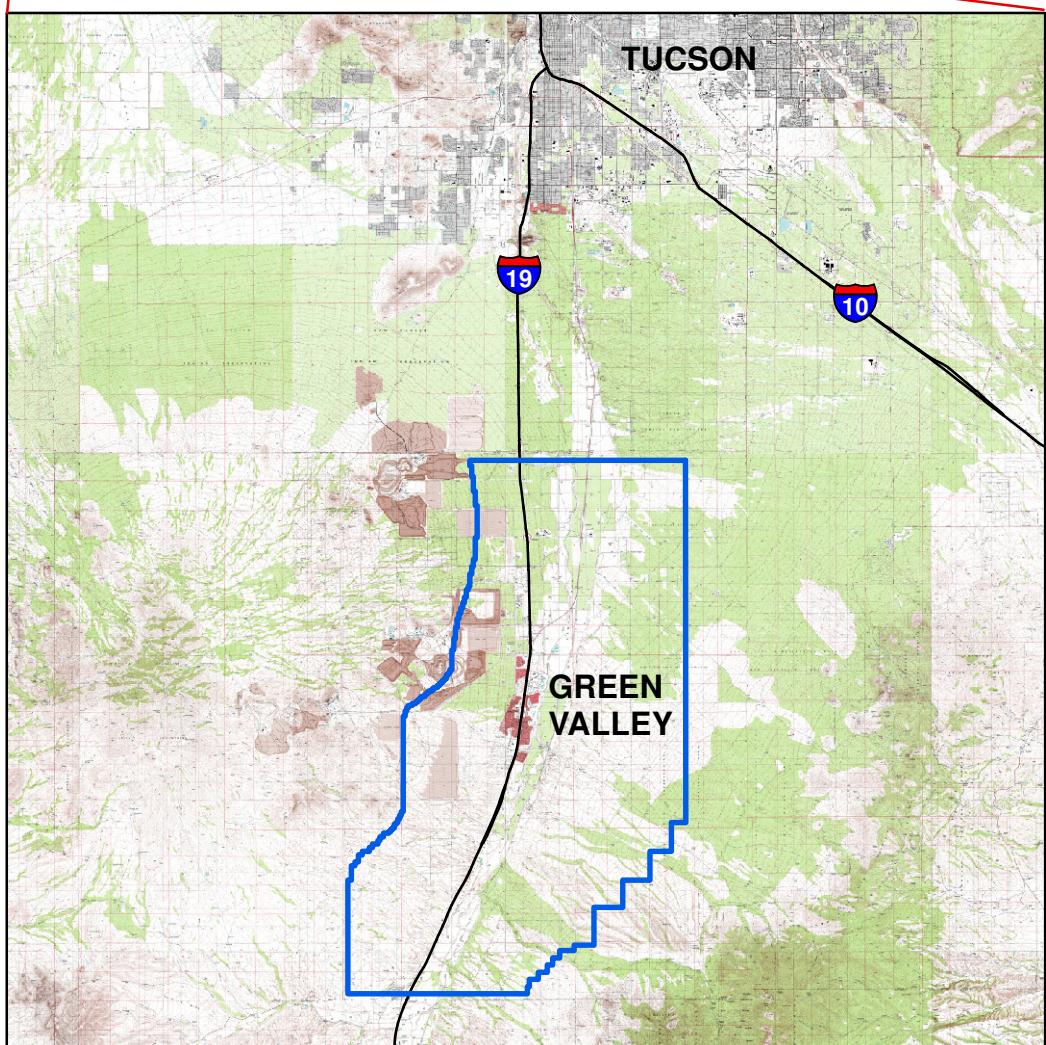


N

1 inch equals 35,000 feet

0 2 4 6 8 10 Miles

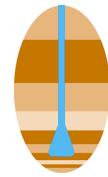
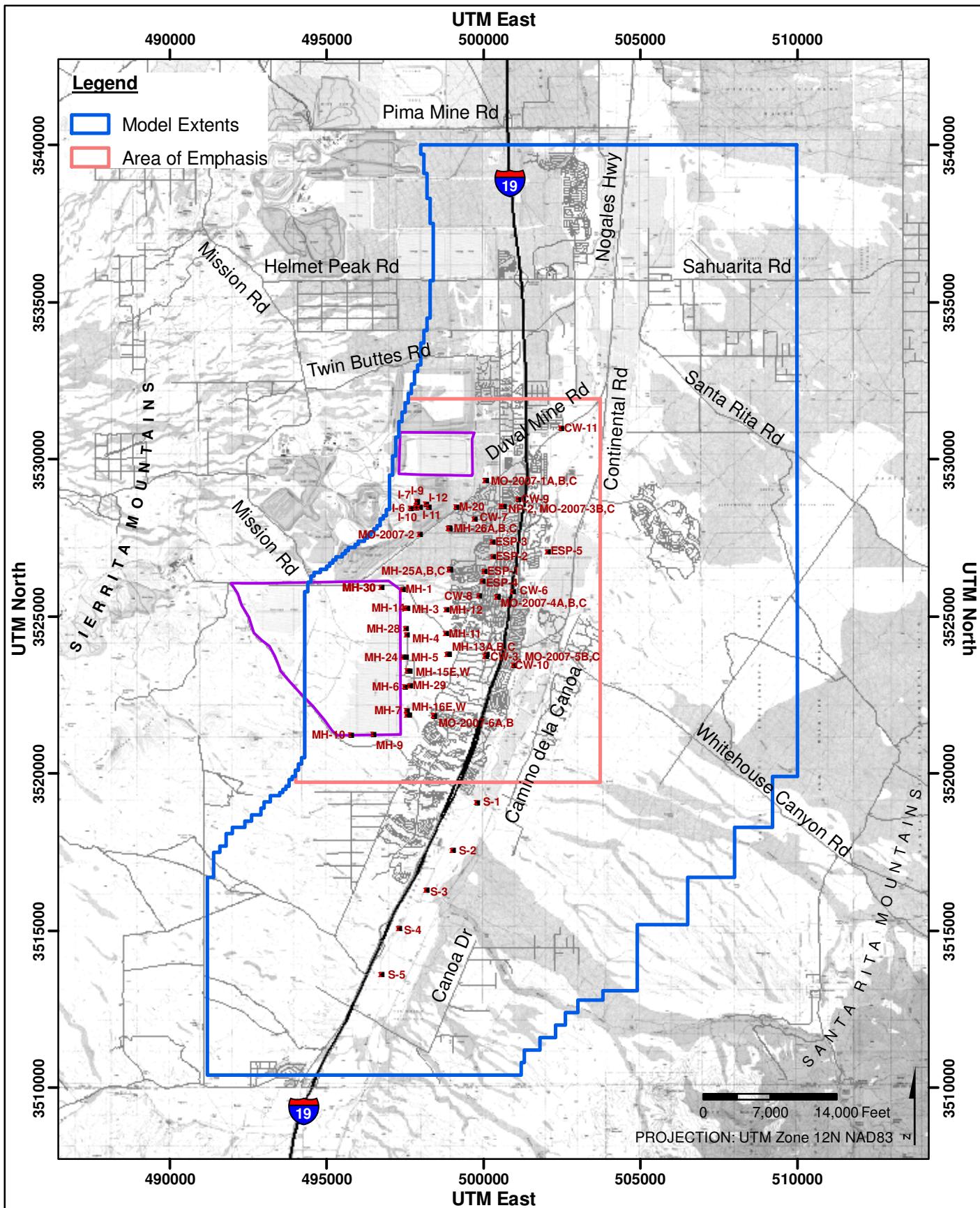
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#### SITE LOCATION

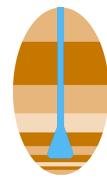
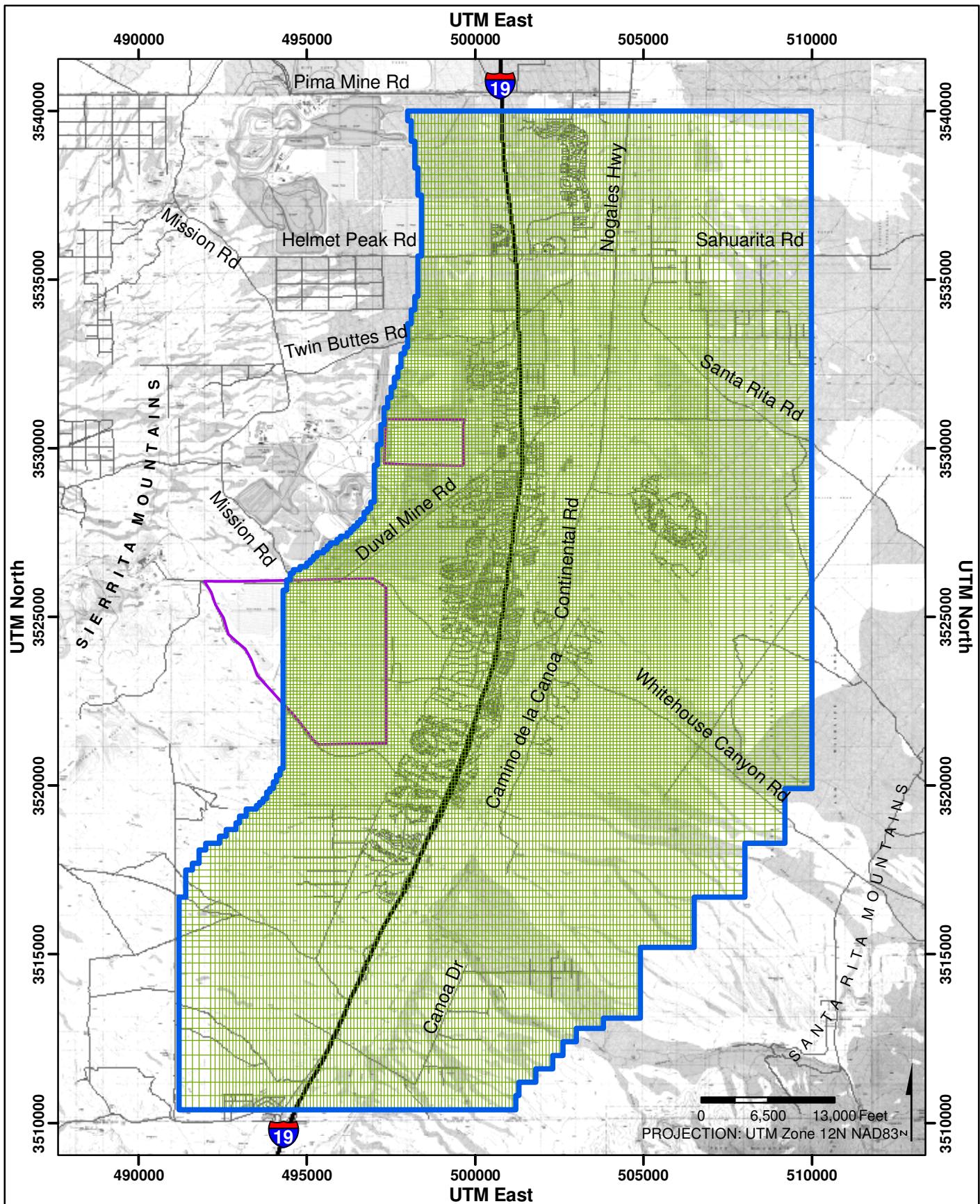
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#### MODEL EXTENTS AND WELL LOCATIONS

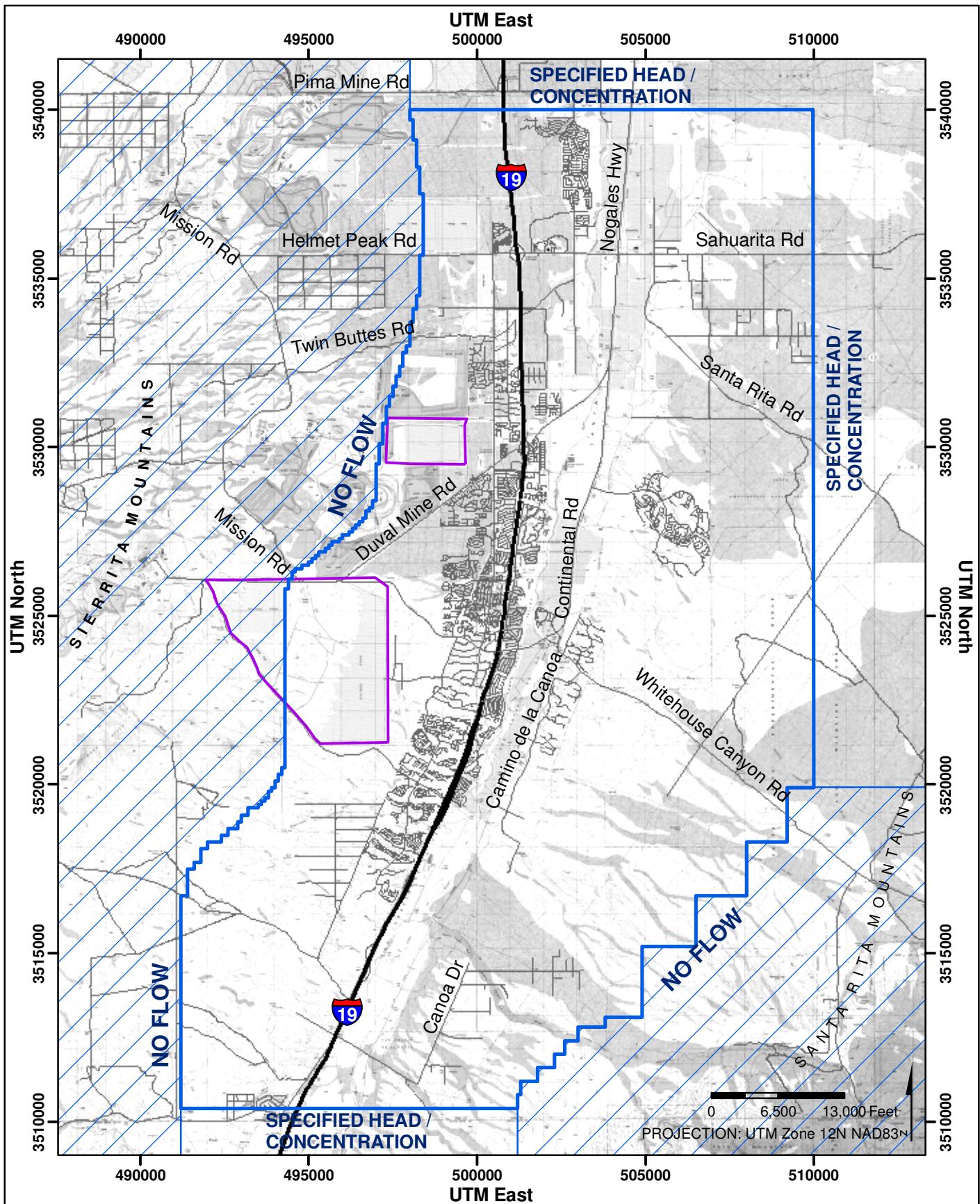
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#### MODEL DISCRETIZATION

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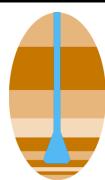
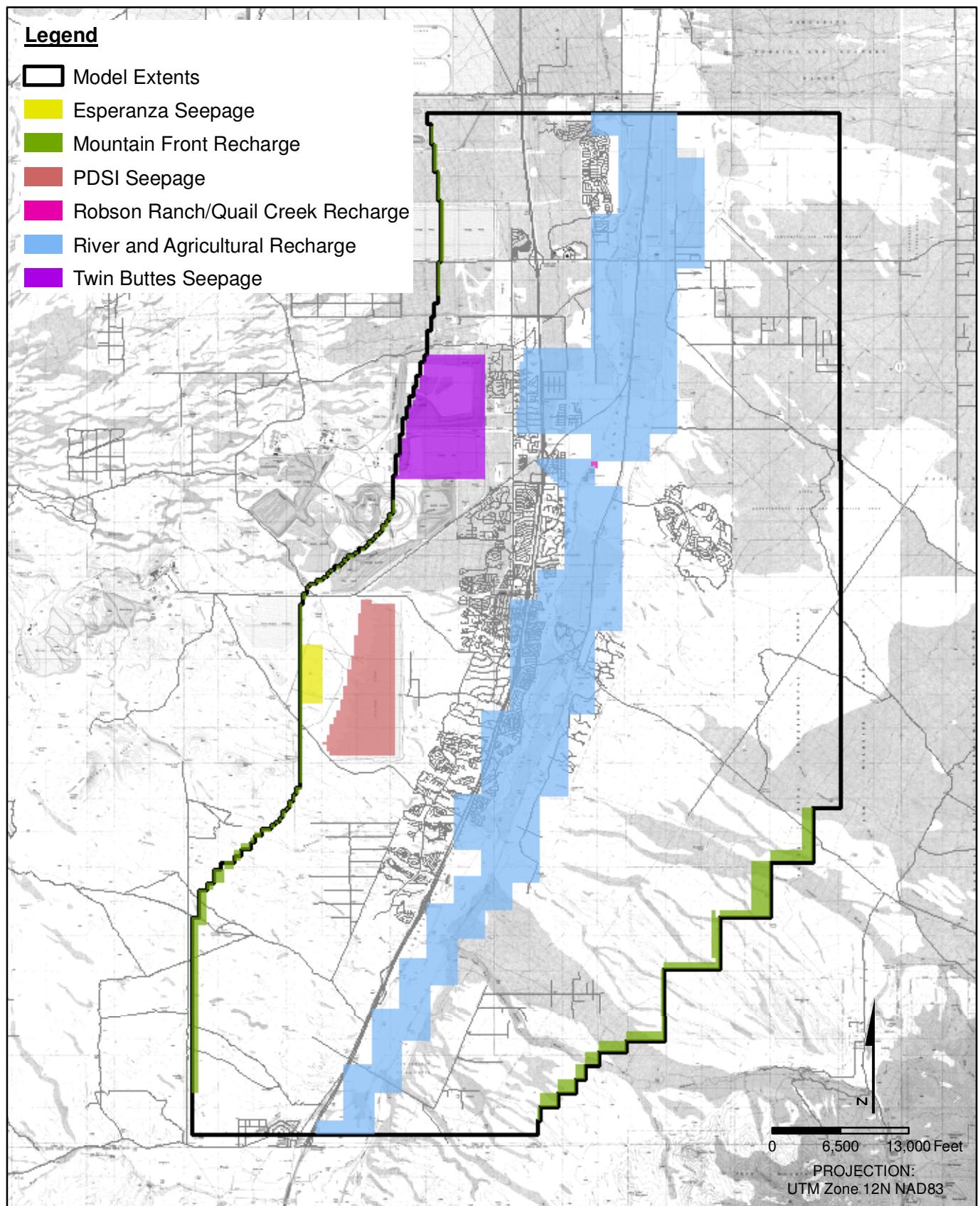
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#### MODEL BOUNDARY CONDITIONS

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| NWH      | 12/21/07 | RAM    | 12/21/07 | 78301404G | I.4    |

### Legend

- Model Extents
- Esperanza Seepage
- Mountain Front Recharge
- PDSI Seepage
- Robson Ranch/Quail Creek Recharge
- River and Agricultural Recharge
- Twin Buttes Seepage



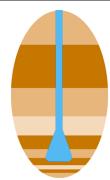
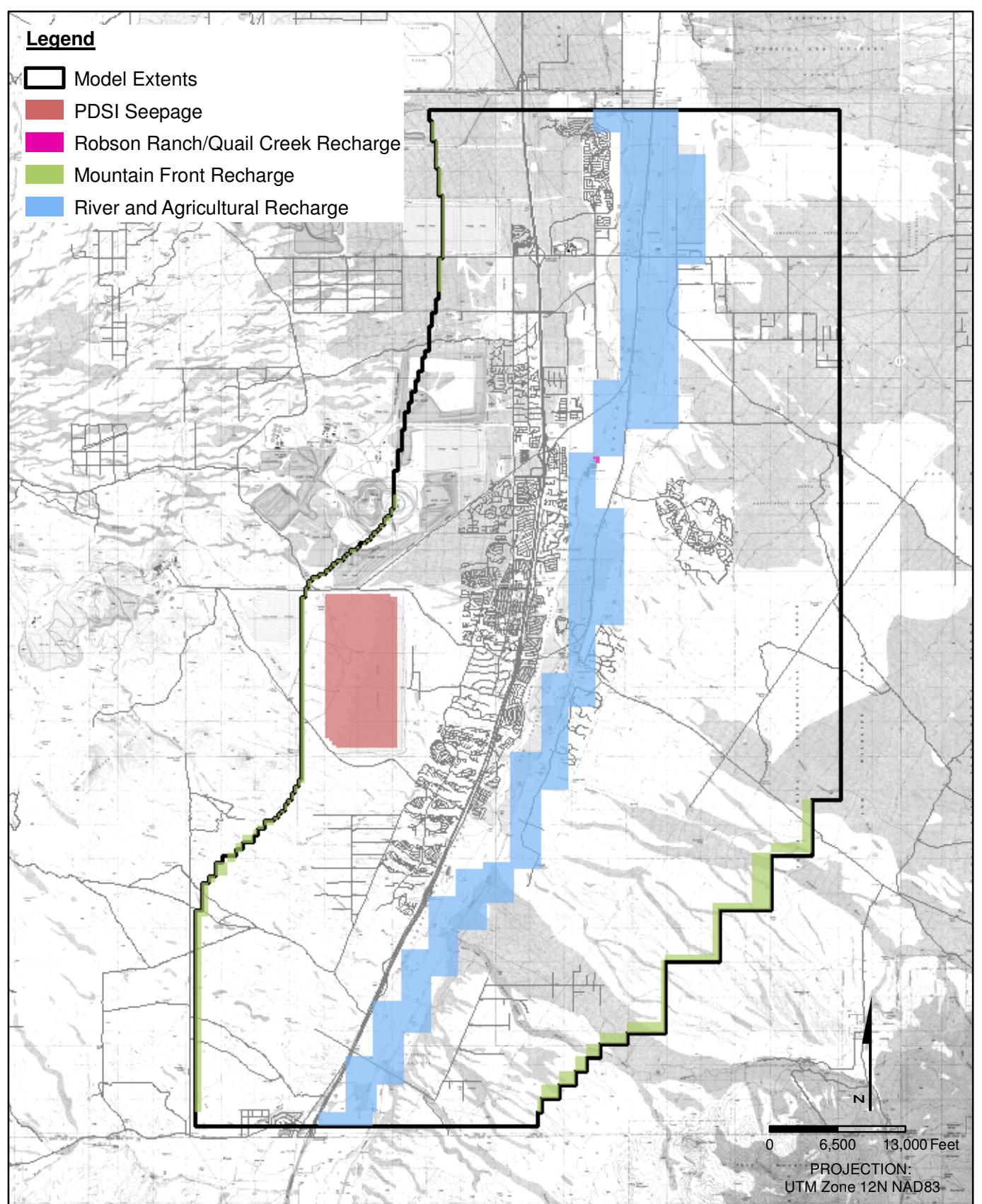
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### MODEL RECHARGE ZONES FOR 1980

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**Legend**

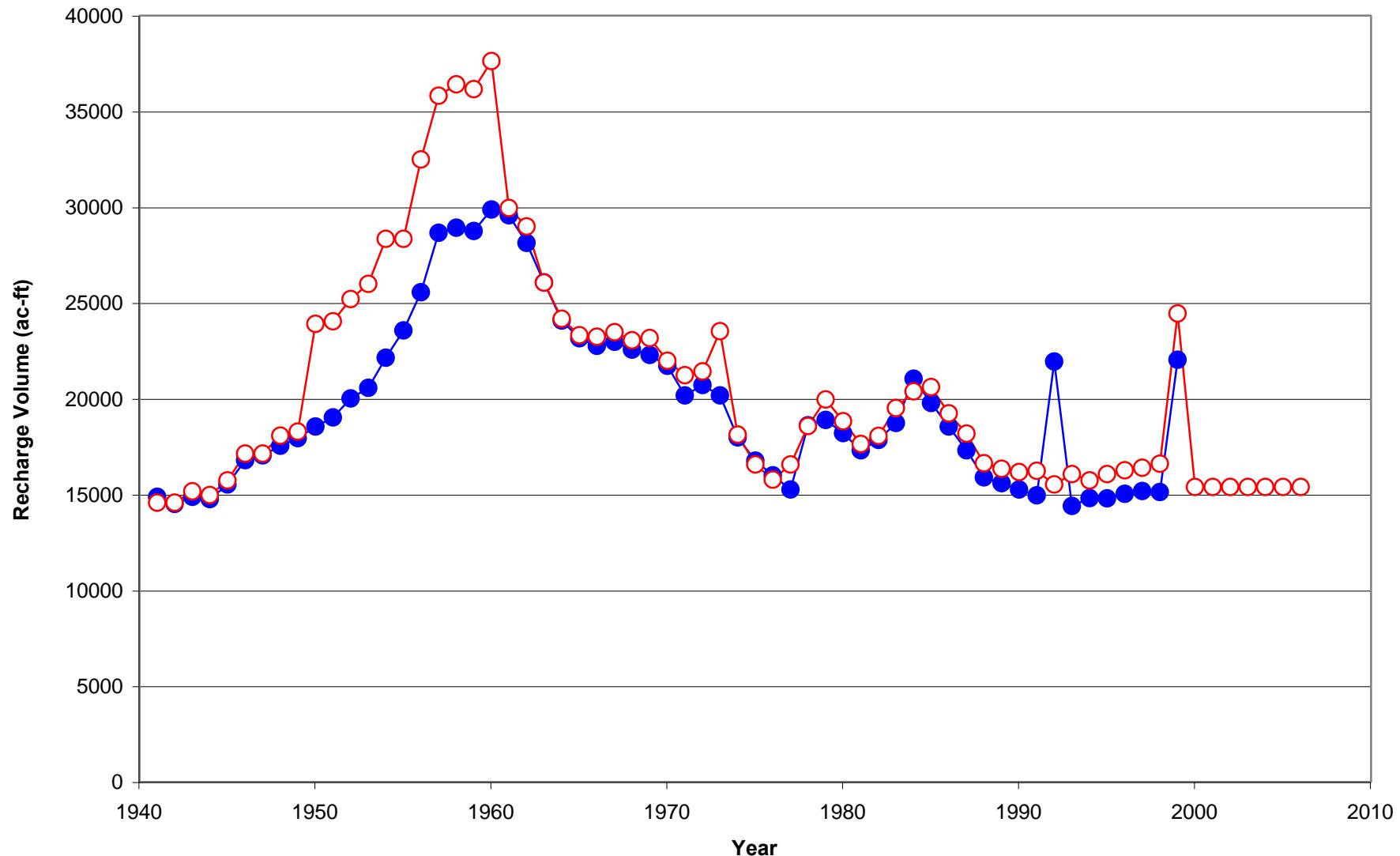
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- PDSI Seepage
- Robson Ranch/Quail Creek Recharge
- Mountain Front Recharge
- River and Agricultural Recharge



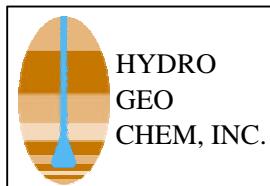
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**MODEL RECHARGE ZONES FOR 2006**

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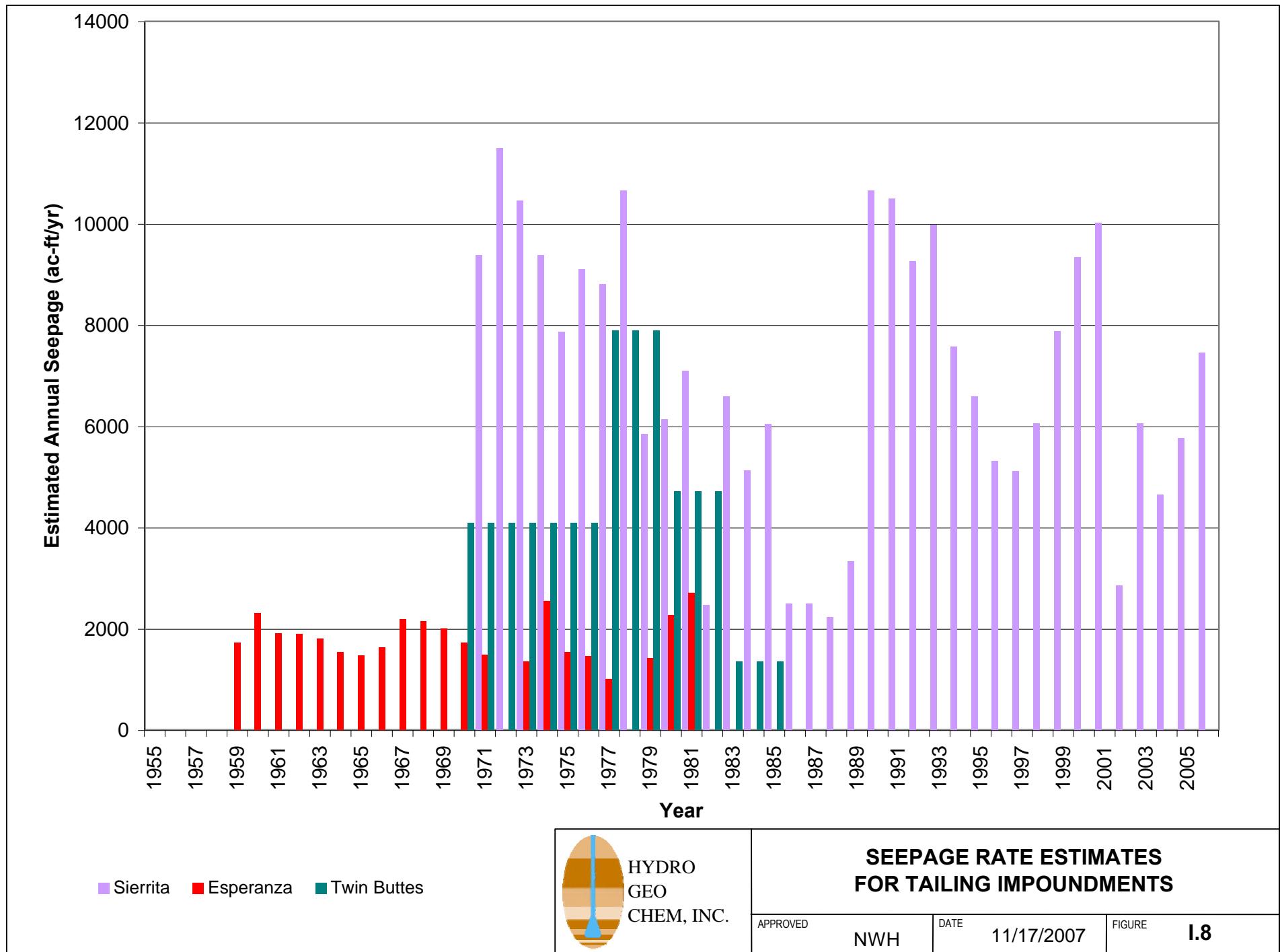
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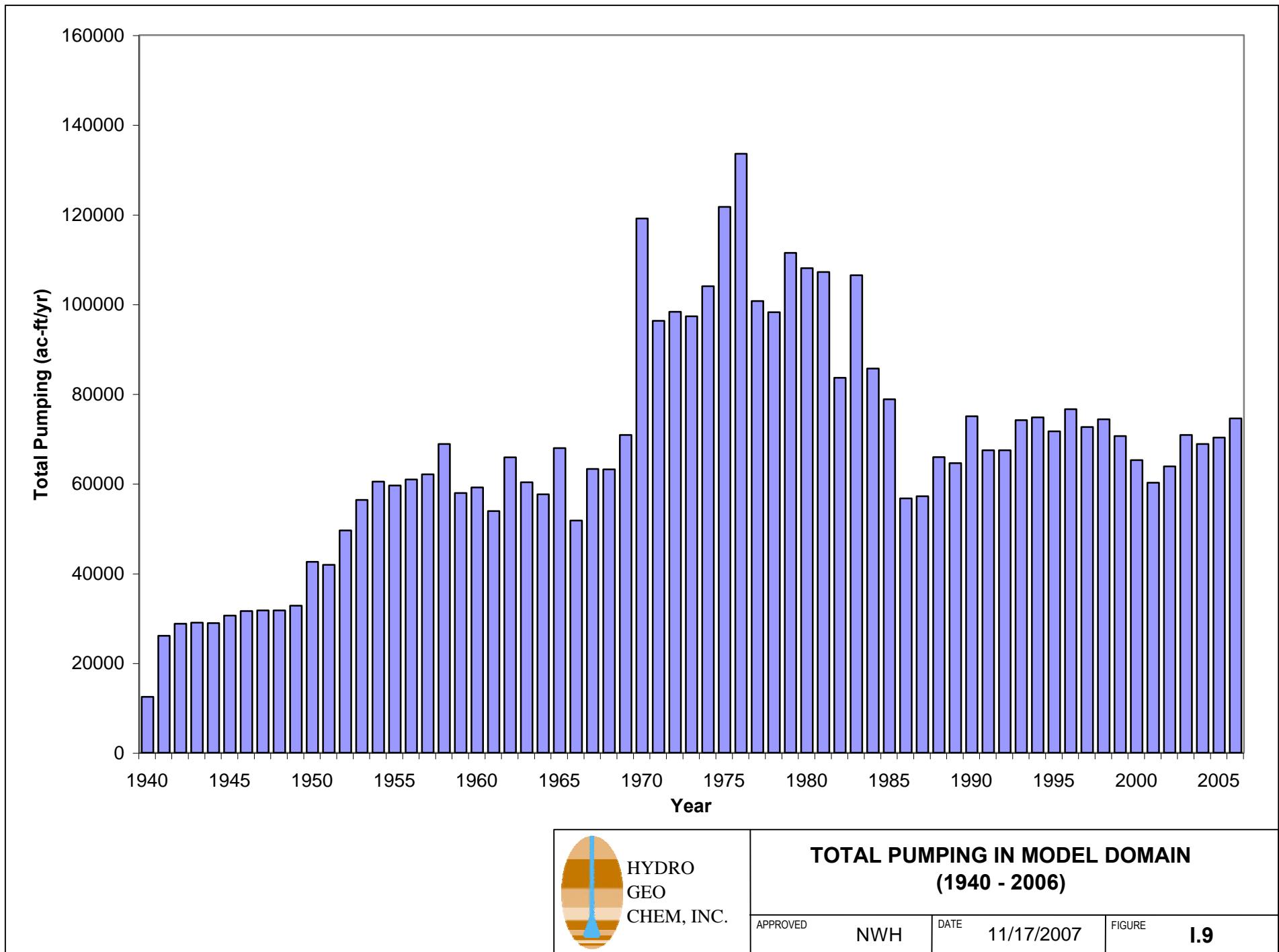


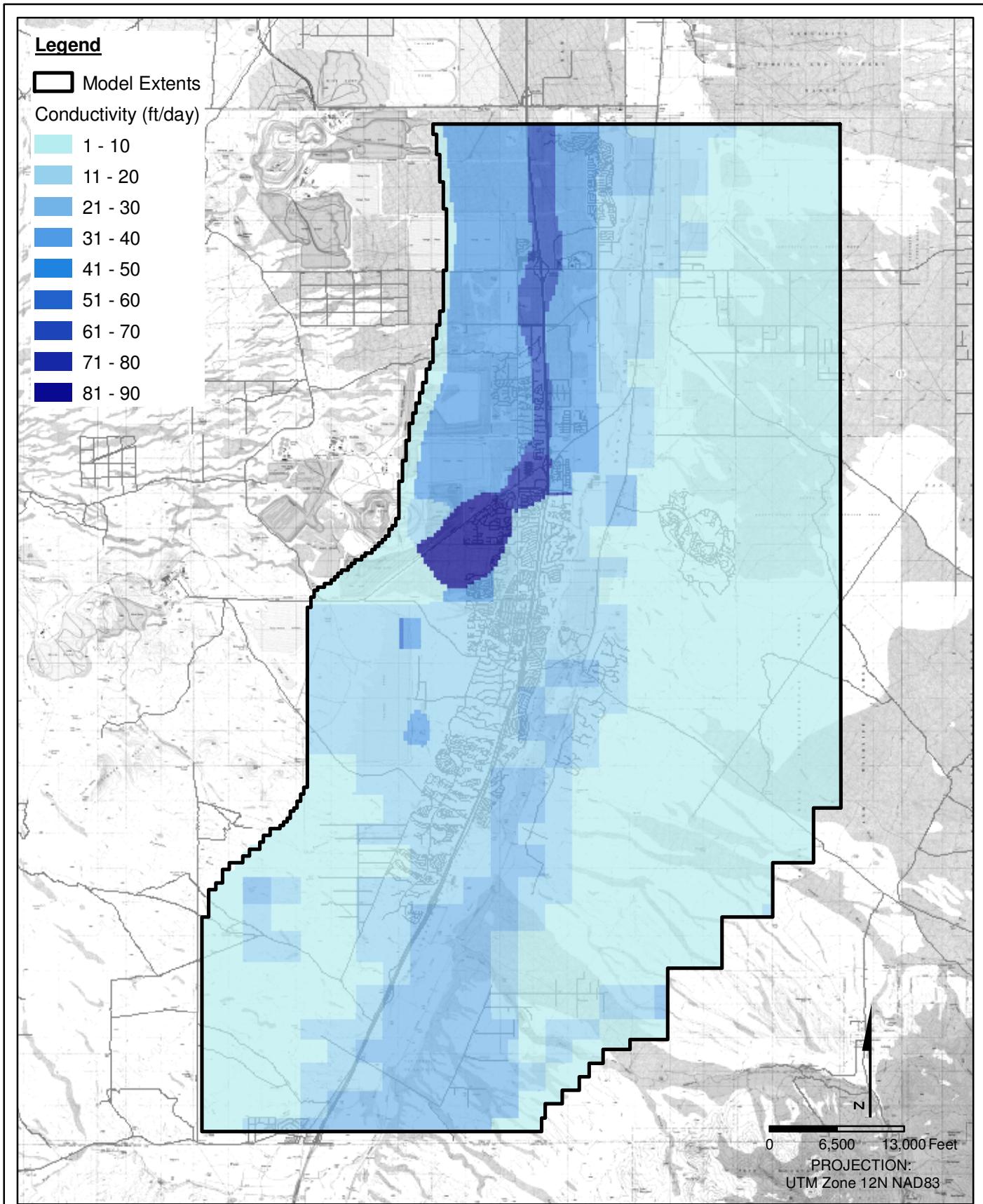
## RIVER AND AGRICULTURAL RECHARGE VOLUMES

|          |     |      |            |        |
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|----------|-----|------|------------|--------|

I.7



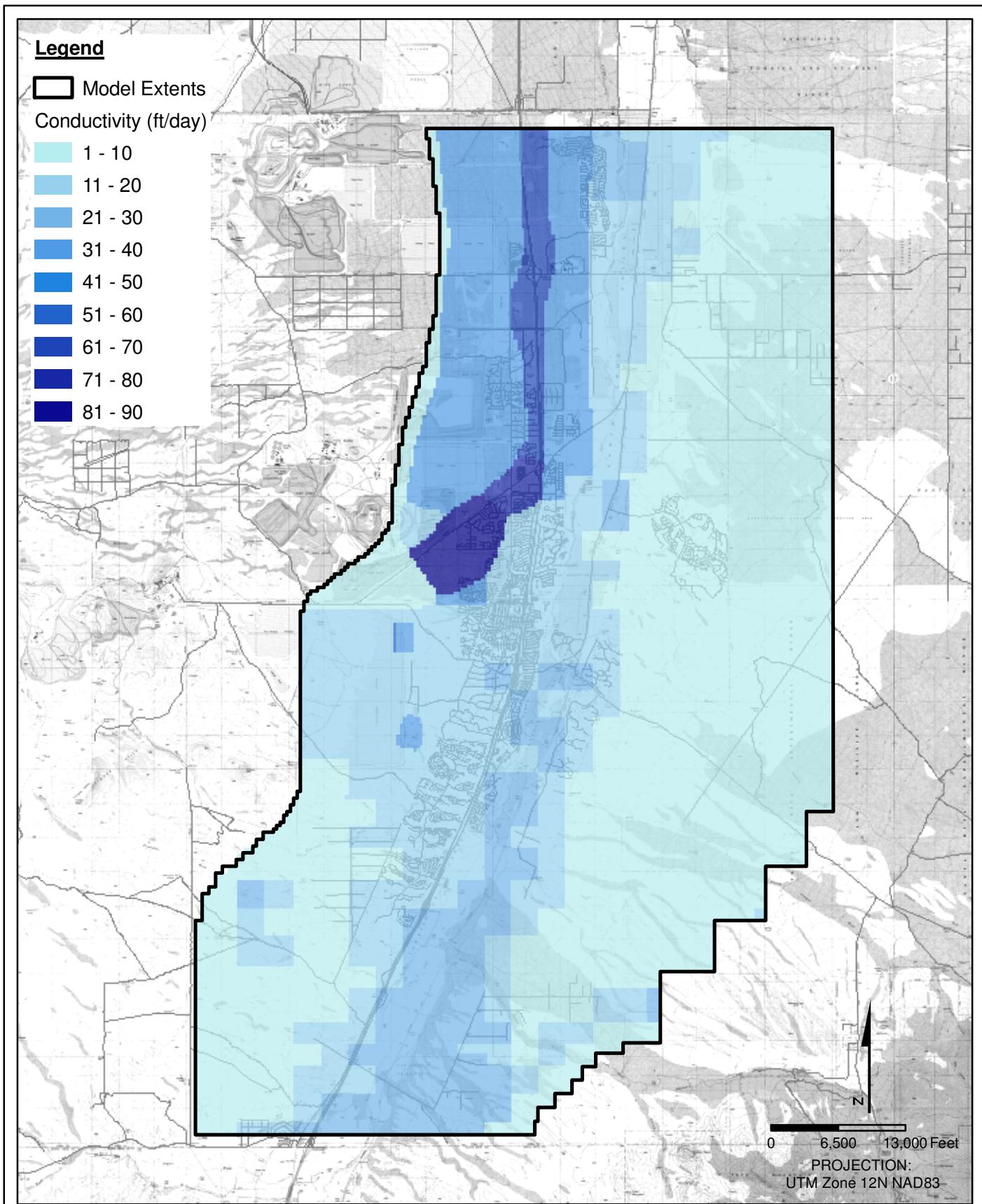




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**SATURATED HYDRAULIC CONDUCTIVITY  
DISTRIBUTION IN UPPER MODEL LAYER (LAYER 1)**

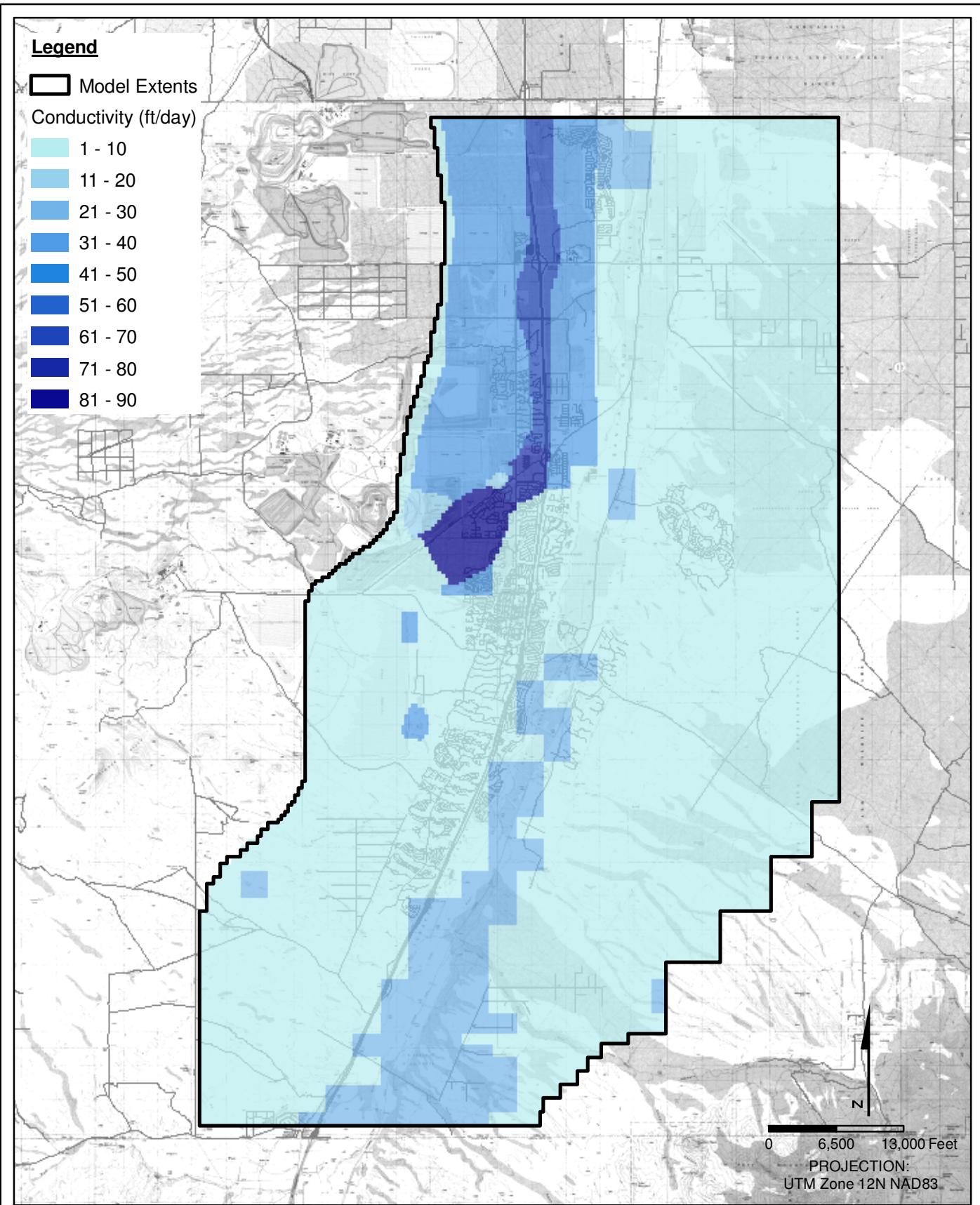
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**SATURATED HYDRAULIC CONDUCTIVITY  
DISTRIBUTION IN MIDDLE MODEL LAYER (LAYER 2)**

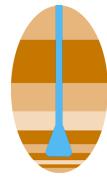
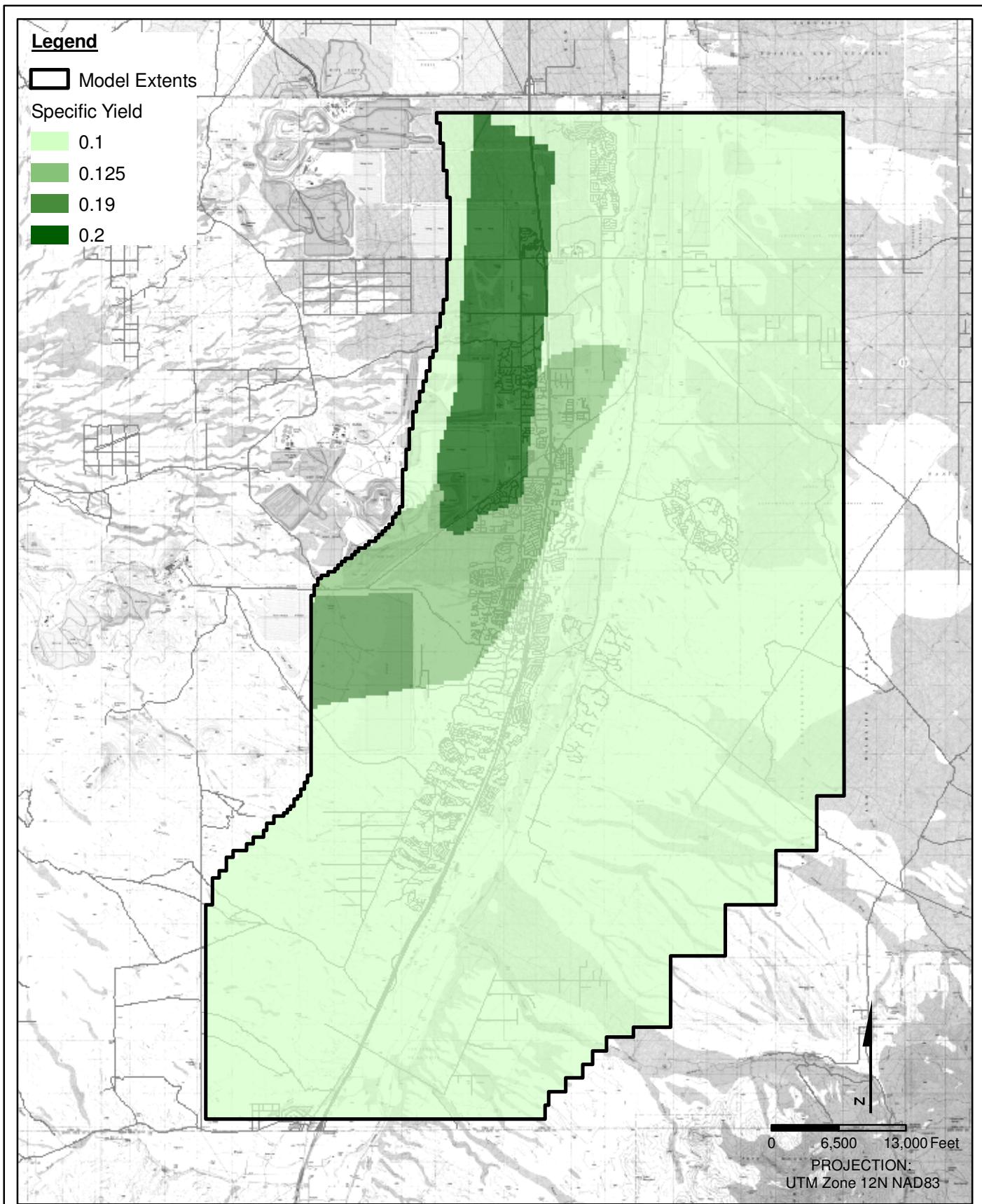
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**SATURATED HYDRAULIC CONDUCTIVITY  
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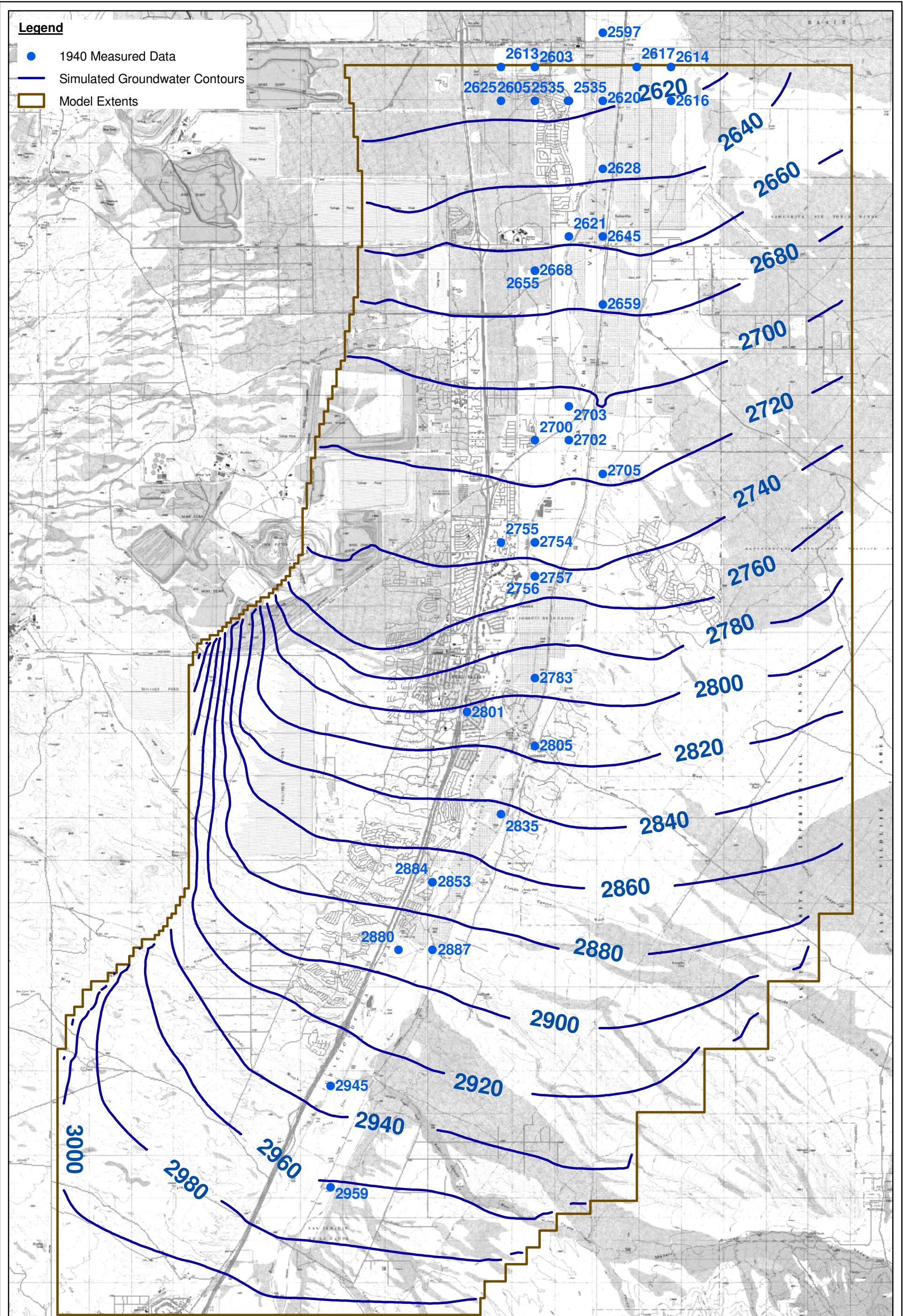
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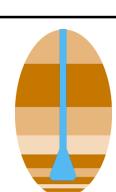
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**SPECIFIC YIELD DISTRIBUTION IN MODEL DOMAIN**

|                 |                  |               |                  |                        |                |
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| Approved<br>NWH | Date<br>11/21/07 | Author<br>RAM | Date<br>11/21/07 | File Name<br>78301410G | Figure<br>I.13 |
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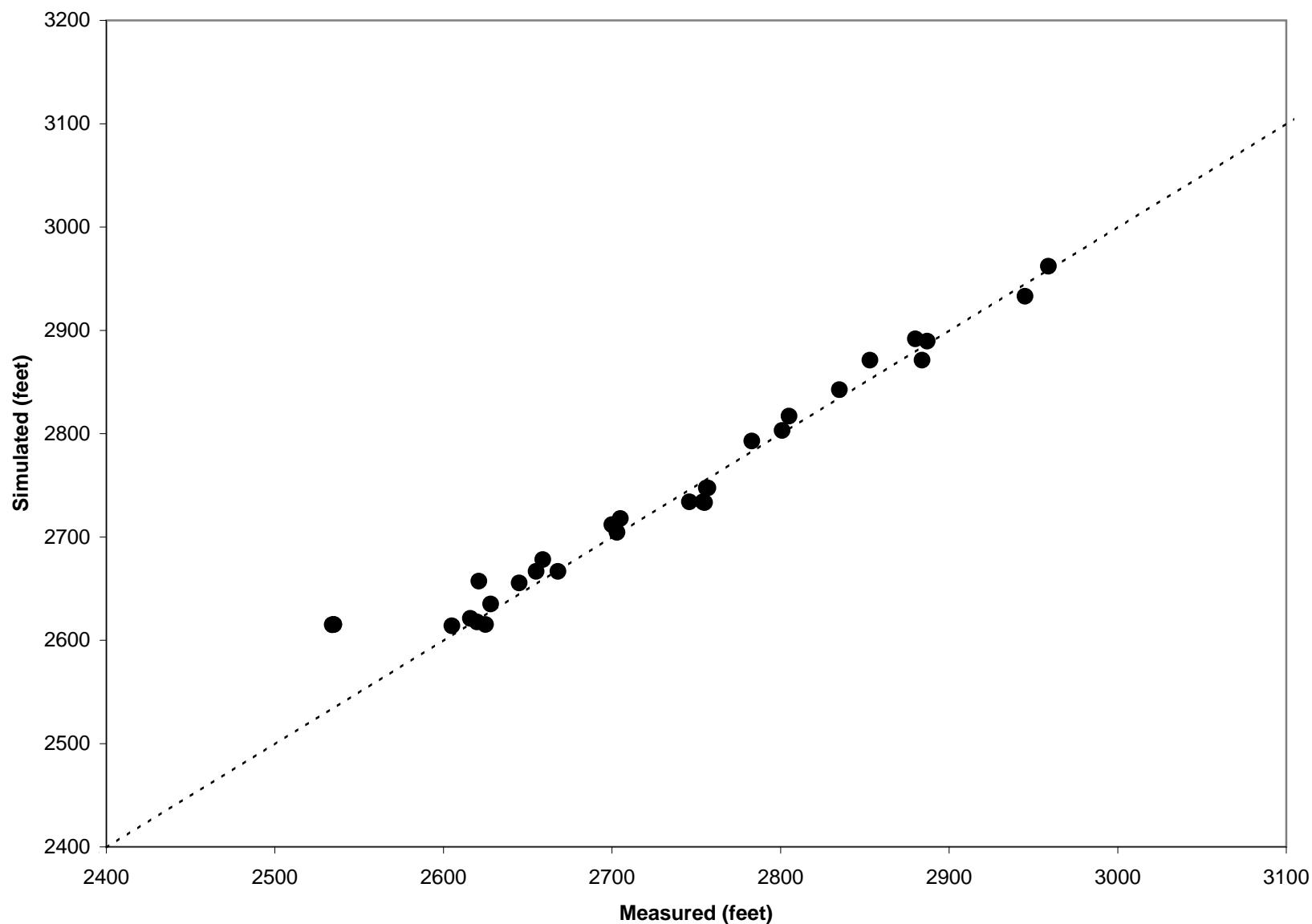
0 3,500 7,000 Feet  
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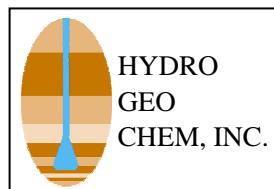
SIMULATED GROUNDWATER LEVEL CONTOURS WITH  
MEASURED DATA FOR 1940 STEADY-STATE SIMULATION

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● 1940 Targets

- - - 1:1



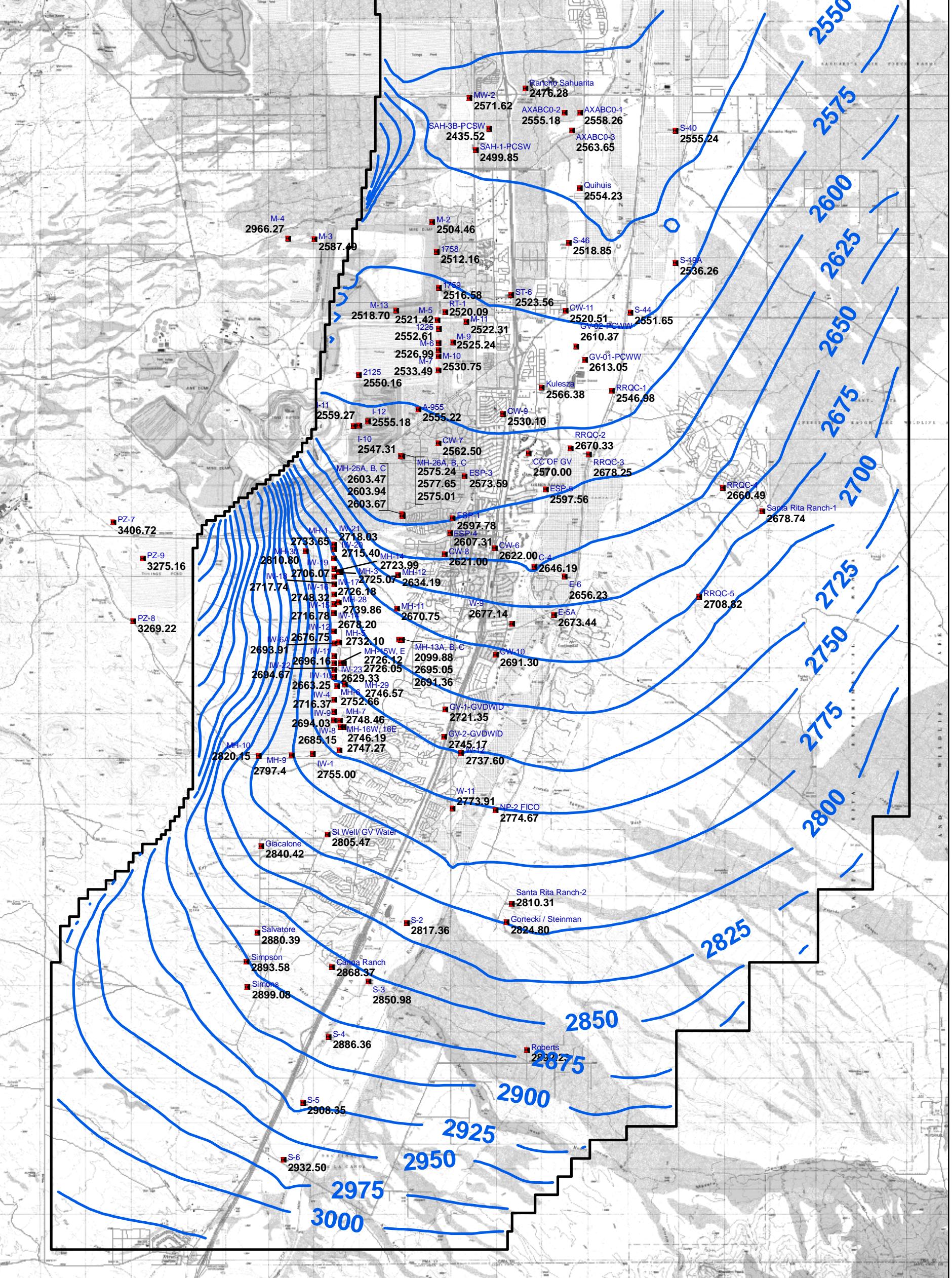
**SIMULATED VERSUS MEASURED  
GROUNDWATER LEVELS FOR STEADY-STATE  
SIMULATION (1940)**

APPROVED NWH DATE 11/21/2007 FIGURE I.15

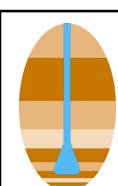
**Legend**

M-2 Well Location & Identifier  
2504.46 Measured Groundwater Elevation (ft amsl)

Simulated Groundwater Contours  
Model Extents



0 3,500 7,000 Feet



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SIMULATED GROUNDWATER LEVEL CONTOURS FOR  
THE END OF 2006 WITH MEASURED GROUNDWATER  
LEVELS FROM FIRST QUARTER 2007

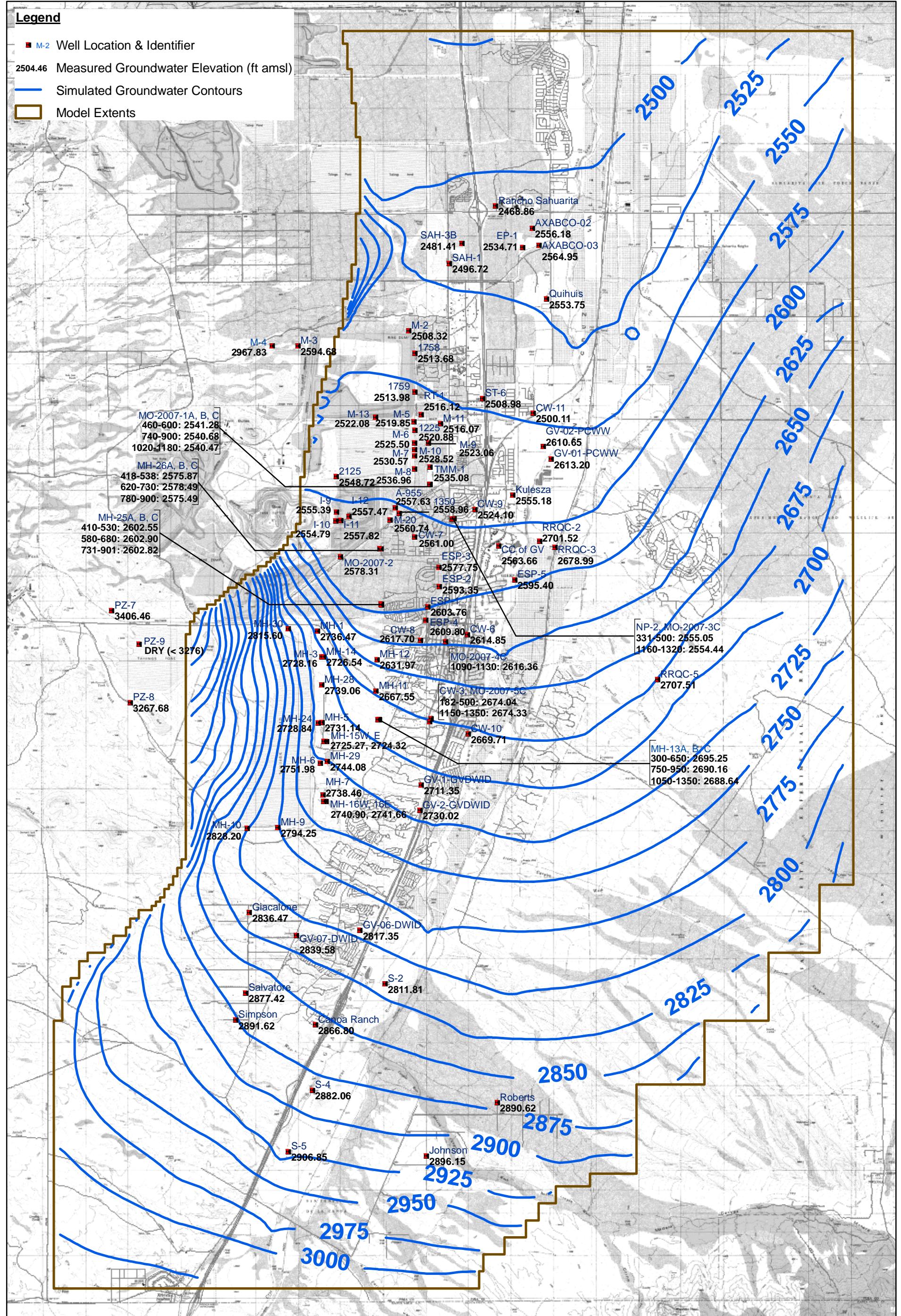
PROJECTION: UTM Zone 12N NAD83

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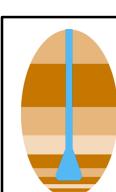
| Approved | Date     | Author | Date     | File Name | Figure |
|----------|----------|--------|----------|-----------|--------|
| NWH      | 12/21/07 | RAM    | 12/21/07 | 78301413G | I.16   |

**Legend**

- M-2 Well Location & Identifier
- 2504.46 Measured Groundwater Elevation (ft amsl)
- Simulated Groundwater Contours
- Model Extents



0 3,000 6,000 Feet



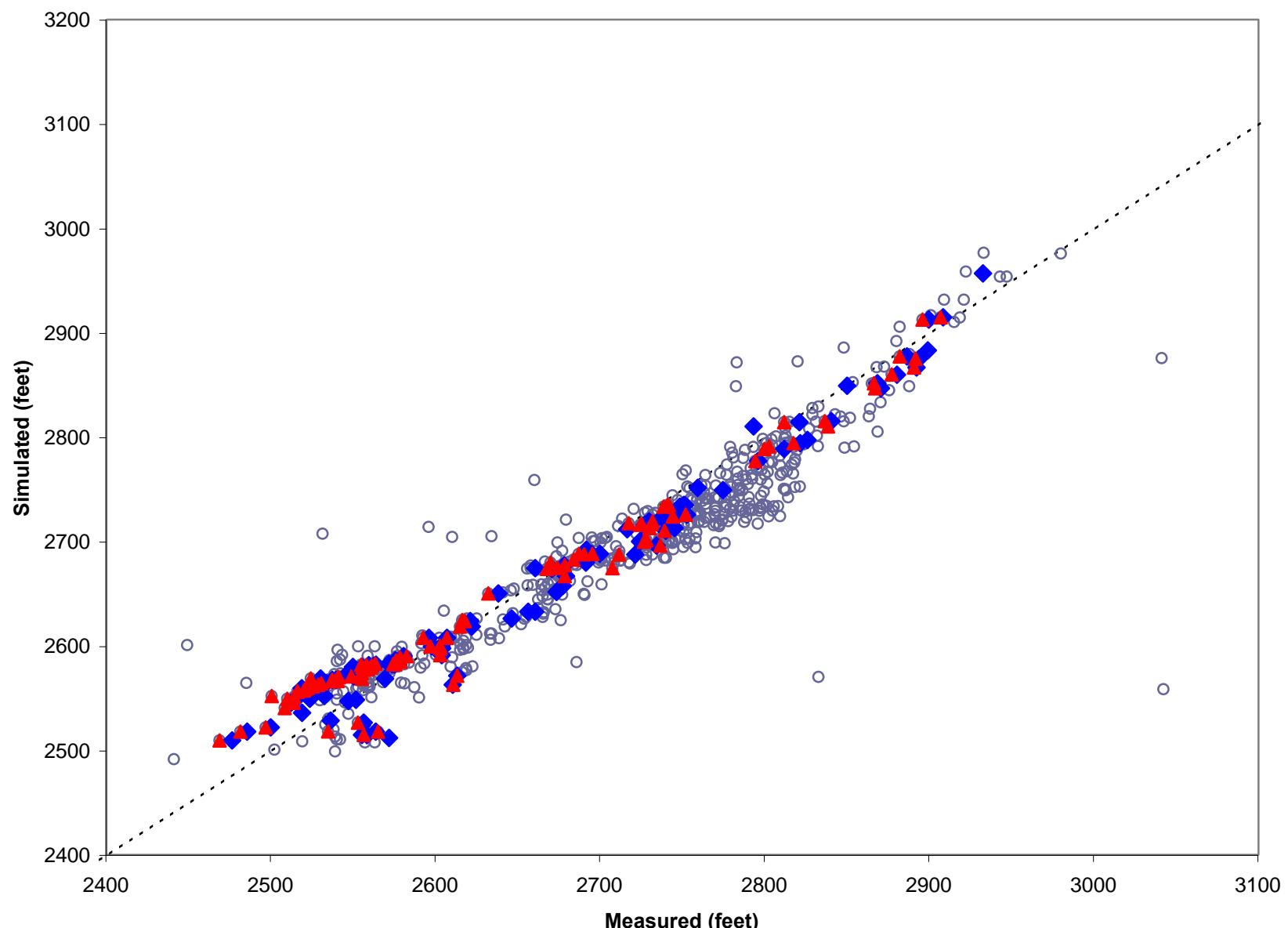
**HYDRO  
GEO  
CHEM, INC.**

**SIMULATED GROUNDWATER LEVEL CONTOURS FOR  
THE END OF 2006 WITH MEASURED GROUNDWATER  
LEVELS FROM THIRD QUARTER 2007**

PROJECTION: UTM Zone 12N NAD83

N

| Approved | Date     | Author | Date     | File Name | Figure |
|----------|----------|--------|----------|-----------|--------|
| NWH      | 12/21/07 | RAM    | 12/21/07 | 78301414G | I.17   |

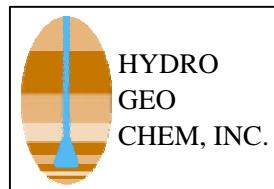


○ All Times

◆ Q1 2007

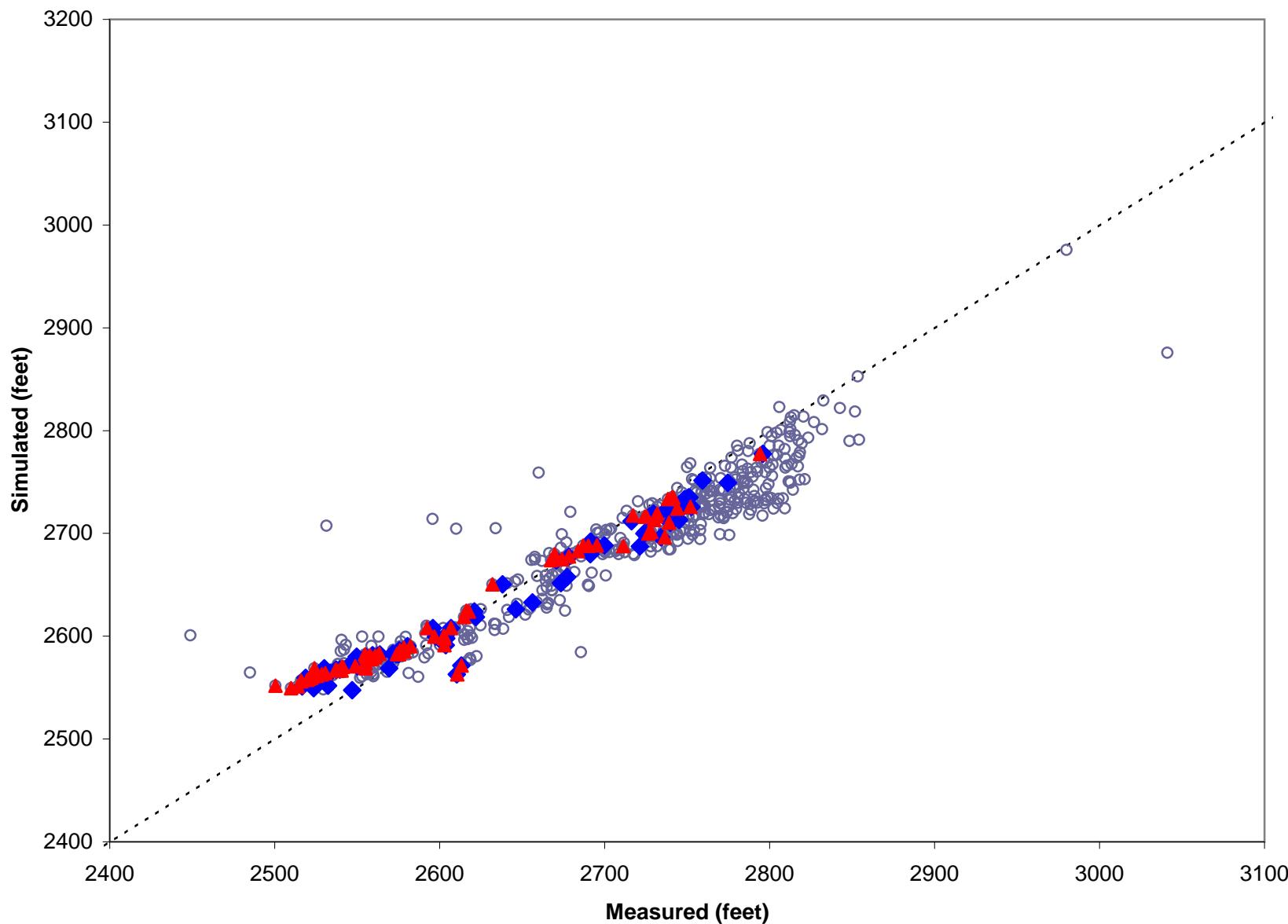
▲ Q3 2007

- - - 1:1

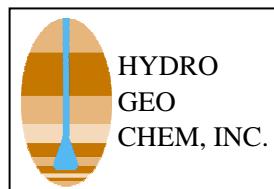


**SIMULATED VS. MEASURED GROUNDWATER  
LEVELS FOR TRANSIENT MODEL  
(Entire Model Domain)**

|          |     |      |            |        |
|----------|-----|------|------------|--------|
| APPROVED | NWH | DATE | 11/21/2007 | FIGURE |
|          |     |      |            | I.18   |



○ All Times      ♦ Q1 2007  
 ▲ Q3 2007      - - - 1:1

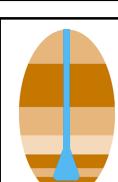
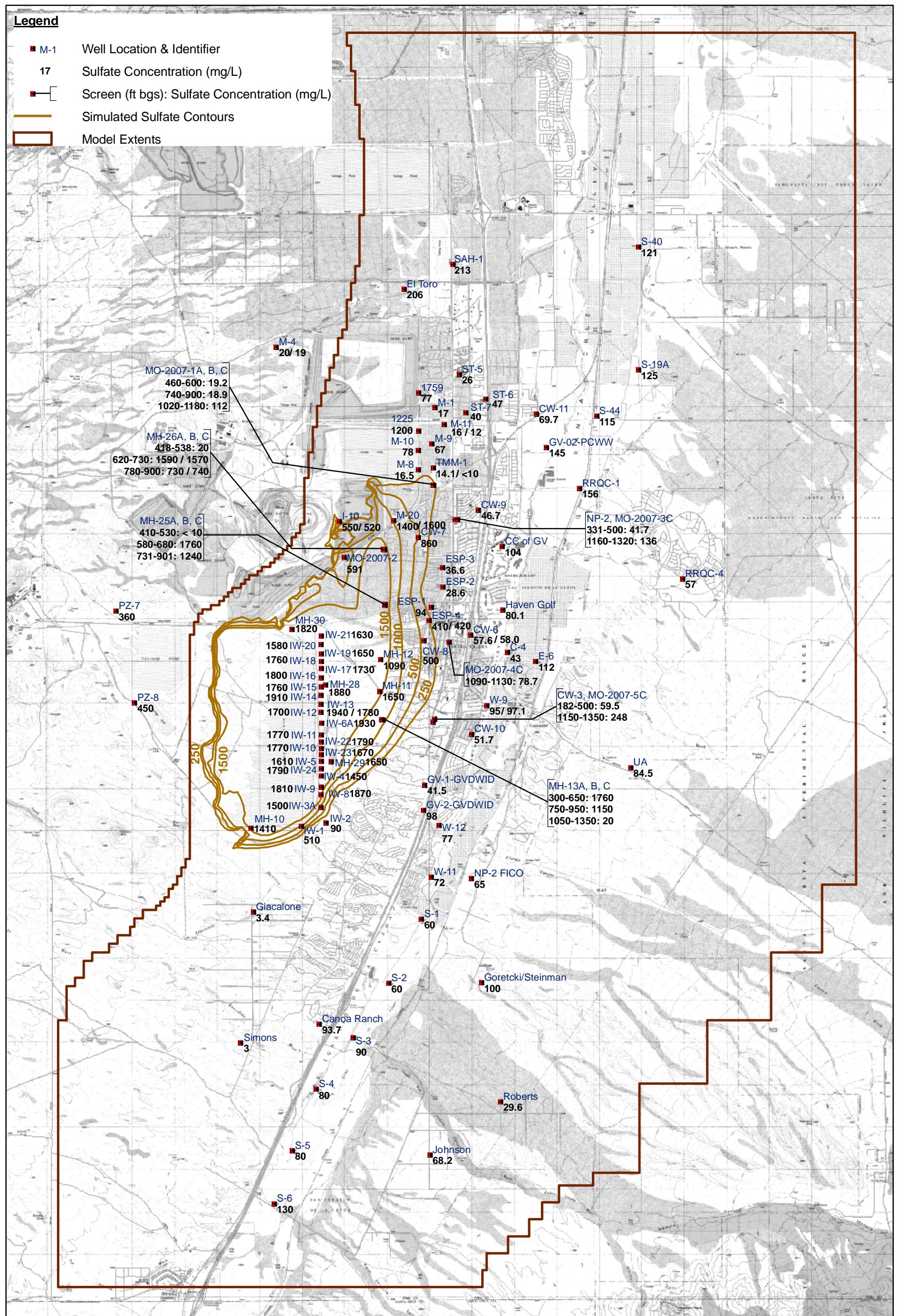


**SIMULATED VS. MEASURED GROUNDWATER  
LEVELS FOR TRANSIENT SIMULATION  
(Area of Emphasis Only)**

|             |     |      |            |        |
|-------------|-----|------|------------|--------|
| APPROVED    | NWH | DATE | 11/21/2007 | FIGURE |
| <b>I.19</b> |     |      |            |        |

**Legend**

- M-1 Well Location & Identifier
- 17 Sulfate Concentration (mg/L)
- Screen (ft bgs): Sulfate Concentration (mg/L)
- Simulated Sulfate Contours
- Model Extents

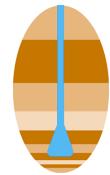
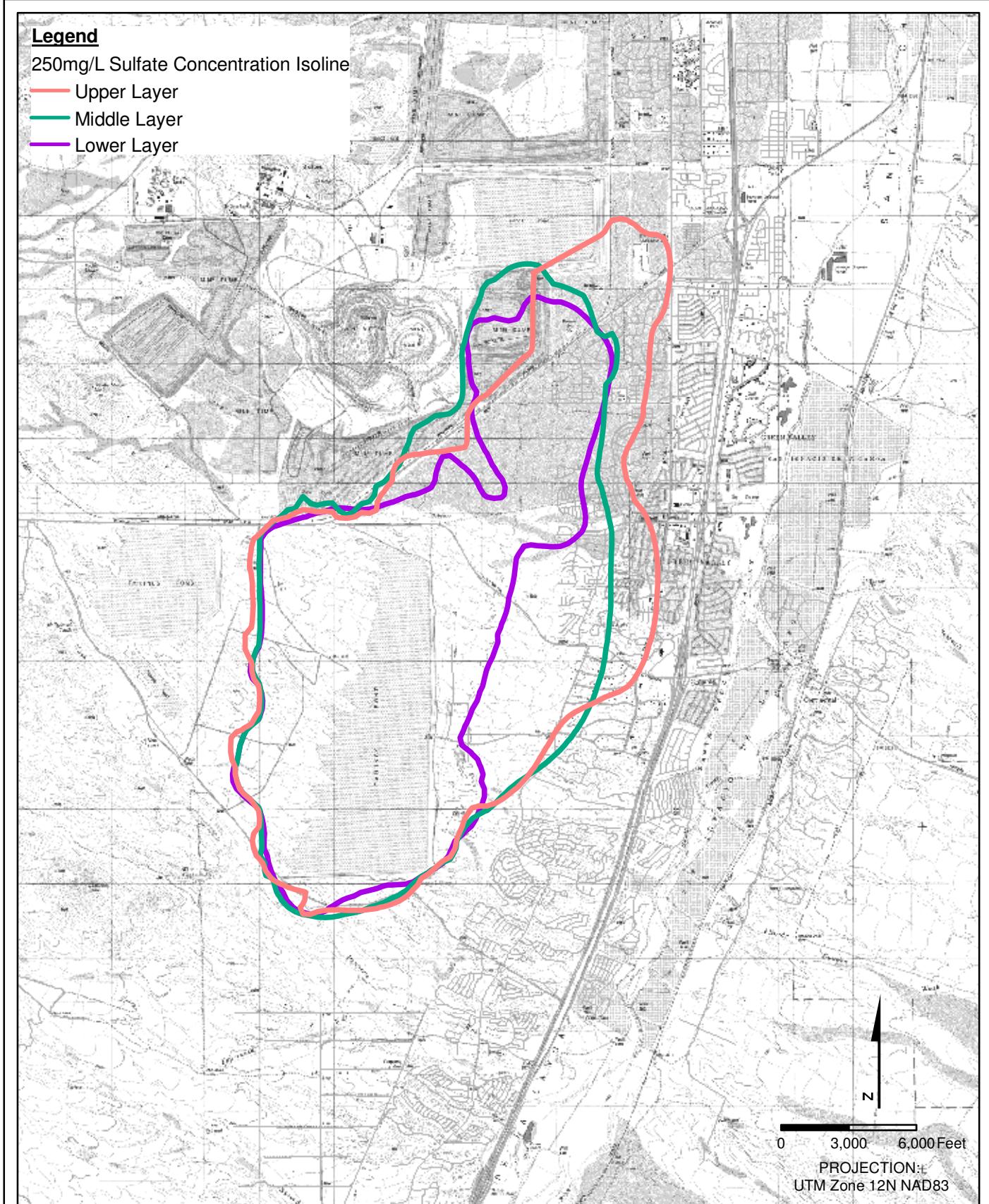


**HYDRO  
GEO  
CHEM, INC.**

**SIMULATED AVERAGE SULFATE CONCENTRATION  
CONTOURS WITH MEASURED SULFATE  
CONCENTRATIONS FROM THIRD QUARTER 2007**

PROJECTION:  
UTM Zone 12N NAD83

| Approved | Date     | Author | Date     | File Name | Figure |
|----------|----------|--------|----------|-----------|--------|
| NWH      | 12/21/07 | RAM    | 12/21/07 | 78301415G | I.20   |



**HYDRO  
GEO  
CHEM, INC.**

**SIMULATED SULFATE PLUME EXTENT IN  
UPPER, MIDDLE, AND LOWER MODEL LAYERS**

|                        |                         |                      |                         |                               |                       |
|------------------------|-------------------------|----------------------|-------------------------|-------------------------------|-----------------------|
| Approved<br><b>NWH</b> | Date<br><b>12/21/07</b> | Author<br><b>RAM</b> | Date<br><b>12/21/07</b> | File Name<br><b>78301421G</b> | Figure<br><b>I.21</b> |
|------------------------|-------------------------|----------------------|-------------------------|-------------------------------|-----------------------|

**APPENDIX I.1**

**WELL LOCATIONS AND PUMPING RATES**

**TABLE I.1.1**  
**Well Locations and Pumping Rates for**  
**Steady-State (1940) Simulation**

| UTM83E | UTM83N  | Pumping Rate<br>(gpm) |
|--------|---------|-----------------------|
| 496051 | 3511005 | 15                    |
| 496051 | 3511810 | 15                    |
| 496051 | 3512615 | 15                    |
| 496855 | 3511005 | 15                    |
| 496855 | 3511810 | 15                    |
| 496855 | 3512615 | 15                    |
| 497660 | 3515029 | 15                    |
| 497660 | 3515833 | 15                    |
| 498465 | 3515029 | 15                    |
| 498465 | 3515833 | 15                    |
| 500879 | 3519857 | 68                    |
| 500879 | 3522271 | 155                   |
| 500879 | 3523075 | 316                   |
| 500879 | 3524685 | 93                    |
| 500879 | 3525489 | 93                    |
| 500879 | 3526294 | 78                    |
| 500879 | 3527099 | 62                    |
| 500879 | 3530318 | 16                    |
| 501683 | 3522271 | 155                   |
| 501683 | 3524685 | 93                    |
| 501683 | 3525489 | 93                    |
| 501683 | 3526294 | 78                    |
| 501683 | 3527099 | 78                    |
| 501683 | 3529513 | 16                    |
| 501683 | 3530318 | 16                    |
| 502488 | 3524685 | 78                    |
| 502488 | 3525489 | 78                    |
| 502488 | 3526294 | 78                    |
| 502488 | 3527099 | 78                    |
| 502488 | 3527904 | 101                   |
| 502488 | 3528686 | 101                   |
| 502488 | 3542388 | 62                    |
| 502415 | 3543192 | 62                    |
| 503293 | 3524685 | 78                    |
| 503293 | 3525489 | 78                    |
| 503270 | 3526294 | 78                    |
| 503293 | 3527099 | 78                    |
| 503293 | 3527904 | 101                   |

**TABLE I.1.1**  
**Well Locations and Pumping Rates for**  
**Steady-State (1940) Simulation**

| UTM83E | UTM83N  | Pumping Rate<br>(gpm) |
|--------|---------|-----------------------|
| 503293 | 3528708 | 101                   |
| 503293 | 3542388 | 62                    |
| 503293 | 3543192 | 62                    |
| 504097 | 3529513 | 93                    |
| 504097 | 3530318 | 93                    |
| 504097 | 3531927 | 868                   |
| 504097 | 3532732 | 336                   |
| 504074 | 3535950 | 310                   |
| 504097 | 3537560 | 139                   |
| 504097 | 3538364 | 279                   |
| 504097 | 3539169 | 174                   |
| 504097 | 3539974 | 174                   |
| 504097 | 3542388 | 62                    |
| 504097 | 3543192 | 62                    |
| 504902 | 3529513 | 93                    |
| 504902 | 3530318 | 93                    |
| 504902 | 3533536 | 336                   |
| 504902 | 3535146 | 310                   |
| 504902 | 3537560 | 139                   |
| 504902 | 3539169 | 174                   |
| 504902 | 3539974 | 174                   |
| 504902 | 3542388 | 62                    |
| 504902 | 3543192 | 62                    |
| 505707 | 3536755 | 558                   |
| 505707 | 3537560 | 78                    |
| 505707 | 3538364 | 78                    |
| 506511 | 3537560 | 78                    |
| 506511 | 3538364 | 78                    |

*Notes:*

*Well locations and pumping rates from ADWR Model (Mason and Bota, 2006)*

*UTM83E = Universal Transverse Mercator, North American Datum 1983, East*

*UTM83N = Universal Transverse Mercator, North American Datum 1983, North*

*gpm = gallons per minute*

**TABLE I.1.2**

### **Applications and Pumping Rates for SRT Model (Mason and Bota, 2006)**

**TABLE I.1.2**

### **Applications and Pumping Rates for SFR Model (Mason and Bota, 2006)**

28

*: Universal Transverse Mercator, North American Datum 1983, East*

: Universal Transverse Mercator, North American Datum 1983, North

Universal Transverse Mercator, North  
specified after 1983

g units in gallons per minute (gpm)

*g units in gallons per minute (gpm)*

TABLE I.1.3

Well Locations and Pumping Rates for  
Transient Simulation, Taken from Various Sources<sup>a</sup>

| Well ID      | ADWR Registration | UTM83E | UTM83N  | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 |   |   |   |   |   |   |   |   |
|--------------|-------------------|--------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|---|---|---|---|---|---|---|---|
| 11caa        | 801179            | 501186 | 3526788 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 55   | 36   | 69   | 38   | 46   | 54   | 53   | 46   | 42   | 58   | 46   | 42   | 35   | 42   | 31   | 28   | 37   | 48   | 37   | 19   | 0    | 0    |      |      |   |   |   |   |   |   |   |   |
| 25cbd        | 634348            | 492757 | 3531386 | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 22   | 18   | 16   | 15   | 19   | 1    | 12   | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |
| AN1          | 608518            | 502595 | 3527990 | 2325 | 2325 | 2325 | 2325 | 1131 | 1131 | 1131 | 1131 | 1131 | 1266 | 1248 | 166  | 10   | 19   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |   |   |   |   |   |   |   |   |
| AN-2(RRQC2)  | 608519            | 503457 | 3529250 | 1548 | 1548 | 1548 | 1548 | 1131 | 1131 | 1131 | 1131 | 1131 | 1189 | 1221 | 126  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 5    | 5    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |
| AN-4(RRQC1)  | 608521            | 503457 | 3527990 | 0    | 0    | 0    | 0    | 0    | 0    | 1131 | 1131 | 1131 | 1131 | 1131 | 1279 | 664  | 58   | 69   | 60   | 3    | 0    | 0    | 0    | 0    | 0    | 0    | 94   | 156  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |   |   |   |   |   |   |   |   |
| C1           | 624008            | 503353 | 3529320 | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 47   | 39   | 35   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |   |   |   |   |   |   |   |   |
| C4           | 624010            | 501760 | 3525384 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1247 | 1033 | 922  | 854  | 823  | 1160 | 932  | 710  | 783  | 756  | 922  | 911  | 852  | 833  | 1167 | 817  | 987  | 840  | 914  | 888  | 757  | 794  | 808  | 908  | 921  | 1113 |      |   |   |   |   |   |   |   |   |
| CcofGV       | 501760            | 501635 | 3527876 | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 453  | 376  | 335  | 311  | 280  | 375  | 336  | 389  | 324  | 396  | 379  | 364  | 388  | 440  | 453  | 408  | 378  | 377  | 353  | 340  | 393  | 371  | 289  | 117  | 54   |      |      |   |   |   |   |   |   |   |   |
| CEMEX        | 607815            | 505129 | 3540303 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |
| Colgate      | 639904            | 509408 | 3532606 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |   |   |   |   |   |   |   |   |
| ContSD39     | 601769            | 504049 | 3522942 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |   |   |   |   |   |   |   |   |
| Cox          | 604432            | 508795 | 3534015 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 4    | 2    | 2    | 3    | 2    | 0    | 2    | 7    | 3    | 3    | 2    | 3    | 4    | 3    | 2    | 2    | 2    | 2    | 2    |      |      |      |      |   |   |   |   |   |   |   |   |
| Cox          | 627079            | 508795 | 3534015 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |   |   |   |   |   |   |   |   |
| CSD39        | 638581            | 504049 | 3522942 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |   |   |   |   |   |   |   |   |
| CW3          | 627483            | 500048 | 3523810 | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 212  | 175  | 157  | 145  | 142  | 5    | 0    | 1    | 0    | 0    | 0    | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |   |   |   |   |   |   |   |   |
| CW5          | 627484            | 501234 | 3522497 | 0    | 0    | 0    | 0    | 187  | 187  | 187  | 187  | 187  | 175  | 145  | 129  | 120  | 275  | 223  | 269  | 284  | 293  | 224  | 268  | 287  | 254  | 290  | 316  | 309  | 199  | 139  | 131  | 89   | 85   | 105  | 0    | 0    | 0    | 0    | 0    | 0 |   |   |   |   |   |   |   |
| CW6          | 627485            | 500891 | 3525794 | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 393  | 326  | 291  | 269  | 276  | 404  | 353  | 348  | 319  | 366  | 311  | 352  | 336  | 388  | 439  | 248  | 371  | 342  | 103  | 326  | 401  | 418  | 221  | 295  | 252  | 183  |   |   |   |   |   |   |   |   |
| CW7          | 502546            | 499660 | 3528094 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 511  | 456  | 423  | 285  | 408  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 |   |   |   |
| CW8          | 543600            | 499799 | 3525661 | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 9    | 428  | 453  | 517  | 623  | 677  | 527  | 723  | 713  | 426  | 1    | 1    |      |      |      |   |   |   |   |   |   |   |   |
| CW9          | 588121            | 501072 | 3528741 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |   |   |   |   |   |   |   |   |
| Davis_Robert | 516216            | 507647 | 3533428 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| E10A         | 086931            | 502452 | 3523995 | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 40   | 33   | 30   | 27   | 27   | 38   | 28   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 |   |   |   |
| E11A         | 624018            | 502092 | 3527822 | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 439  | 363  | 324  | 300  | 325  | 191  | 100  | 245  | 296  | 294  | 304  | 373  | 294  | 339  | 298  | 246  | 341  | 332  | 378  | 330  | 305  | 284  | 446  | 496  | 501  | 445  |   |   |   |   |   |   |   |   |
| E12          | 624019            | 500635 | 3520347 | 490  | 490  | 490  | 490  | 490  | 490  | 490  | 490  | 490  | 490  | 459  | 380  | 339  | 314  | 341  | 447  | 325  | 202  | 199  | 183  | 190  | 232  | 221  | 263  |      |      |      |      |      |      |      |      |      |      |      |      |   |   |   |   |   |   |   |   |

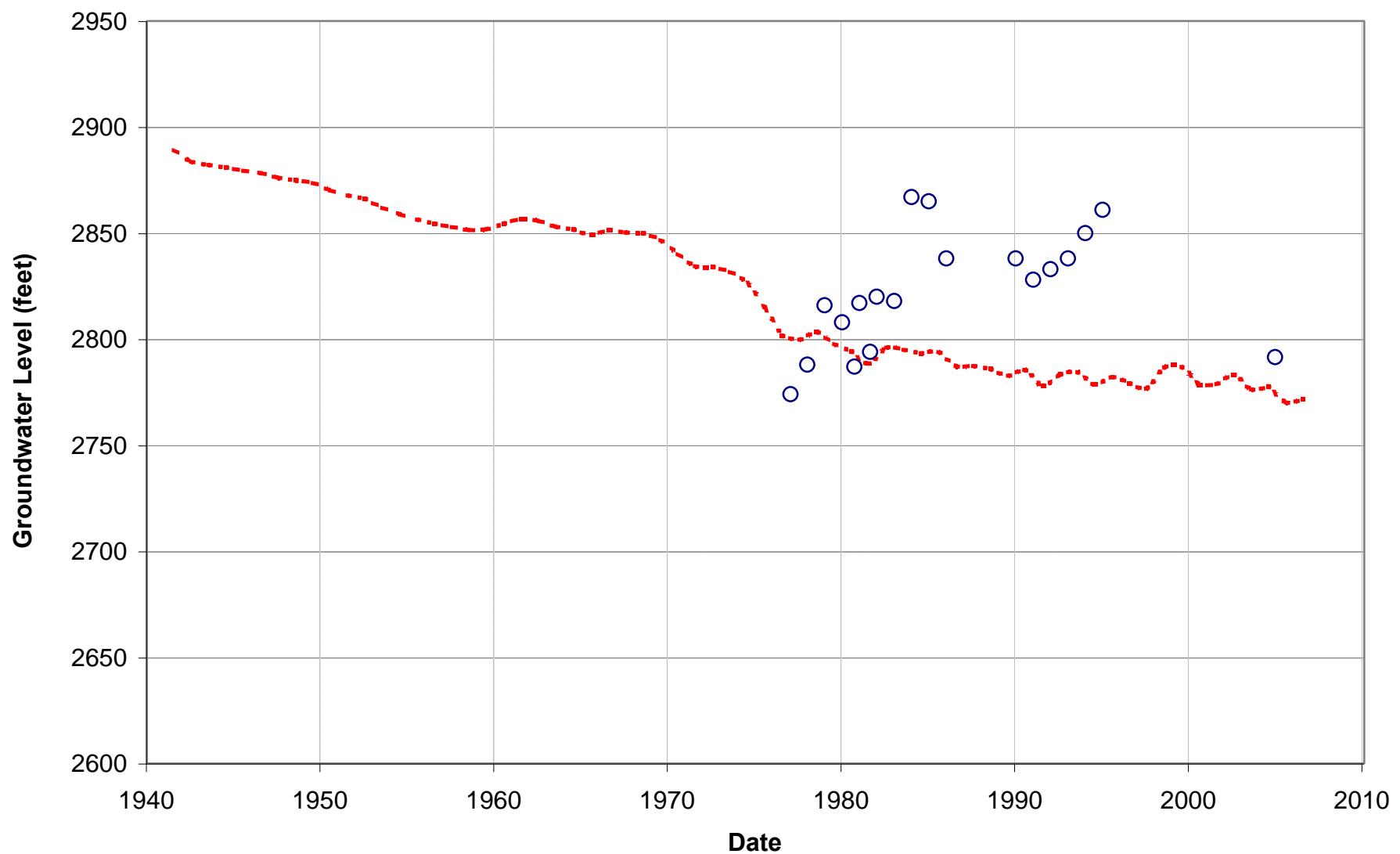
TABLE I.1.3

Well Locations and Pumping Rates for  
Transient Simulation, Taken from Various Sources<sup>a</sup>

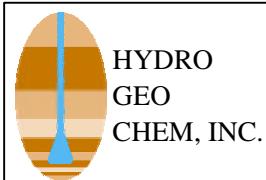
| Well ID           | ADWR Registration | UTM83E | UTM83N  | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 |      |      |
|-------------------|-------------------|--------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| M13               | 611139            | 503350 | 3540498 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 107  | 521  | 611  | 507  | 703  | 608  | 726  | 643  | 590  | 759  | 790  | 452  | 257  | 487  | 241  | 724  |      |      |      |
| M14               | 532046            | 502554 | 3539883 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 19   | 473  | 533  | 833  | 911  | 645  | 849  | 648  | 922  | 799  | 659  | 361  | 307  | 409  | 293  | 717  |      |      |      |
| M6                | 607787            | 500542 | 3540494 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 517  | 671  | 673  | 926  | 781  | 872  | 378  | 346  | 434  | 176  | 84   | 137  | 241  | 346  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| M7                | 607788            | 500947 | 3540494 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 514  | 832  | 649  | 949  | 970  | 532  | 134  | 205  | 796  | 479  | 500  | 205  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| M8                | 607789            | 501351 | 3540493 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 524  | 125  | 801  | 878  | 660  | 471  | 794  | 753  | 576  | 568  | 593  | 614  | 510  | 417  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |
| Madera_Highlands  | 624019            | 503285 | 3526162 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 93   | 101  | 132  | 96   | 60   | 59   | 184  | 191  | 232  | 221  | 243  | 229  | 249  | 176  | 171  | 164  | 183  | 144  | 0    | 0    | 0    | 0    | 0    | 0    |      |
| NP1               | 605899            | 501004 | 3529211 | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 76   | 63   | 56   | 52   | 32   | 32   | 35   | 41   | 39   | 24   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| NP2               | 624028            | 500929 | 3519541 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 1    | 1    | 1    | 2    | 4    | 0    | 6    | 0    | 4    | 6    |      |      |      |      |
| NP2               | 605898            | 500909 | 3520046 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 20   | 27   | 25   | 20   | 22   | 21   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |
| OcotilloCommunity | 801309            | 498963 | 3511412 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2    | 2    | 1    | 1    | 2    | 7    | 4    | 4    | 8    | 5    | 12   | 12   | 20   | 22   | 7    | 8    | 11   | 14   | 10   | 11   | 11   |      |      |
| Olivas            | 801154            | 503396 | 3531213 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 3    | 10   | 6    | 3    | 6    | 4    | 3    | 2    | 0    | 0    | 1    | 0    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    |      |      |      |      |
| P1                | 611138            | 503152 | 3540091 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 48   | 48   | 7    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |
| PDSI              | 611140            | 503554 | 3539692 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| PDSI              | 611745            | 503553 | 3540095 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| Poole             | 801975            | 495659 | 3519508 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 1    | 2    | 3    | 2    | 2    | 1    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 0    |      |      |      |      |      |      |
| QCWC_No13         | 608522            | 504788 | 3528380 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |      |
| RchoSah_WC        | 611144            | 502752 | 3537471 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |      |
| RT1               | 504946            | 499811 | 3530971 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 539  | 1688 | 2232 | 2294 | 58   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 796  | 1609 | 1748 | 1716 | 1610 | 1092 | 1495 | 1091 | 1069 | 0    | 0    | 0    |      |
| S1                | 623111            | 499931 | 3518793 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1232 | 947  | 1683 | 1566 | 1332 | 1446 | 862  | 1663 | 1038 | 787  | 1704 | 1002 | 1408 | 1776 | 668  | 748  | 1583 | 1350 | 964  | 1740 | 1164 | 1883 | 1443 |
| S12               | 623981            | 505183 | 3535660 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 661  | 805  | 891  | 706  | 637  | 722  | 712  | 661  | 686  | 579  | 620  | 590  | 677  | 591  | 536  | 642  | 664  | 639  | 624  | 580  | 603  | 780  | 871  |      |      |
| S19               | 623982            | 504841 | 3532023 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 642  | 1077 | 1113 | 797  | 657  | 877  | 847  | 867  | 758  | 855  | 659  | 866  | 842  | 660  | 786  | 772  | 736  | 795  | 832  | 915  | 847  | 938  |      |      |      |
| S2                | 623112            | 499133 | 3517459 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2145 | 2025 | 1072 | 271  | 2028 | 1674 | 1851 | 2329 | 1267 | 2425 | 1914 | 2158 | 2569 | 1973 | 892  | 608  | 1288 | 1210 | 600  | 1672 | 1327 | 1409 | 1172 |      |
| S22               | 623983            | 503660 | 3531621 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 432  | 434  | 458  | 308  | 277  | 273  | 270  | 351  | 322  | 501  | 404  | 351  | 302  | 288  | 221  | 76   | 305  | 319  | 262  | 374  | 448  | 388  | 466  |      |
| S25               | 623985            | 503037 | 3533248 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 519  | 815  | 906  | 810  | 880  | 873  | 785  | 880  | 205  | 818  | 808  | 754  | 778  | 705  | 683  | 875  | 750  | 777  | 700  | 828  | 944  |      |      |      |      |

**APPENDIX I.2**

**MEASURED AND SIMULATED HYDROGRAPHS AT SELECT WELLS**

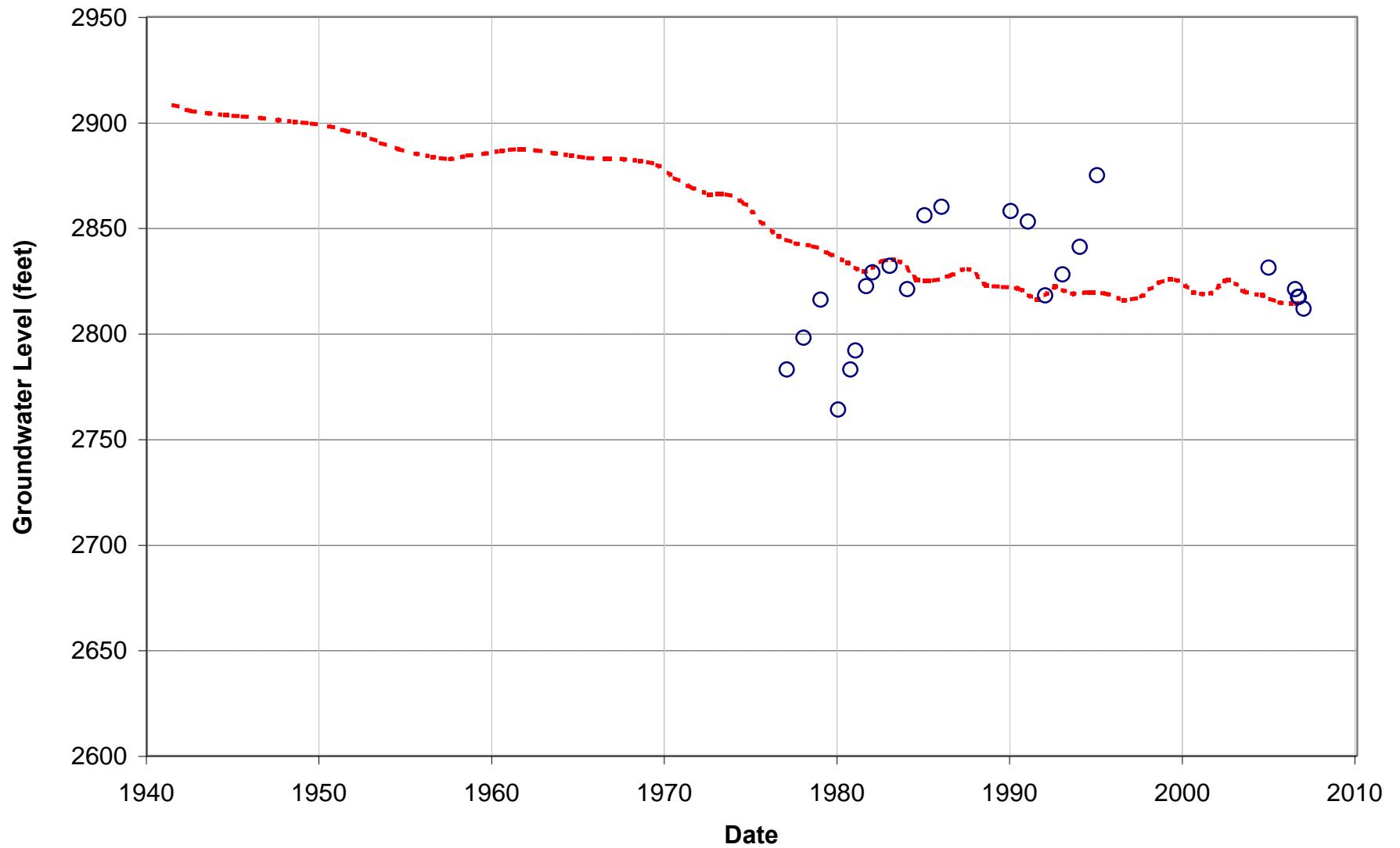


○ S-1 meas  
- - - S-1 sim



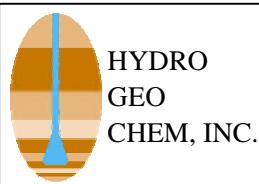
**Simulated and Measured  
Groundwater Levels at Well S-1**

APPROVED NWH DATE 11/20/2007 FIGURE I.2.1



○ S-2 meas

- - - S-2 sim



**Simulated and Measured  
Groundwater Levels at Well S-2**

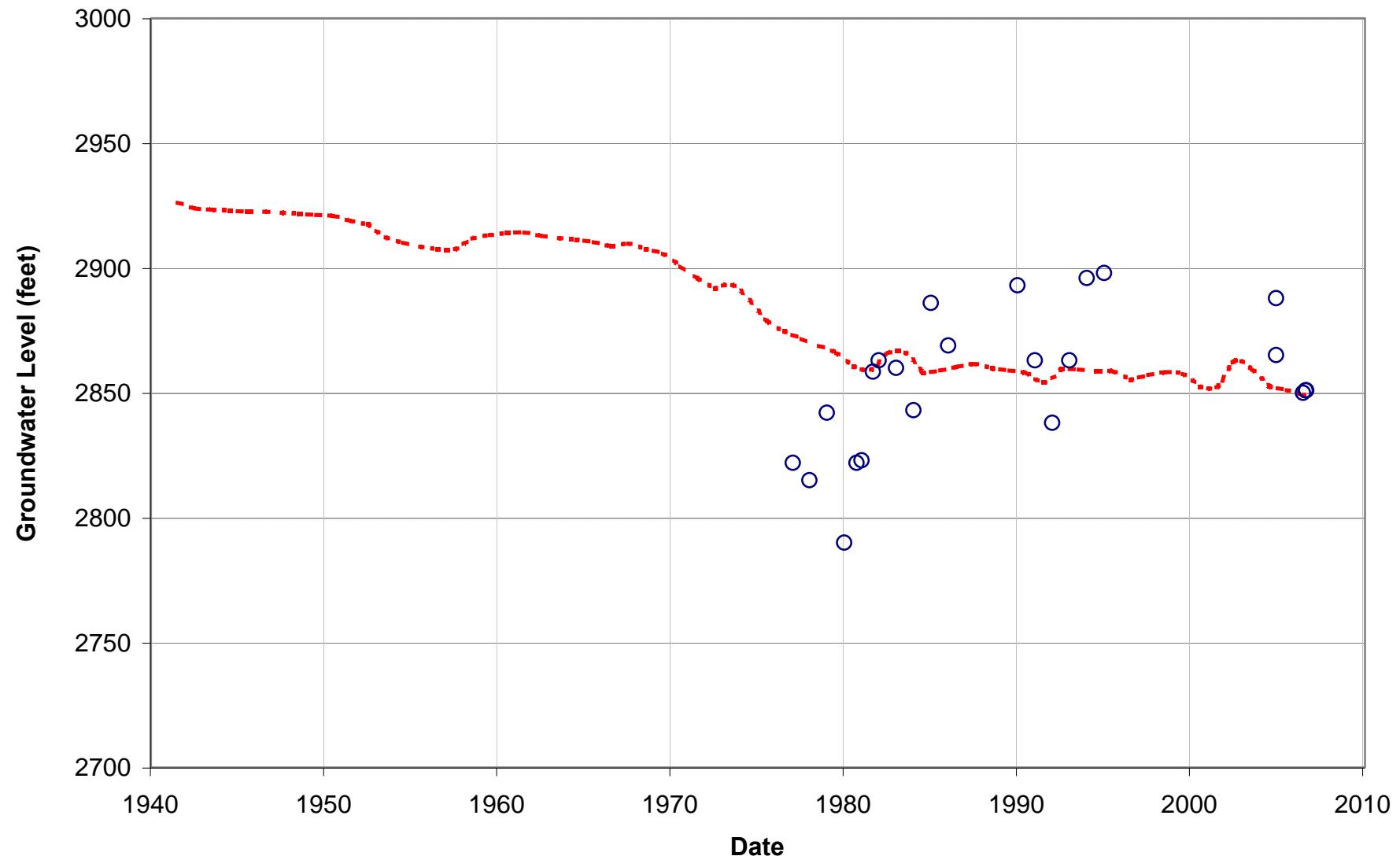
APPROVED

NWH

DATE  
11/20/2007

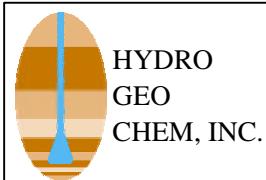
FIGURE

**I.2.2**



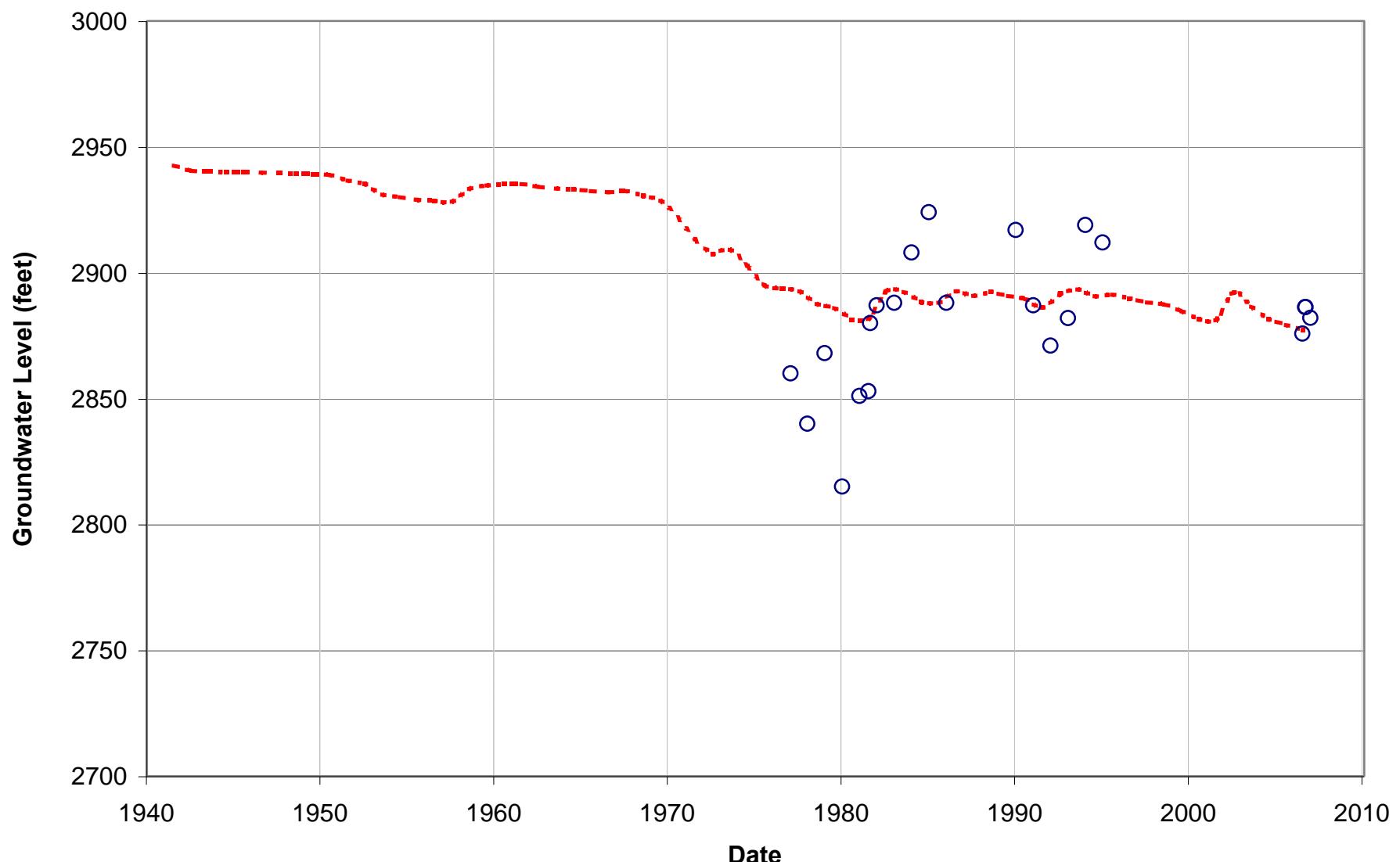
○ S-3 meas

- - - S-3 sim



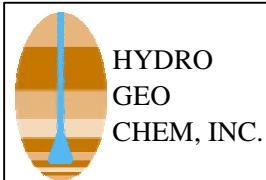
**Simulated and Measured  
Groundwater Levels at Well S-3**

APPROVED NWH DATE 11/20/2007 FIGURE I.2.3



○ S-4 meas

- - - S-4 sim



**Simulated and Observed  
Groundwater Levels at Well S-4**

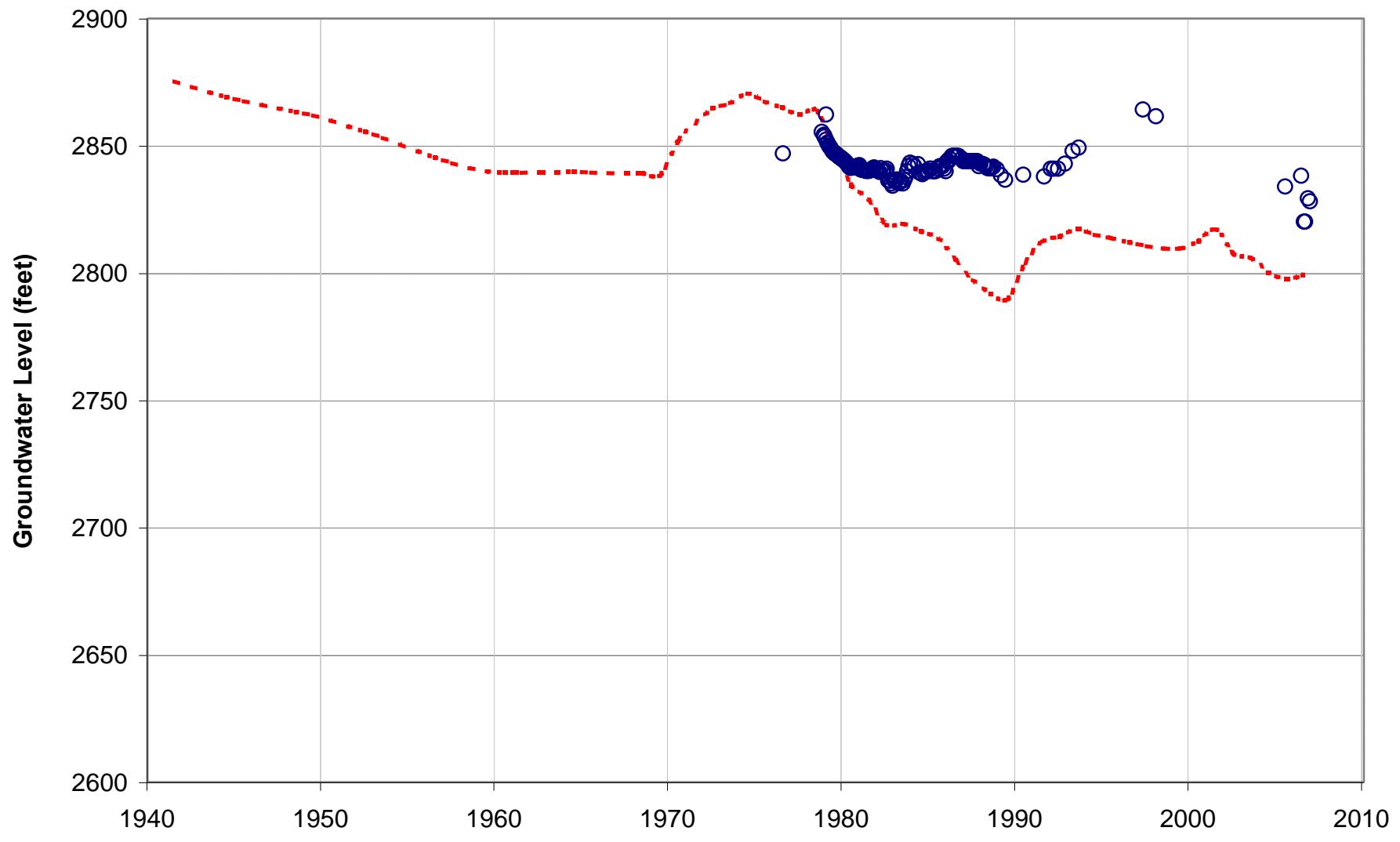
APPROVED

NWH

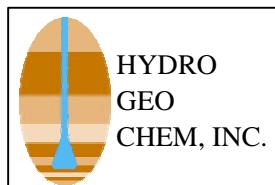
DATE 11/20/2007

FIGURE

**I.2.4**



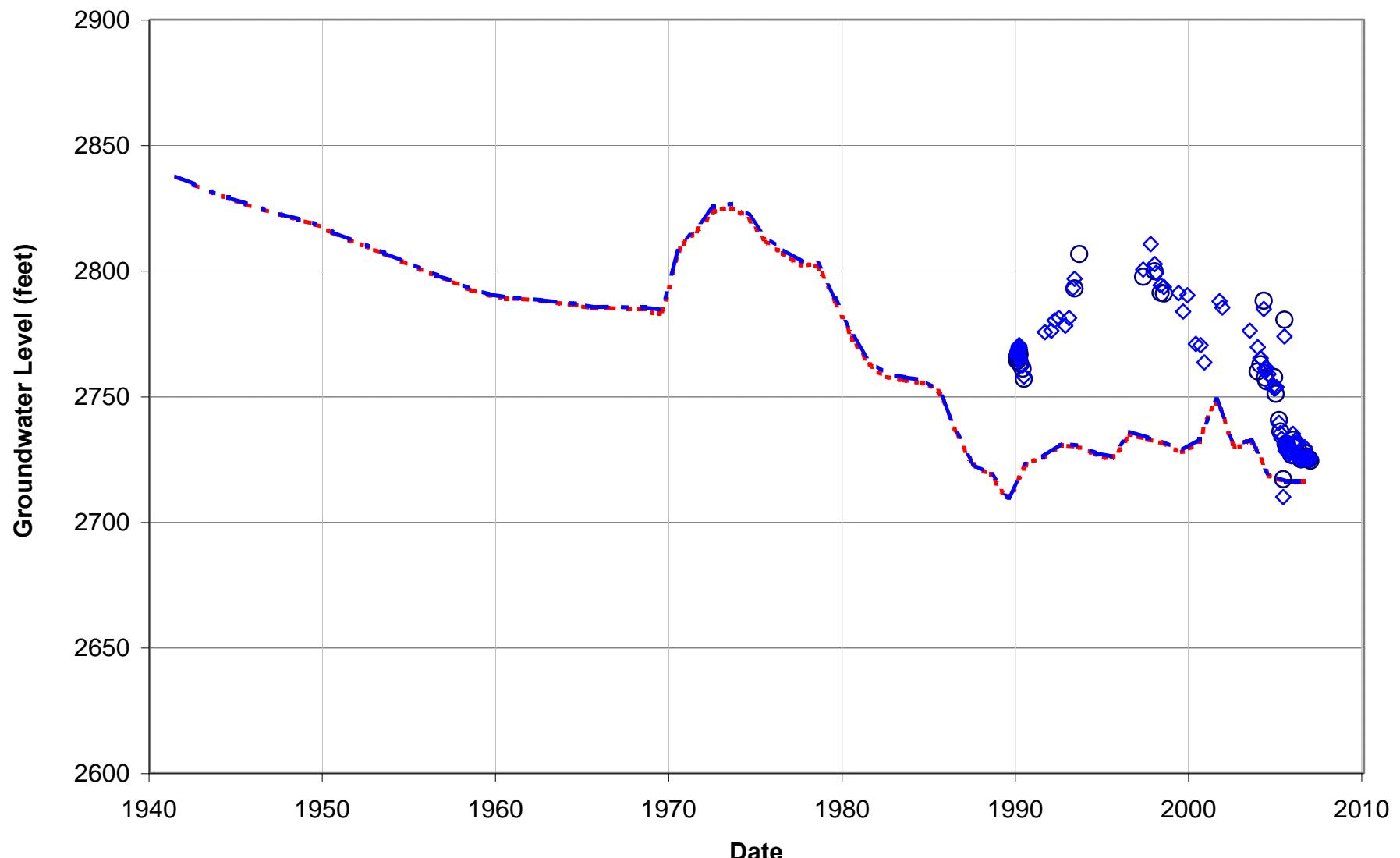
- MH-10 meas
- - MH-10 sim



### Simulated and Measured Groundwater Levels at Well MH-10

|          |     |      |            |        |
|----------|-----|------|------------|--------|
| APPROVED | NWH | DATE | 11/20/2007 | FIGURE |
|----------|-----|------|------------|--------|

**I.2.5**

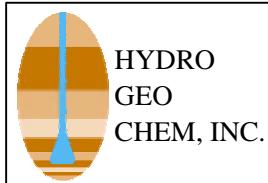


○ MH-15E meas

◇ MH-15W meas

- - - MH-15E sim

- - - MH-15W sim

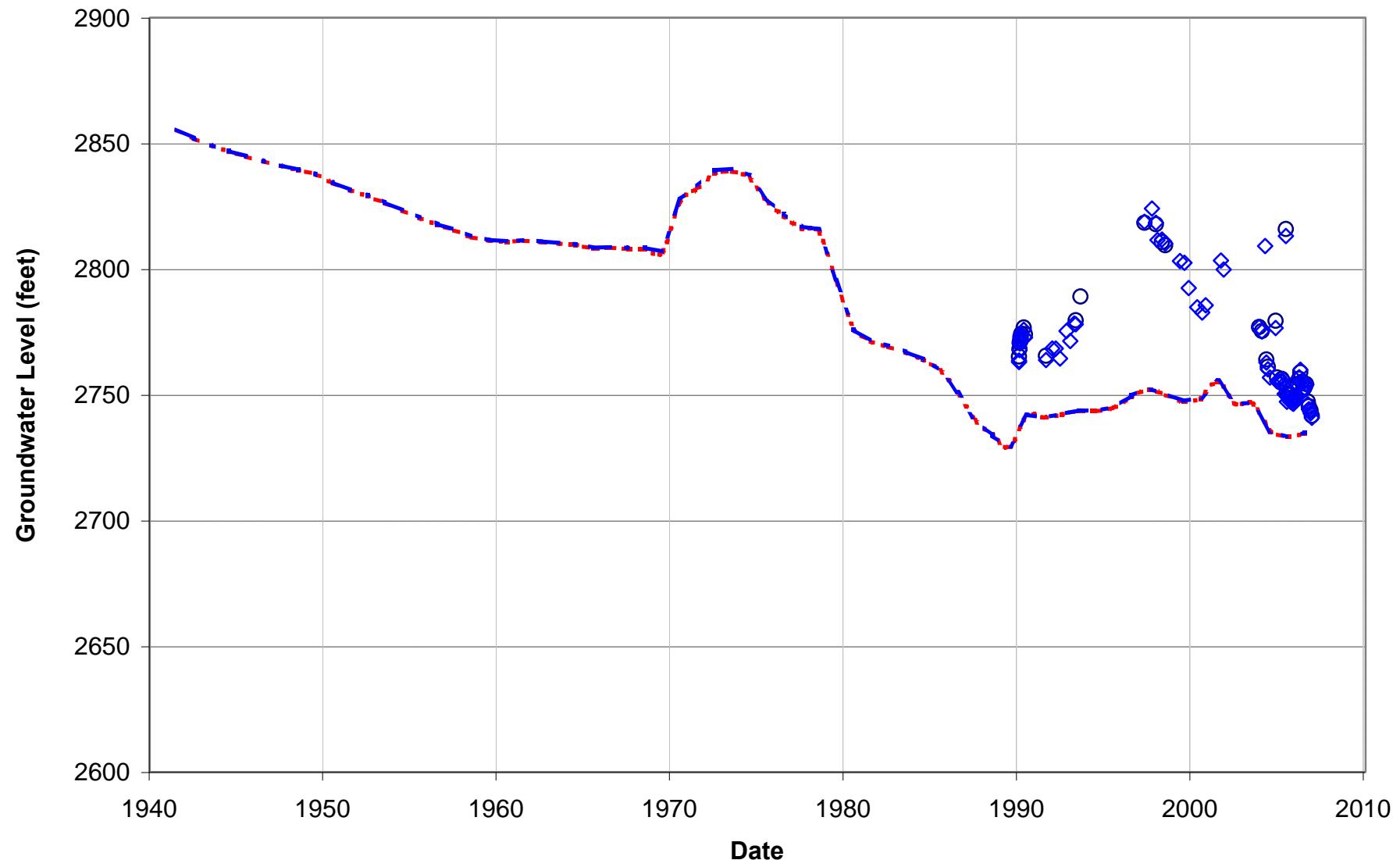


### Simulated and Measured Groundwater Levels at Wells MH-15E and MH-15W

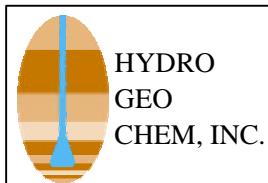
APPROVED NWH DATE 11/20/2007

FIGURE

I.2.6

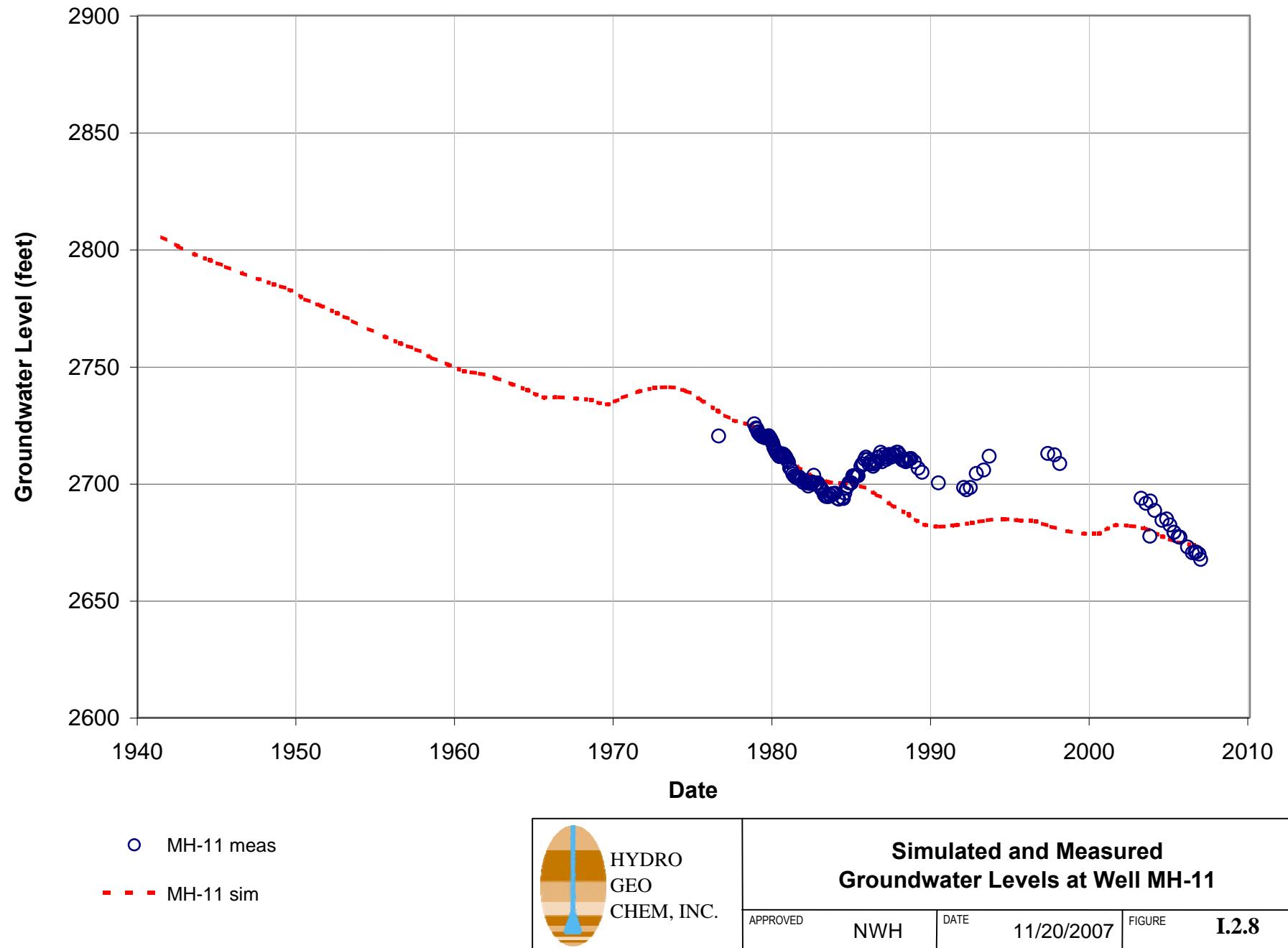


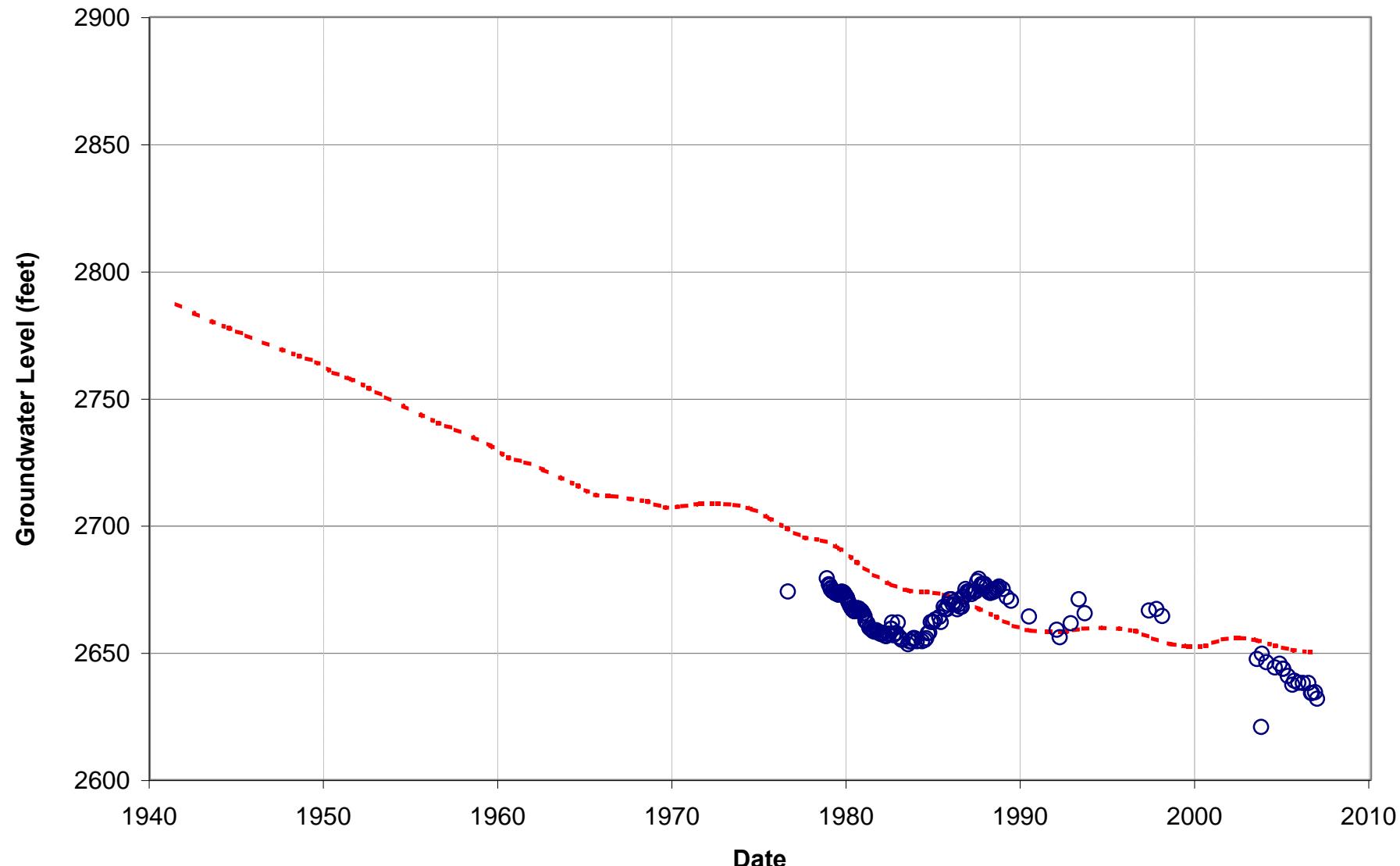
○ MH-16E meas      ◊ MH-16W meas  
- - - MH-16E sim      - - - MH-16W sim



### Simulated and Measured Groundwater Levels at Wells MH-16E and MH-16W

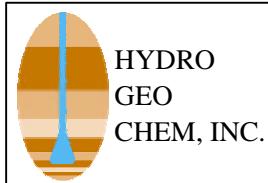
|          |     |      |            |        |       |
|----------|-----|------|------------|--------|-------|
| APPROVED | NWH | DATE | 11/20/2007 | FIGURE | I.2.7 |
|----------|-----|------|------------|--------|-------|





○ MH-12 meas

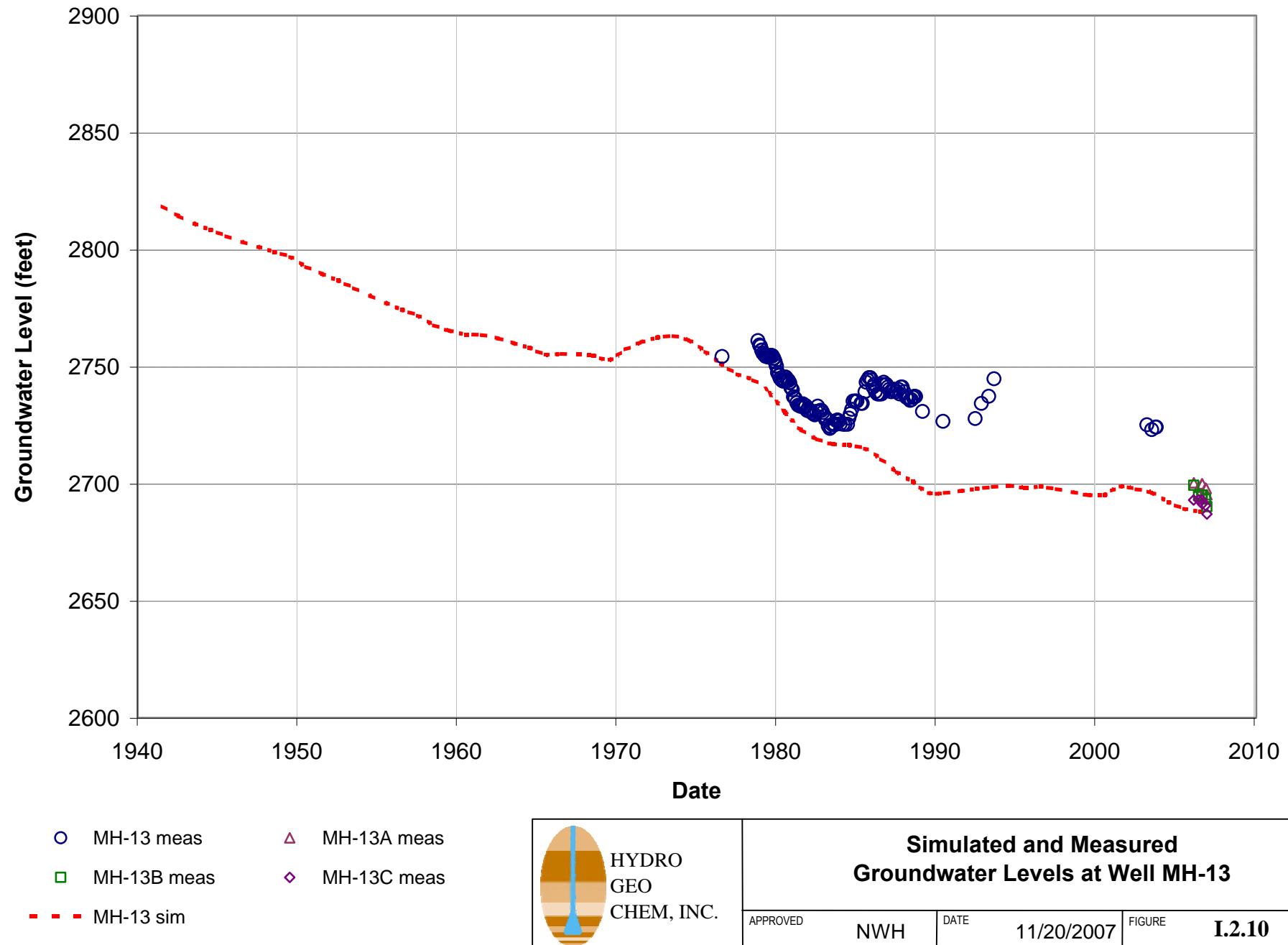
- - MH-12 sim

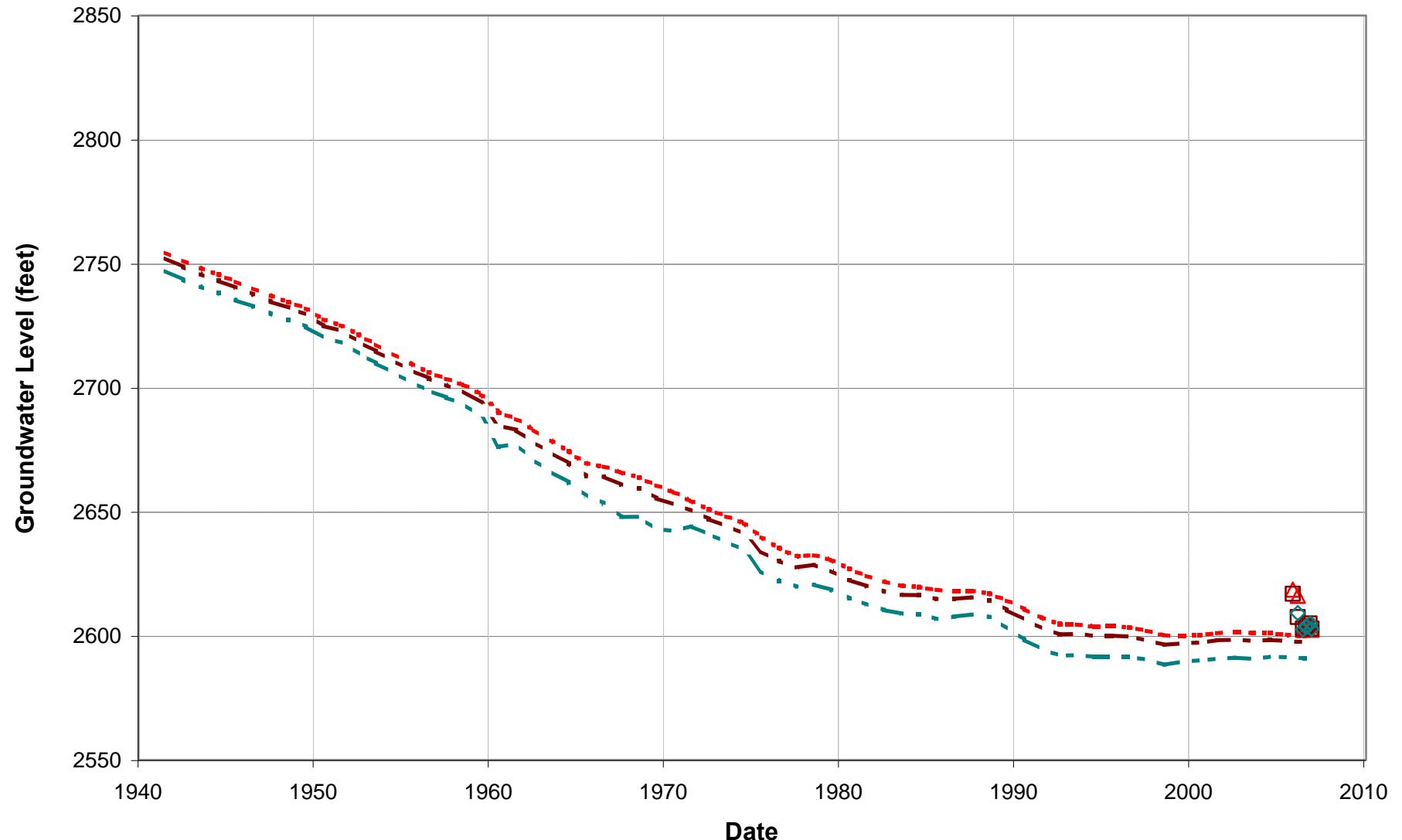


### Simulated and Measured Groundwater Levels at Well MH-12

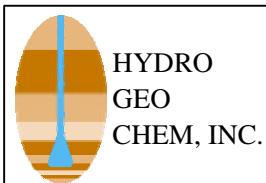
APPROVED NWH DATE 11/20/2007 FIGURE

I.2.9



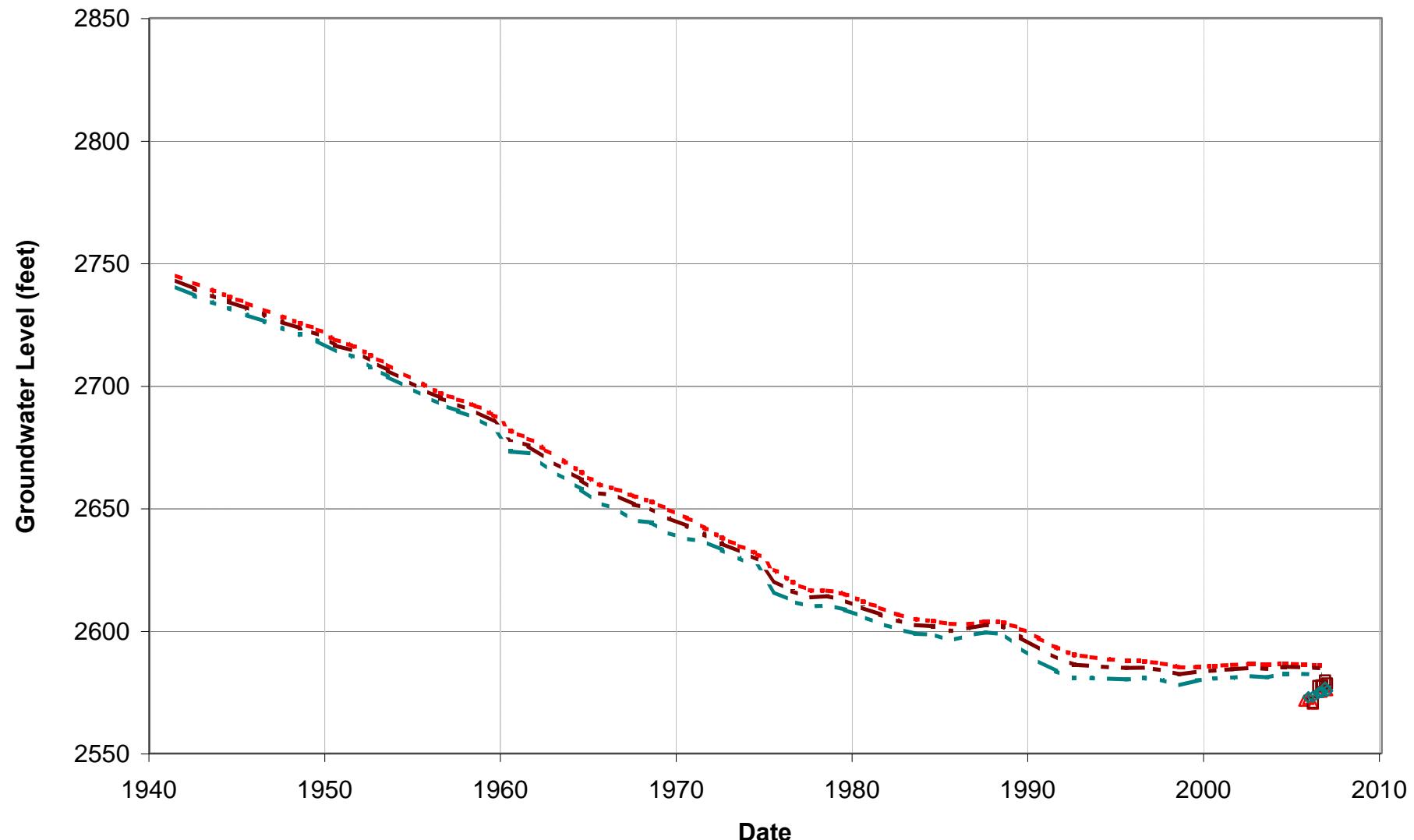


△ MH-25A meas      □ MH-25B meas  
◆ MH-25C meas      - - - MH-25A sim  
— MH-25B sim      — MH-25C sim

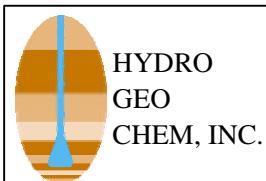


### Simulated and Measured Groundwater Levels at Well Nest MH-25

APPROVED      NWH      DATE      11/20/2007      FIGURE      I.2.11



▲ MH-26A meas      □ MH-26B meas  
 ◆ MH-26C meas      - - - MH-26A sim  
 — MH-26B sim      - - - MH-26C sim



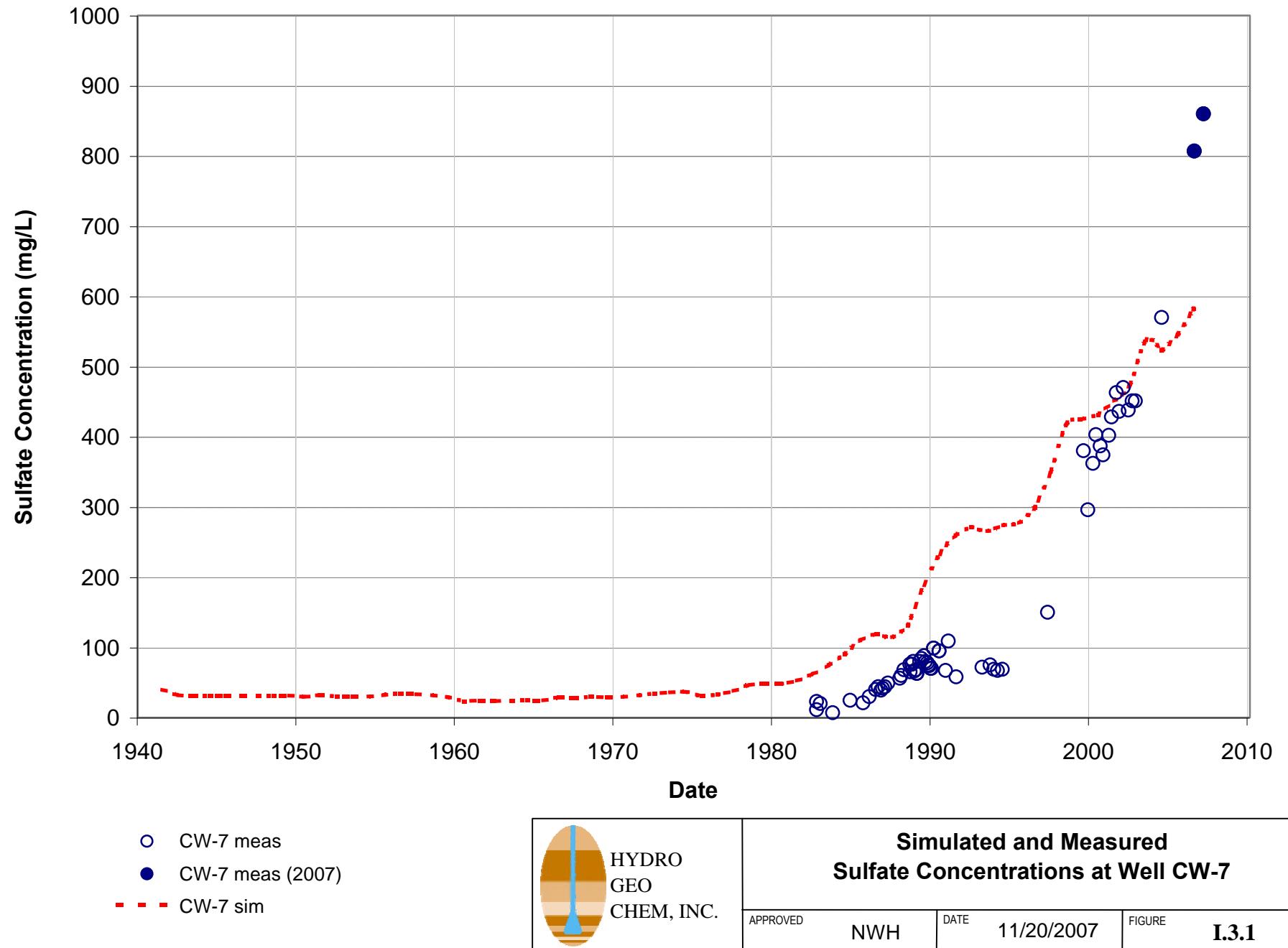
### Simulated and Measured Groundwater Levels at Well Nest MH-26

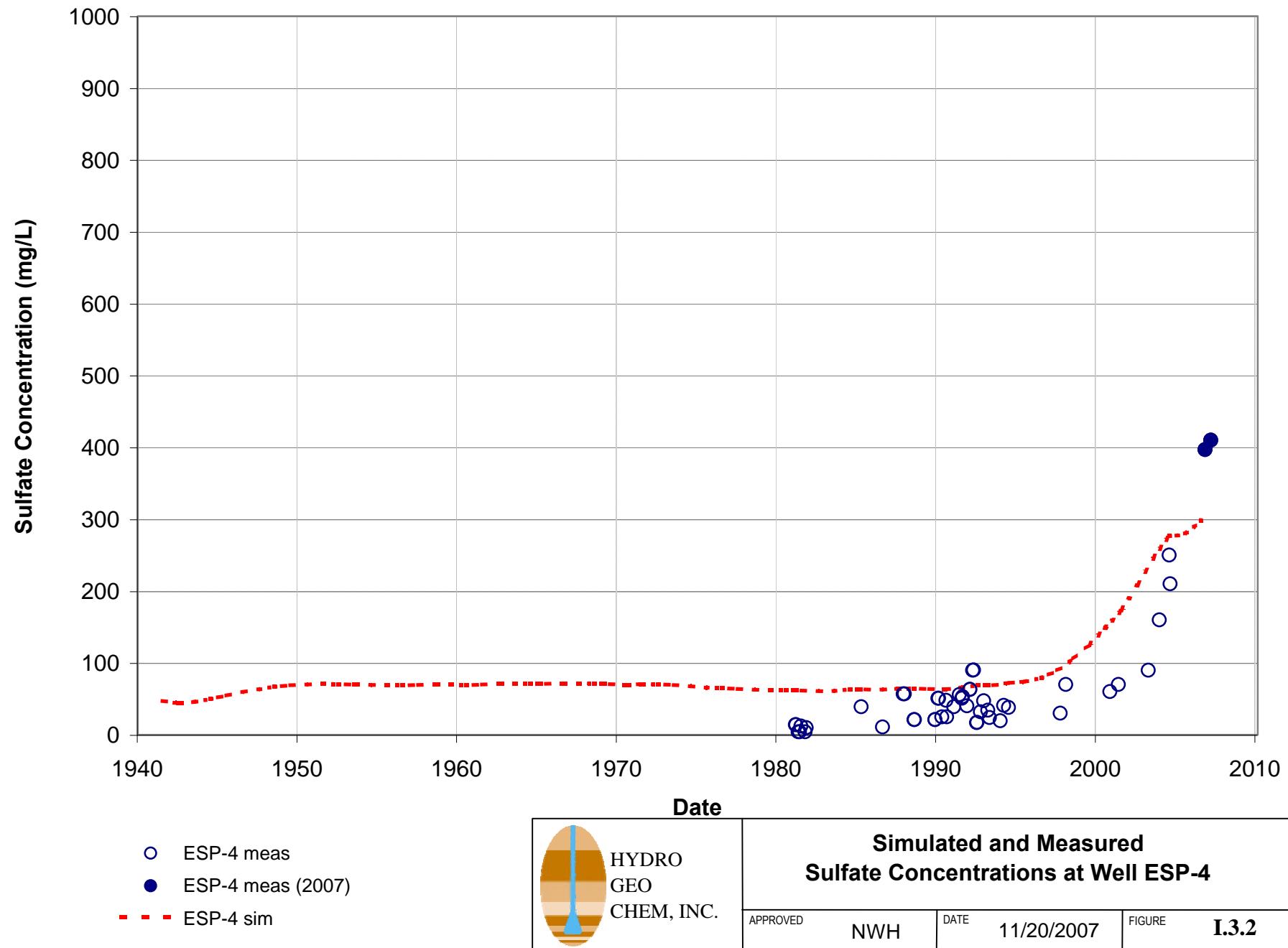
APPROVED NWH DATE 11/20/2007 FIGURE

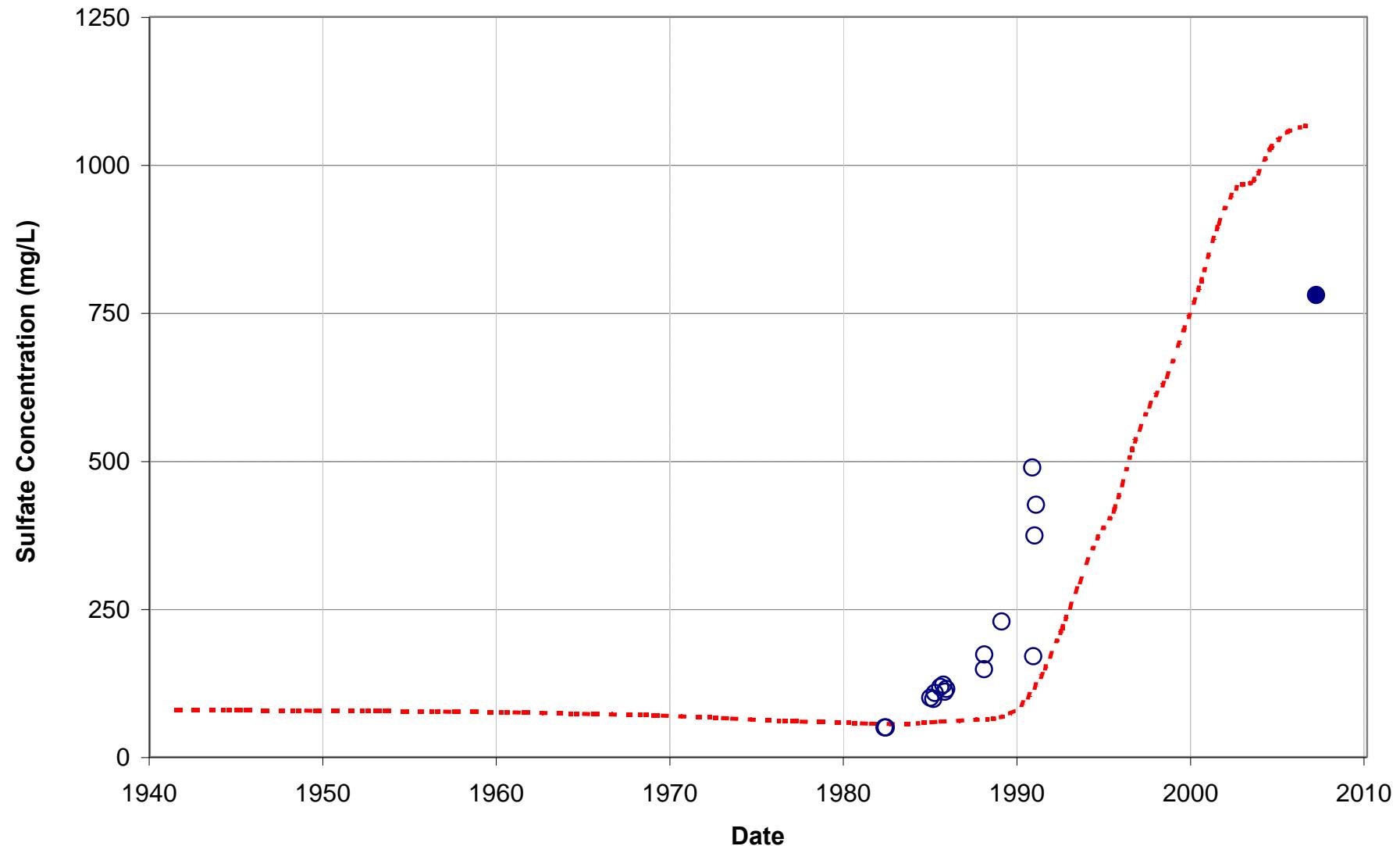
**I.2.12**

### **APPENDIX I.3**

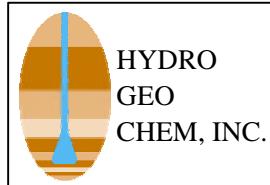
#### **MEASURED AND SIMULATED CHEMOGRAPHS AT SELECT WELLS**





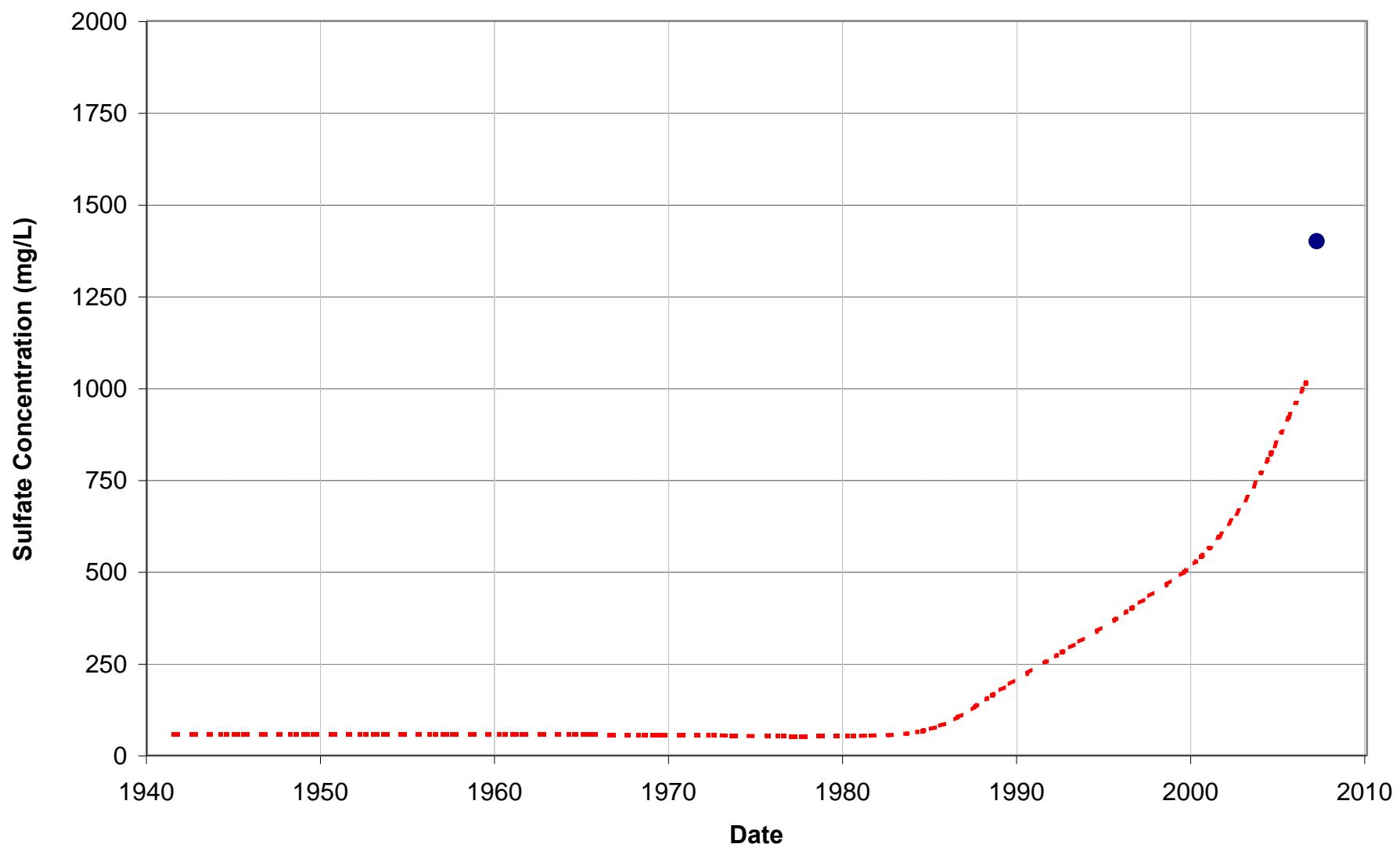


- I-12 meas
- I-12 meas (2007)
- - - I-12 sim



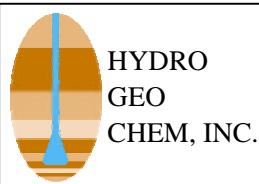
**Simulated and Measured  
Sulfate Concentrations at Well I-12**

APPROVED NWH DATE 11/20/2007 FIGURE I.3.3



● M-20 meas (2007)

- - - M-20 sim

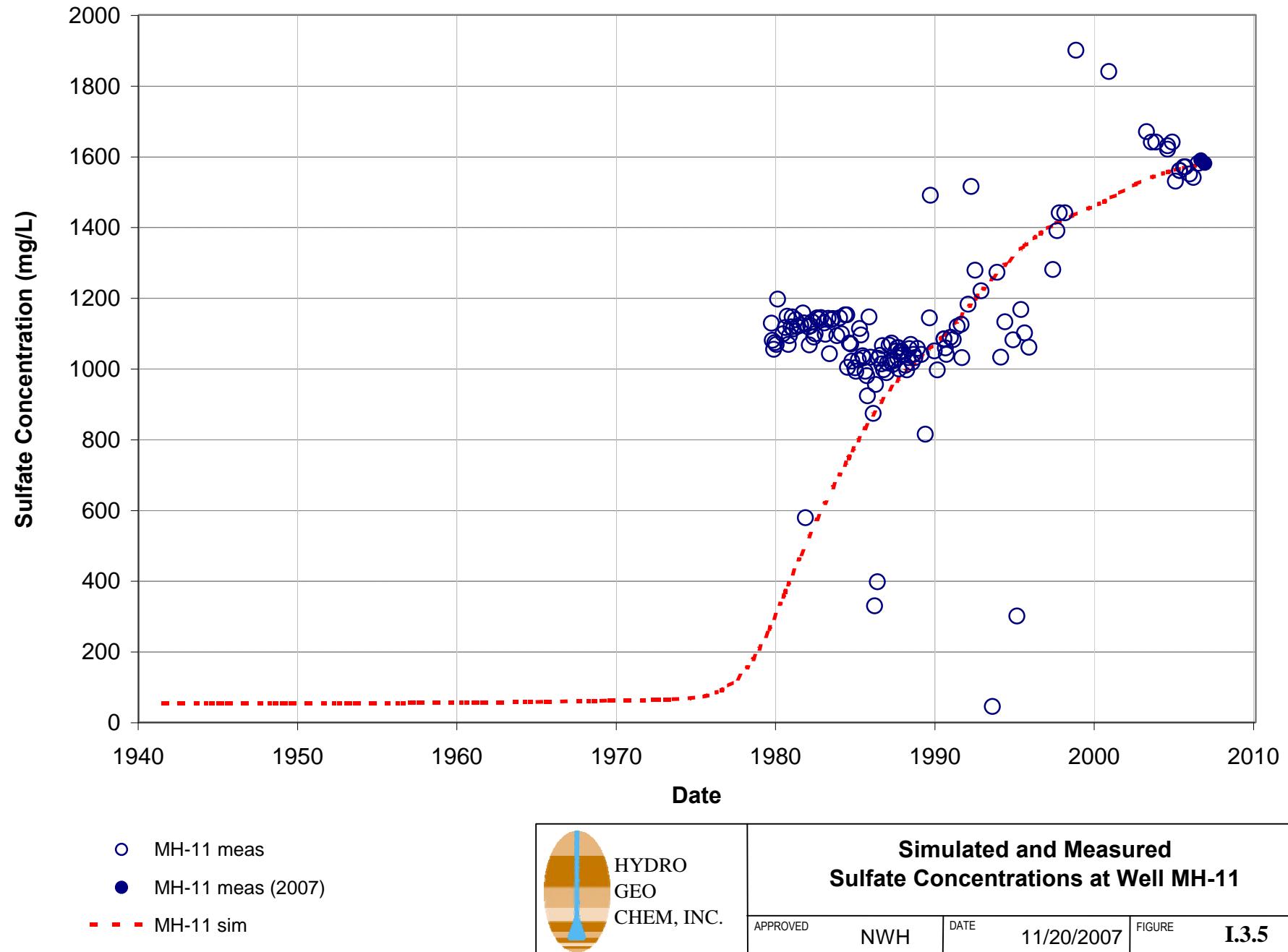


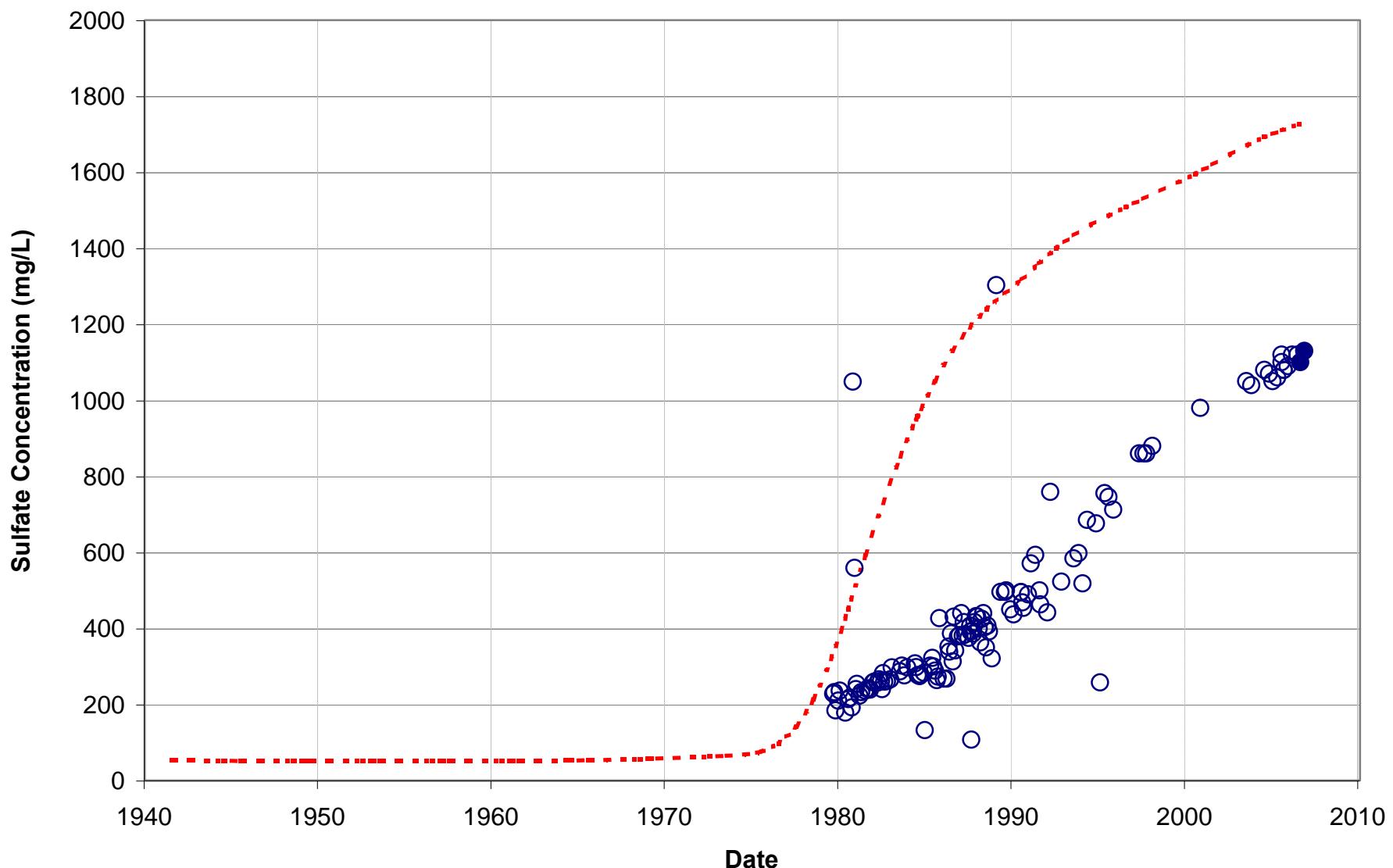
**Simulated and Measured  
Sulfate Concentrations at Well M-20**

APPROVED NWH DATE 11/20/2007

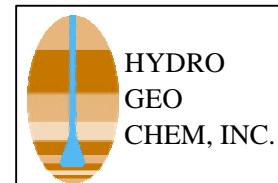
FIGURE

I.3.4





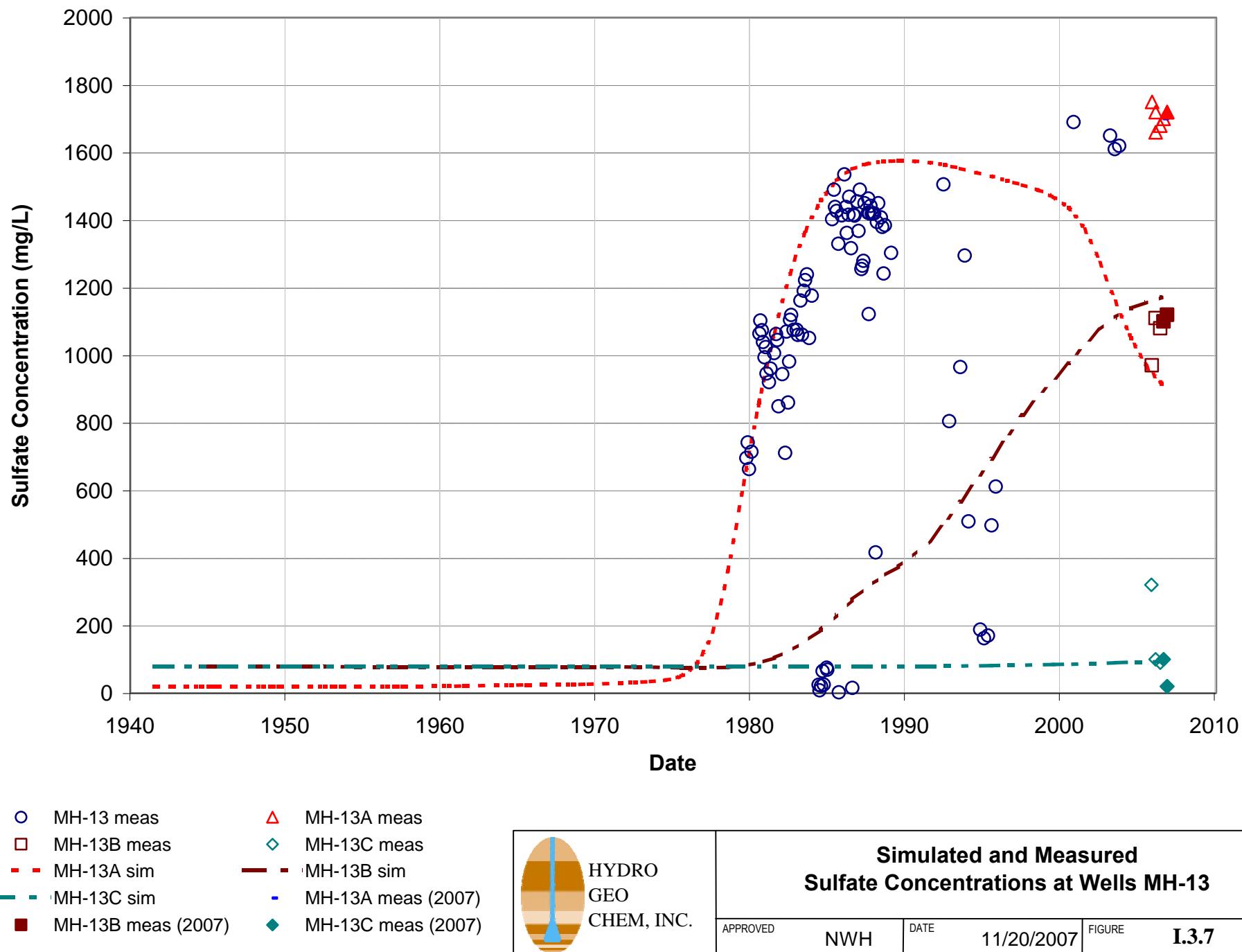
- MH-12 meas
- MH-12 meas (2007)
- - MH-12 sim



### Simulated and Measured Sulfate Concentrations at Well MH-12

APPROVED NWH DATE 11/20/2007 FIGURE

I.3.6



**APPENDIX I.1**

**WELL LOCATIONS AND PUMPING RATES**

**TABLE I.1.1**  
**Well Locations and Pumping Rates for**  
**Steady-State (1940) Simulation**

| UTM83E | UTM83N  | Pumping Rate<br>(gpm) |
|--------|---------|-----------------------|
| 496051 | 3511005 | 15                    |
| 496051 | 3511810 | 15                    |
| 496051 | 3512615 | 15                    |
| 496855 | 3511005 | 15                    |
| 496855 | 3511810 | 15                    |
| 496855 | 3512615 | 15                    |
| 497660 | 3515029 | 15                    |
| 497660 | 3515833 | 15                    |
| 498465 | 3515029 | 15                    |
| 498465 | 3515833 | 15                    |
| 500879 | 3519857 | 68                    |
| 500879 | 3522271 | 155                   |
| 500879 | 3523075 | 316                   |
| 500879 | 3524685 | 93                    |
| 500879 | 3525489 | 93                    |
| 500879 | 3526294 | 78                    |
| 500879 | 3527099 | 62                    |
| 500879 | 3530318 | 16                    |
| 501683 | 3522271 | 155                   |
| 501683 | 3524685 | 93                    |
| 501683 | 3525489 | 93                    |
| 501683 | 3526294 | 78                    |
| 501683 | 3527099 | 78                    |
| 501683 | 3529513 | 16                    |
| 501683 | 3530318 | 16                    |
| 502488 | 3524685 | 78                    |
| 502488 | 3525489 | 78                    |
| 502488 | 3526294 | 78                    |
| 502488 | 3527099 | 78                    |
| 502488 | 3527904 | 101                   |
| 502488 | 3528686 | 101                   |
| 502488 | 3542388 | 62                    |
| 502415 | 3543192 | 62                    |
| 503293 | 3524685 | 78                    |
| 503293 | 3525489 | 78                    |
| 503270 | 3526294 | 78                    |
| 503293 | 3527099 | 78                    |
| 503293 | 3527904 | 101                   |

**TABLE I.1.1**  
**Well Locations and Pumping Rates for**  
**Steady-State (1940) Simulation**

| UTM83E | UTM83N  | Pumping Rate<br>(gpm) |
|--------|---------|-----------------------|
| 503293 | 3528708 | 101                   |
| 503293 | 3542388 | 62                    |
| 503293 | 3543192 | 62                    |
| 504097 | 3529513 | 93                    |
| 504097 | 3530318 | 93                    |
| 504097 | 3531927 | 868                   |
| 504097 | 3532732 | 336                   |
| 504074 | 3535950 | 310                   |
| 504097 | 3537560 | 139                   |
| 504097 | 3538364 | 279                   |
| 504097 | 3539169 | 174                   |
| 504097 | 3539974 | 174                   |
| 504097 | 3542388 | 62                    |
| 504097 | 3543192 | 62                    |
| 504902 | 3529513 | 93                    |
| 504902 | 3530318 | 93                    |
| 504902 | 3533536 | 336                   |
| 504902 | 3535146 | 310                   |
| 504902 | 3537560 | 139                   |
| 504902 | 3539169 | 174                   |
| 504902 | 3539974 | 174                   |
| 504902 | 3542388 | 62                    |
| 504902 | 3543192 | 62                    |
| 505707 | 3536755 | 558                   |
| 505707 | 3537560 | 78                    |
| 505707 | 3538364 | 78                    |
| 506511 | 3537560 | 78                    |
| 506511 | 3538364 | 78                    |

*Notes:*

*Well locations and pumping rates from ADWR Model (Mason and Bota, 2006)*

*UTM83E = Universal Transverse Mercator, North American Datum 1983, East*

*UTM83N = Universal Transverse Mercator, North American Datum 1983, North*

*gpm = gallons per minute*

**TABLE I.1.2**

lications and Pumping Rates for  
Model (Mason and Bota, 2006)

**TABLE I.1.2**

### Well Locations and Pumping Rates for taken from ADWR Model (Mason and Bota, 2006)

*Universal Transverse Mercator, North American Datum 1983, East*

*Universal Transverse Mercator, North American Datum 1983, North*

*specified after 1983*

*gallons per minute (gpm)*

TABLE I.1.3

Well Locations and Pumping Rates for  
Transient Simulation, Taken from Various Sources<sup>a</sup>

| Well ID      | ADWR Registration | UTM83E | UTM83N  | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980  | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 |   |   |   |   |   |   |   |   |   |
|--------------|-------------------|--------|---------|------|------|------|------|------|------|------|------|------|-------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|---|---|---|---|---|---|---|---|---|
| 11caa        | 801179            | 501186 | 3526788 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 1    | 55   | 36   | 69   | 38   | 46   | 54   | 53   | 46   | 42   | 58   | 46   | 42   | 35   | 42   | 31   | 28   | 37   | 48   | 37   | 19   | 0    | 0    |      |      |   |   |   |   |   |   |   |   |   |
| 25cbd        | 634348            | 492757 | 3531386 | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23   | 23    | 23   | 22   | 18   | 16   | 15   | 19   | 1    | 12   | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| AN1          | 608518            | 502595 | 3527990 | 2325 | 2325 | 2325 | 2325 | 1131 | 1131 | 1131 | 1131 | 1131 | 1131  | 1266 | 1248 | 166  | 10   | 19   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |   |   |   |   |   |   |   |   |   |
| AN-2(RRQC2)  | 608519            | 503457 | 3529250 | 1548 | 1548 | 1548 | 1548 | 1131 | 1131 | 1131 | 1131 | 1131 | 1131  | 1189 | 1221 | 126  | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 5    | 5    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |   |   |   |   |   |   |   |   |   |
| AN-4(RRQC1)  | 608521            | 503457 | 3527990 | 0    | 0    | 0    | 0    | 0    | 0    | 1131 | 1131 | 1131 | 1131  | 1131 | 1279 | 664  | 58   | 69   | 60   | 3    | 0    | 0    | 0    | 0    | 0    | 94   | 156  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |   |   |   |   |   |   |   |   |   |
| C1           | 624008            | 503353 | 3529320 | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50   | 50    | 47   | 39   | 35   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |   |   |   |   |   |   |   |   |   |
| C4           | 624010            | 501760 | 3525384 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 1332 | 13247 | 1033 | 922  | 854  | 823  | 1160 | 932  | 710  | 783  | 756  | 922  | 911  | 852  | 833  | 1167 | 817  | 987  | 840  | 914  | 888  | 757  | 794  | 808  | 908  | 921  | 1113 |      |   |   |   |   |   |   |   |   |   |
| CcofGV       | 501760            | 501635 | 3527876 | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 484  | 484   | 453  | 376  | 335  | 311  | 280  | 375  | 336  | 389  | 324  | 396  | 379  | 364  | 388  | 440  | 453  | 408  | 378  | 377  | 353  | 340  | 393  | 371  | 289  | 117  | 54   |      |   |   |   |   |   |   |   |   |   |
| CEMEX        | 607815            | 505129 | 3540303 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| Colgate      | 639904            | 509408 | 3532606 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| ContSD39     | 601769            | 504049 | 3522942 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| Cox          | 604432            | 508795 | 3534015 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 4    | 2    | 2    | 3    | 2    | 0    | 2    | 2    | 7    | 3    | 3    | 2    | 3    | 4    | 3    | 2    | 2    | 2    | 2    | 2    |      |      |      |   |   |   |   |   |   |   |   |   |
| Cox          | 627079            | 508795 | 3534015 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| CSD39        | 638581            | 504049 | 3522942 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |   |   |   |   |   |   |   |   |   |
| CW3          | 627483            | 500048 | 3523810 | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 137  | 137   | 212  | 175  | 157  | 145  | 142  | 5    | 0    | 1    | 0    | 0    | 0    | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 |   |   |   |   |   |   |   |   |
| CW5          | 627484            | 501234 | 3522497 | 0    | 0    | 0    | 0    | 187  | 187  | 187  | 187  | 187  | 187   | 175  | 145  | 129  | 120  | 275  | 223  | 269  | 284  | 293  | 224  | 268  | 287  | 254  | 290  | 316  | 309  | 199  | 139  | 131  | 89   | 85   | 105  | 0    | 0    | 0    | 0    | 0 | 0 |   |   |   |   |   |   |   |
| CW6          | 627485            | 500891 | 3525794 | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420  | 420   | 393  | 326  | 291  | 269  | 276  | 404  | 353  | 348  | 319  | 366  | 311  | 352  | 336  | 388  | 439  | 248  | 371  | 342  | 103  | 326  | 401  | 418  | 221  | 295  | 252  | 183  | 0 | 0 |   |   |   |   |   |   |   |
| CW7          | 502546            | 499660 | 3528094 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 511  | 456  | 423  | 285  | 408  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 | 0 |   |   |   |
| CW8          | 543600            | 499799 | 3525661 | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300  | 300   | 300  | 300  | 300  | 300  | 300  | 300  | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 9    | 428  | 453  | 517  | 623  | 677  | 527  | 723  | 713  | 426  | 1    | 1    |   |   |   |   |   |   |   |   |   |
| CW9          | 588121            | 501072 | 3528741 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Davis_Robert | 516216            | 507647 | 3533428 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0     | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| E10A         | 086931            | 502452 | 3523995 | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 43   | 43    | 40   | 33   | 30   | 27   | 27   | 38   | 28   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0 | 0 | 0 | 0 | 0 | 0 |   |   |   |
| E11A         | 624018            | 502092 | 3527822 | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468  | 468   | 439  | 363  | 324  | 300  | 325  | 191  | 100  | 245  | 296  | 294  | 304  | 373  | 294  | 339  | 298  | 246  | 341  | 332  | 378  | 330  | 305  | 284  | 446  | 496  | 501  | 445  | 0 | 0 |   |   |   |   |   |   |   |
| E12          | 624019            | 500635 | 35203   |      |      |      |      |      |      |      |      |      |       |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |   |   |   |   |   |   |   |   |   |

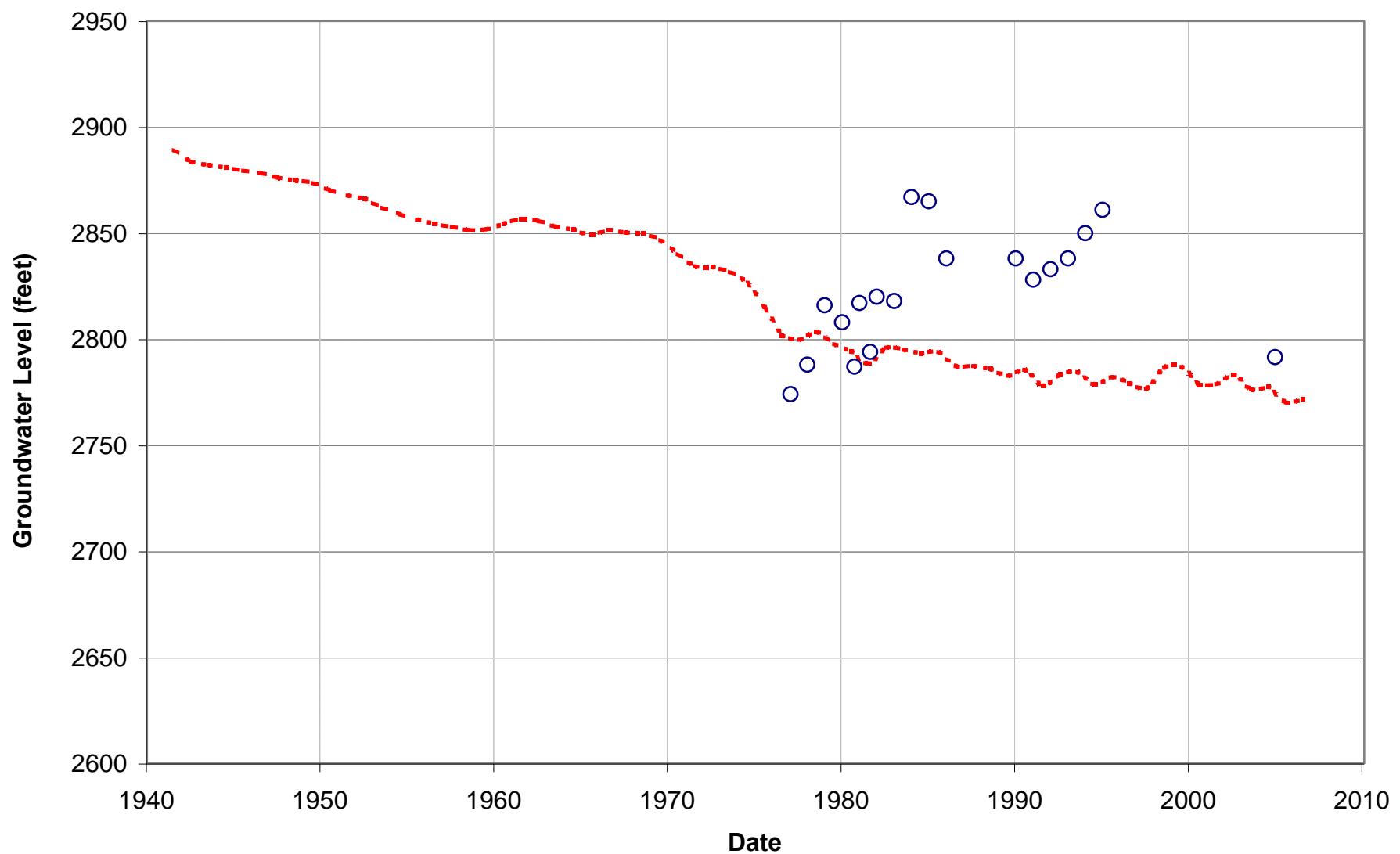
TABLE I.1.3

Well Locations and Pumping Rates for  
Transient Simulation, Taken from Various Sources<sup>a</sup>

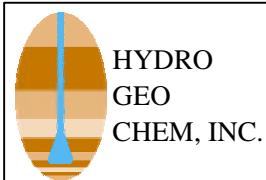
| Well ID           | ADWR Registration | UTM83E | UTM83N  | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 |      |      |
|-------------------|-------------------|--------|---------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| M13               | 611139            | 503350 | 3540498 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 107  | 521  | 611  | 507  | 703  | 608  | 726  | 643  | 590  | 759  | 790  | 452  | 257  | 487  | 241  | 724  |      |      |      |
| M14               | 532046            | 502554 | 3539883 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 19   | 473  | 533  | 833  | 911  | 645  | 849  | 648  | 922  | 799  | 659  | 361  | 307  | 409  | 293  | 717  |      |      |      |
| M6                | 607787            | 500542 | 3540494 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 517  | 671  | 673  | 926  | 781  | 872  | 378  | 346  | 434  | 176  | 84   | 137  | 241  | 346  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| M7                | 607788            | 500947 | 3540494 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 514  | 832  | 649  | 949  | 970  | 532  | 134  | 205  | 796  | 479  | 500  | 205  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| M8                | 607789            | 501351 | 3540493 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 524  | 125  | 801  | 878  | 660  | 471  | 794  | 753  | 576  | 568  | 593  | 614  | 510  | 417  | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |
| Madera_Highlands  | 624019            | 503285 | 3526162 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 93   | 101  | 132  | 96   | 60   | 59   | 184  | 191  | 232  | 221  | 243  | 229  | 249  | 176  | 171  | 164  | 183  | 144  | 0    | 0    | 0    | 0    | 0    | 0    |      |
| NP1               | 605899            | 501004 | 3529211 | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 81   | 76   | 63   | 56   | 52   | 32   | 32   | 35   | 41   | 39   | 24   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| NP2               | 624028            | 500929 | 3519541 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 1    | 1    | 1    | 2    | 4    | 0    | 6    | 0    | 4    | 6    |      |      |      |      |
| NP2               | 605898            | 500909 | 3520046 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 20   | 27   | 25   | 20   | 22   | 21   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |
| OcotilloCommunity | 801309            | 498963 | 3511412 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2    | 2    | 1    | 1    | 2    | 7    | 4    | 4    | 8    | 5    | 12   | 12   | 20   | 22   | 7    | 8    | 11   | 14   | 10   | 11   | 11   | 11   |      |
| Olivas            | 801154            | 503396 | 3531213 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 3    | 10   | 6    | 3    | 6    | 4    | 3    | 2    | 0    | 0    | 1    | 0    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    | 1    |      |      |
| P1                | 611138            | 503152 | 3540091 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 48   | 48   | 7    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |
| PDSI              | 611140            | 503554 | 3539692 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |
| PDSI              | 611745            | 503553 | 3540095 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |
| Poole             | 801975            | 495659 | 3519508 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1    | 1    | 2    | 3    | 2    | 2    | 1    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 2    | 0    |      |      |      |      |      |
| QCWC_No13         | 608522            | 504788 | 3528380 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| RchoSah_WC        | 611144            | 502752 | 3537471 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |      |      |      |
| RT1               | 504946            | 499811 | 3530971 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 539  | 1688 | 2232 | 2294 | 58   | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    |      |
| S1                | 623111            | 499931 | 3518793 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 1232 | 947  | 1683 | 1566 | 1332 | 1446 | 862  | 1663 | 1038 | 787  | 1704 | 1002 | 1408 | 1776 | 668  | 748  | 1583 | 1350 | 964  | 1740 | 1164 | 1883 | 1443 |
| S12               | 623981            | 505183 | 3535660 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 661  | 805  | 891  | 706  | 637  | 722  | 712  | 661  | 686  | 579  | 620  | 590  | 677  | 591  | 536  | 642  | 664  | 639  | 624  | 580  | 603  | 780  | 871  |
| S19               | 623982            | 504841 | 3532023 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 642  | 1077 | 1113 | 797  | 657  | 877  | 847  | 867  | 758  | 855  | 659  | 866  | 842  | 660  | 786  | 772  | 736  | 795  | 832  | 915  | 847  | 938  |      |
| S2                | 623112            | 499133 | 3517459 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2145 | 2025 | 1072 | 271  | 2028 | 1674 | 1851 | 2329 | 1267 | 2425 | 1914 | 2158 | 2569 | 1973 | 892  | 608  | 1288 | 1210 | 600  | 1672 | 1327 | 1409 | 1172 |
| S22               | 623983            | 503660 | 3531621 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 432  | 434  | 458  | 308  | 277  | 273  | 270  | 351  | 322  | 501  | 404  | 351  | 302  | 288  | 221  | 76   | 305  | 319  | 262  | 374  | 448  | 388  | 466  |
| S25               | 623985            | 503037 | 3533248 | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 519  | 815  | 906  | 810  | 880  | 873  | 785  | 880  | 205  | 818  | 808  |      |      |      |      |      |      |      |      |      |      |      |      |

**APPENDIX I.2**

**MEASURED AND SIMULATED HYDROGRAPHS AT SELECT WELLS**

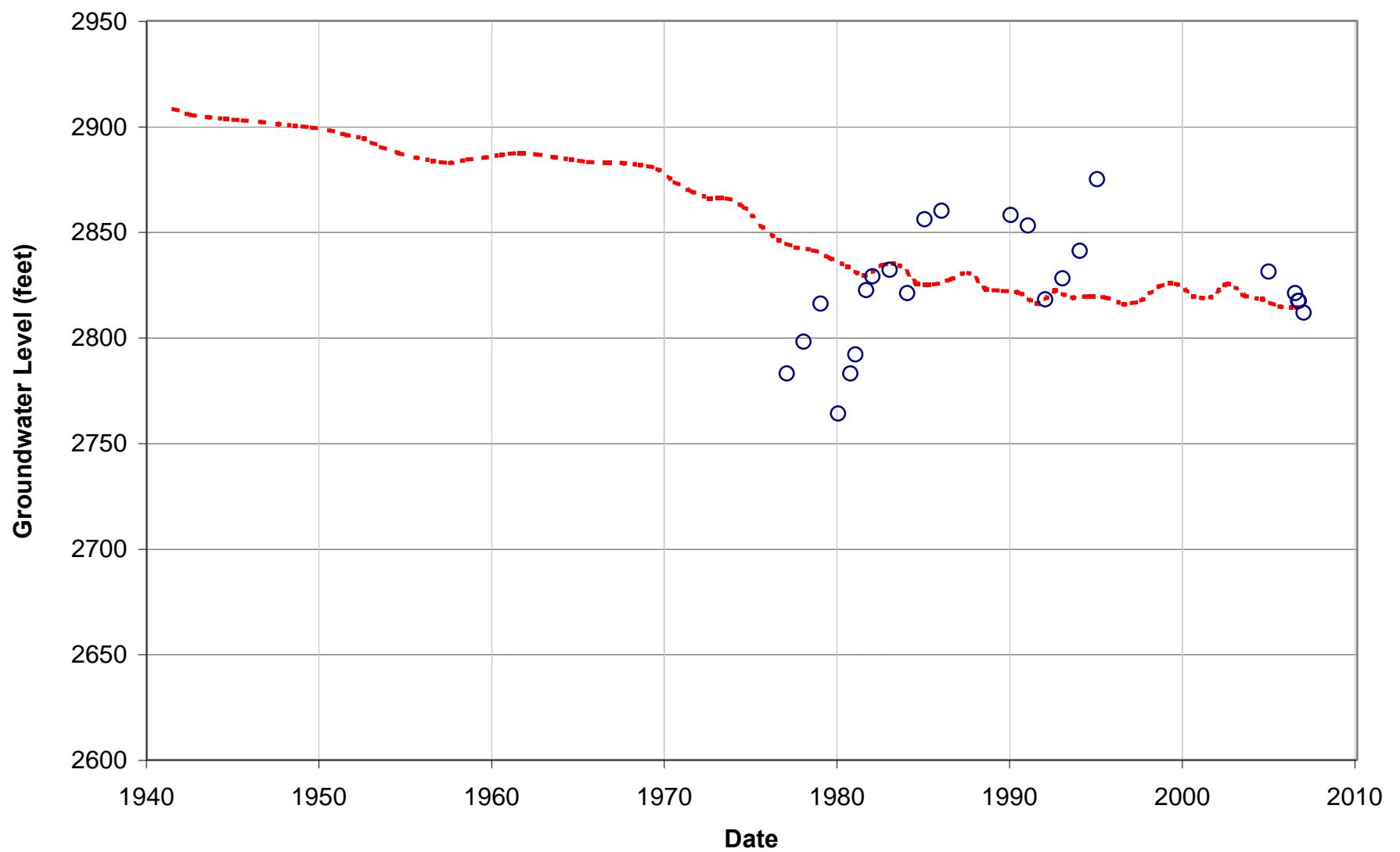


○ S-1 meas  
- - - S-1 sim



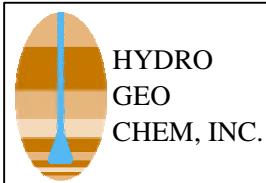
**Simulated and Measured  
Groundwater Levels at Well S-1**

APPROVED NWH DATE 11/20/2007 FIGURE I.2.1



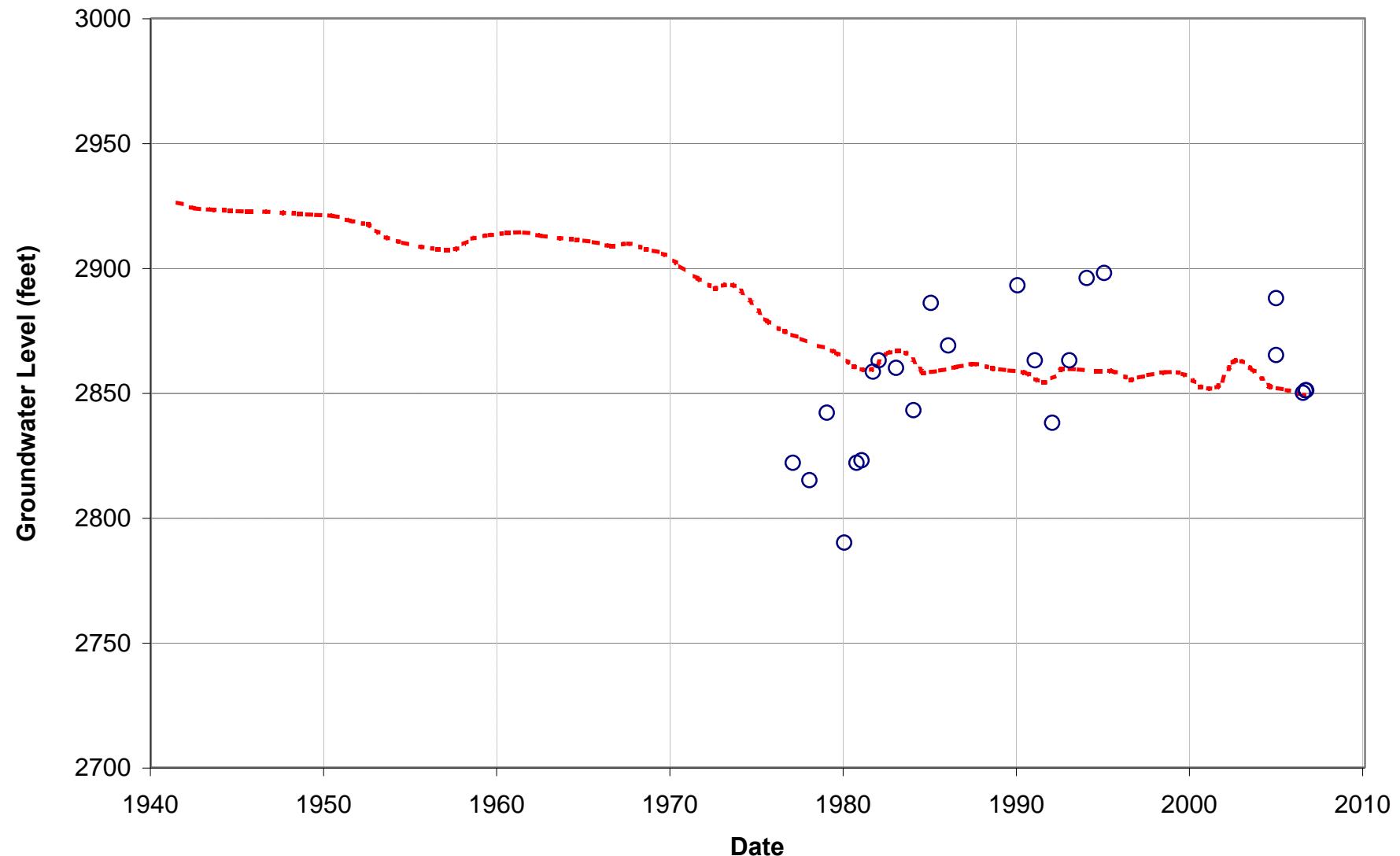
○ S-2 meas

- - - S-2 sim



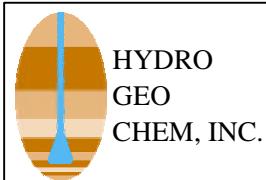
### Simulated and Measured Groundwater Levels at Well S-2

APPROVED NWH DATE 11/20/2007 FIGURE I.2.2



○ S-3 meas

- - - S-3 sim

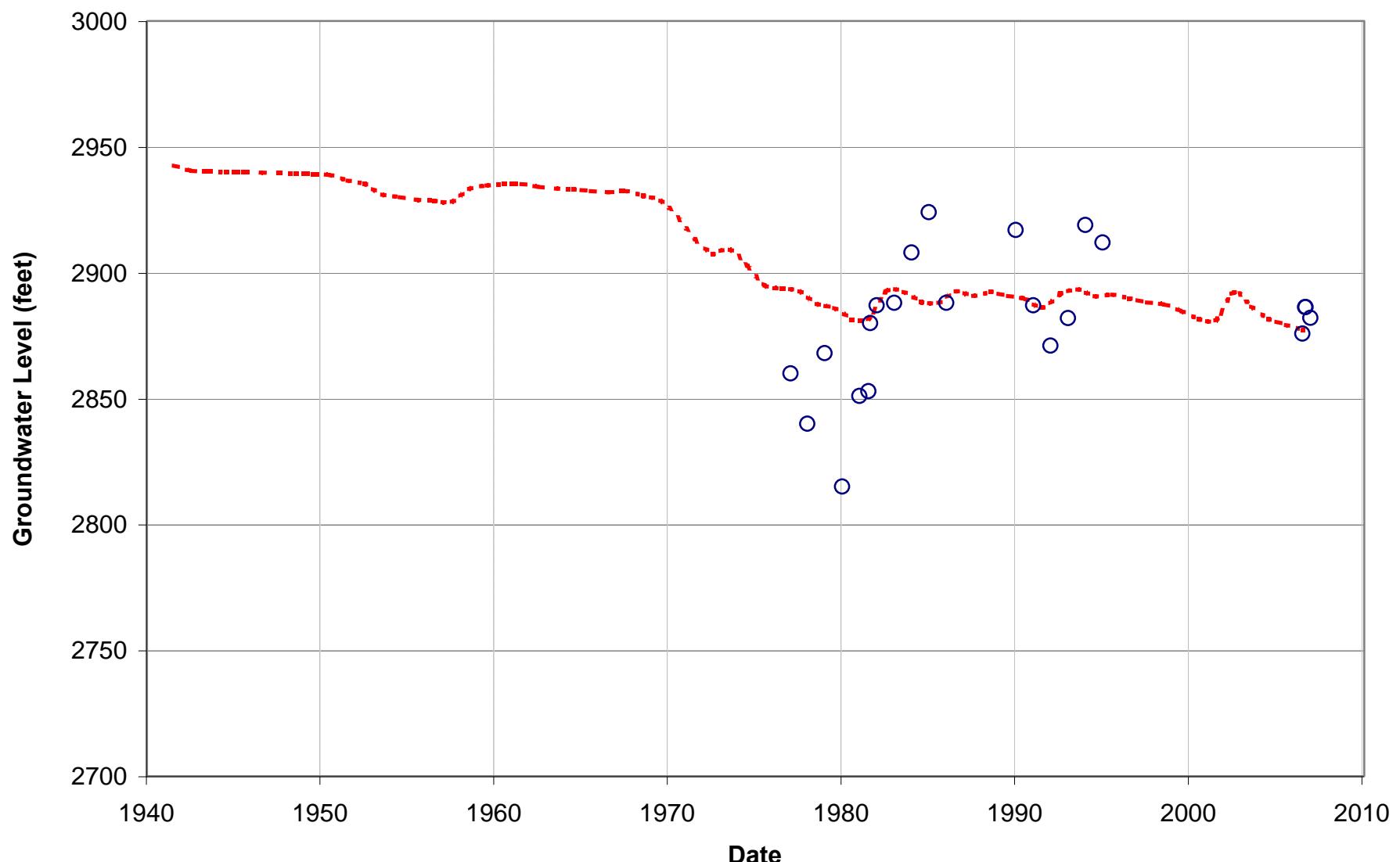


**Simulated and Measured  
Groundwater Levels at Well S-3**

APPROVED NWH DATE 11/20/2007

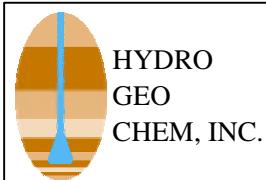
FIGURE

I.2.3



○ S-4 meas

- - - S-4 sim



**Simulated and Observed  
Groundwater Levels at Well S-4**

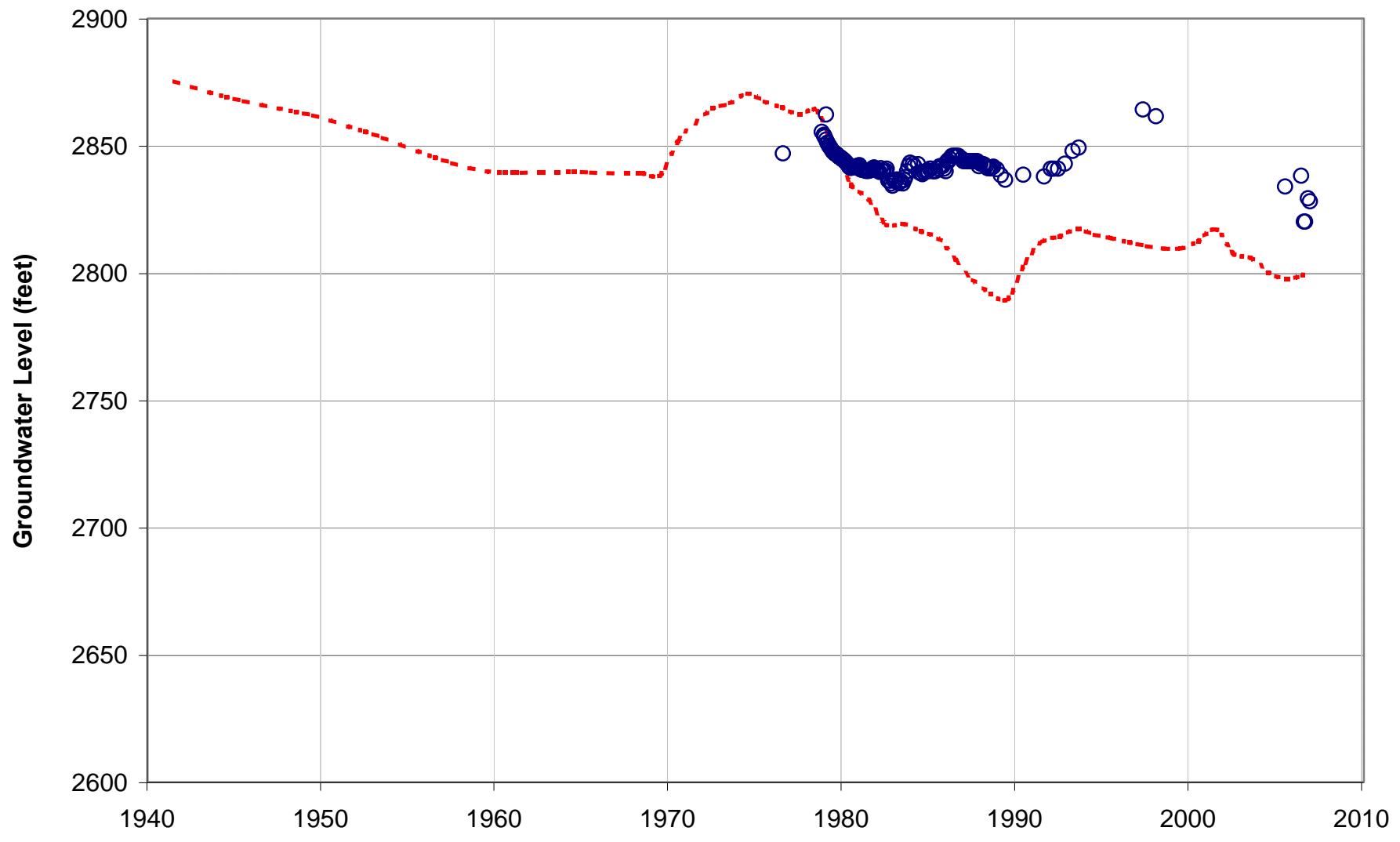
APPROVED

NWH

DATE 11/20/2007

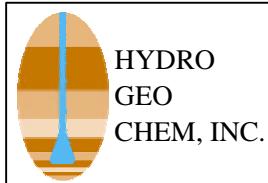
FIGURE

**I.2.4**



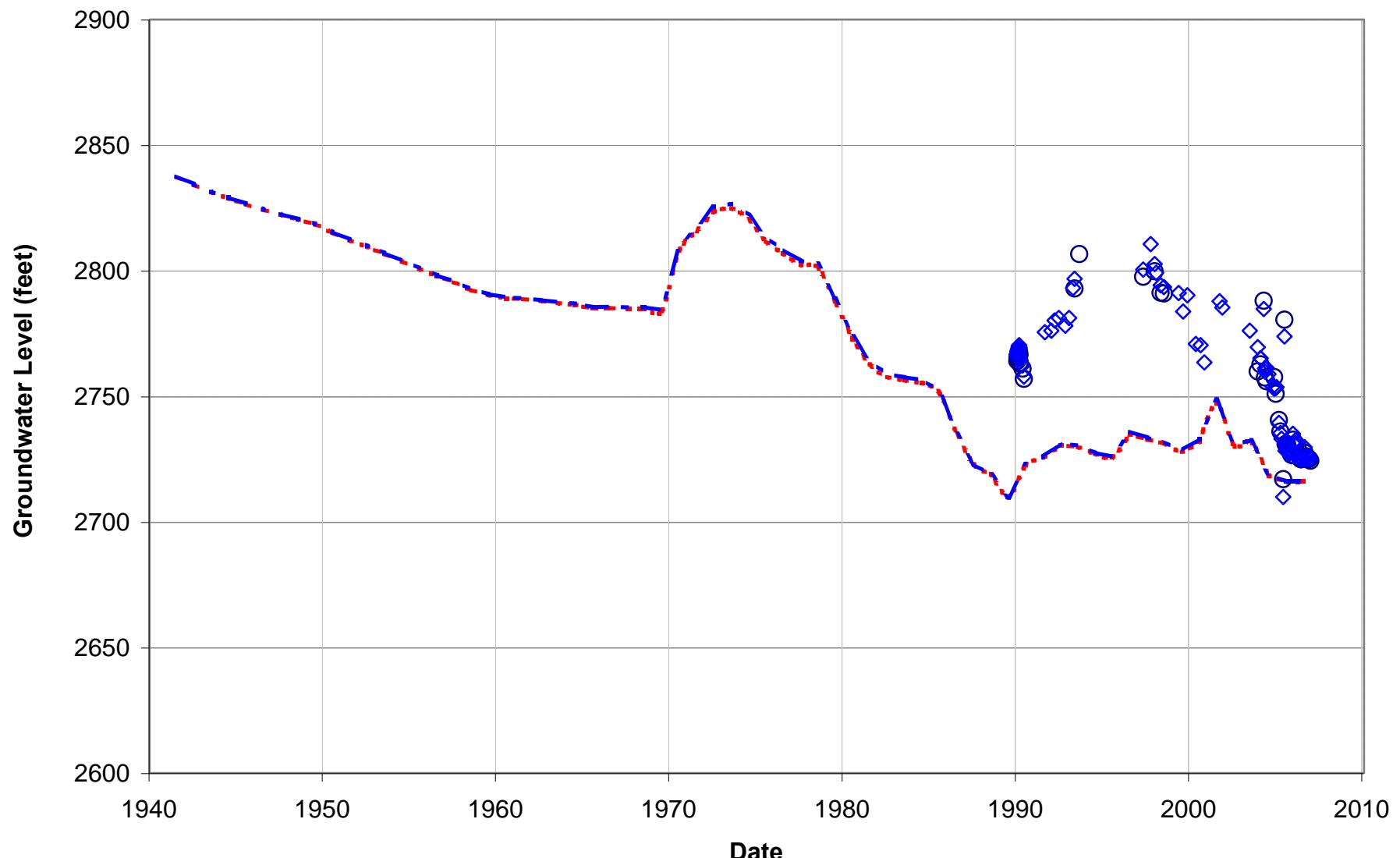
○ MH-10 meas

- - MH-10 sim



### Simulated and Measured Groundwater Levels at Well MH-10

APPROVED NWH DATE 11/20/2007 FIGURE I.2.5

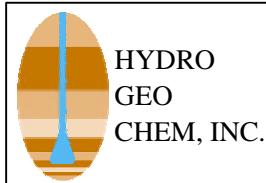


○ MH-15E meas

◇ MH-15W meas

- - MH-15E sim

- - MH-15W sim

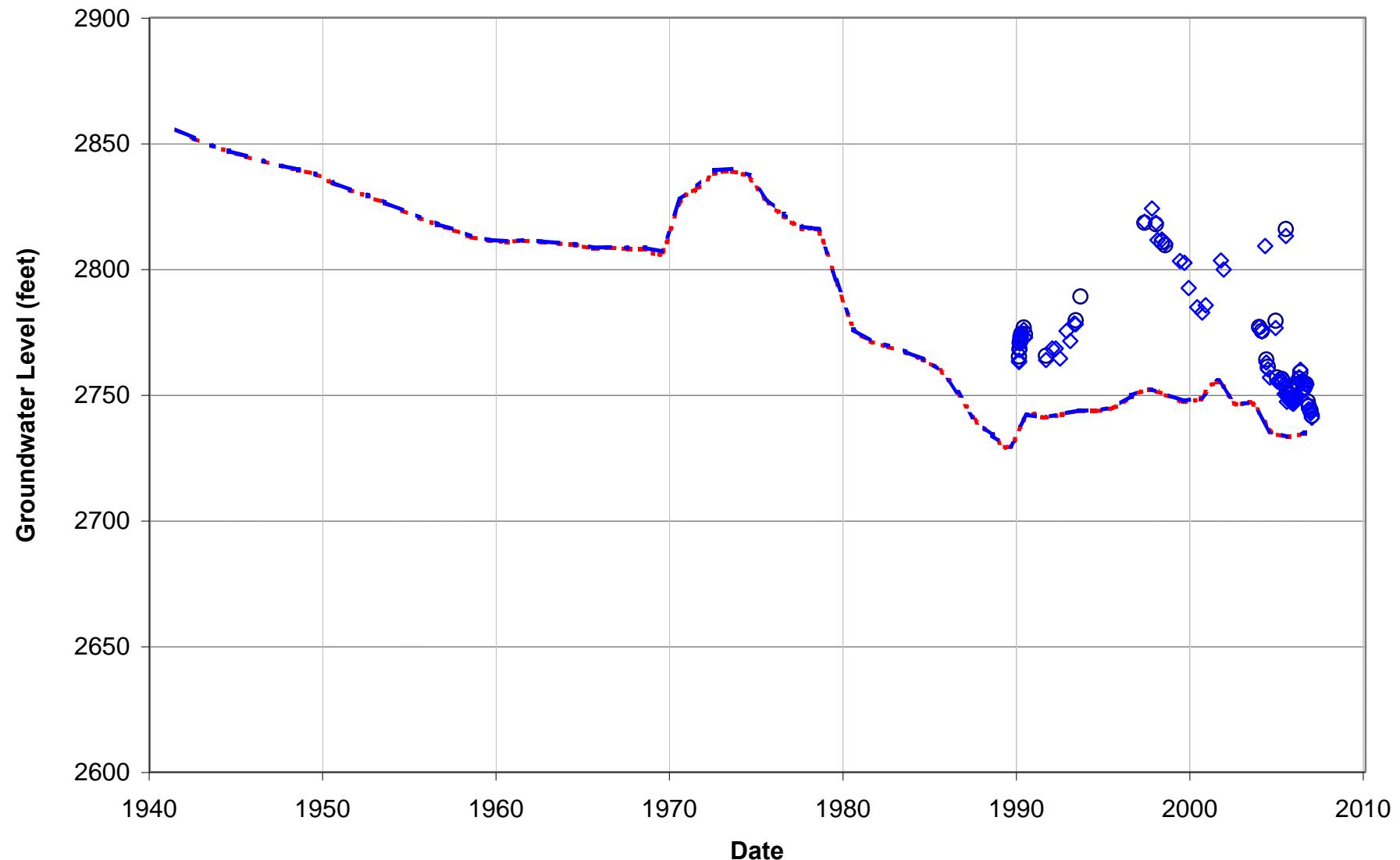


### Simulated and Measured Groundwater Levels at Wells MH-15E and MH-15W

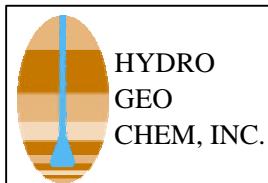
APPROVED NWH DATE 11/20/2007

FIGURE

I.2.6

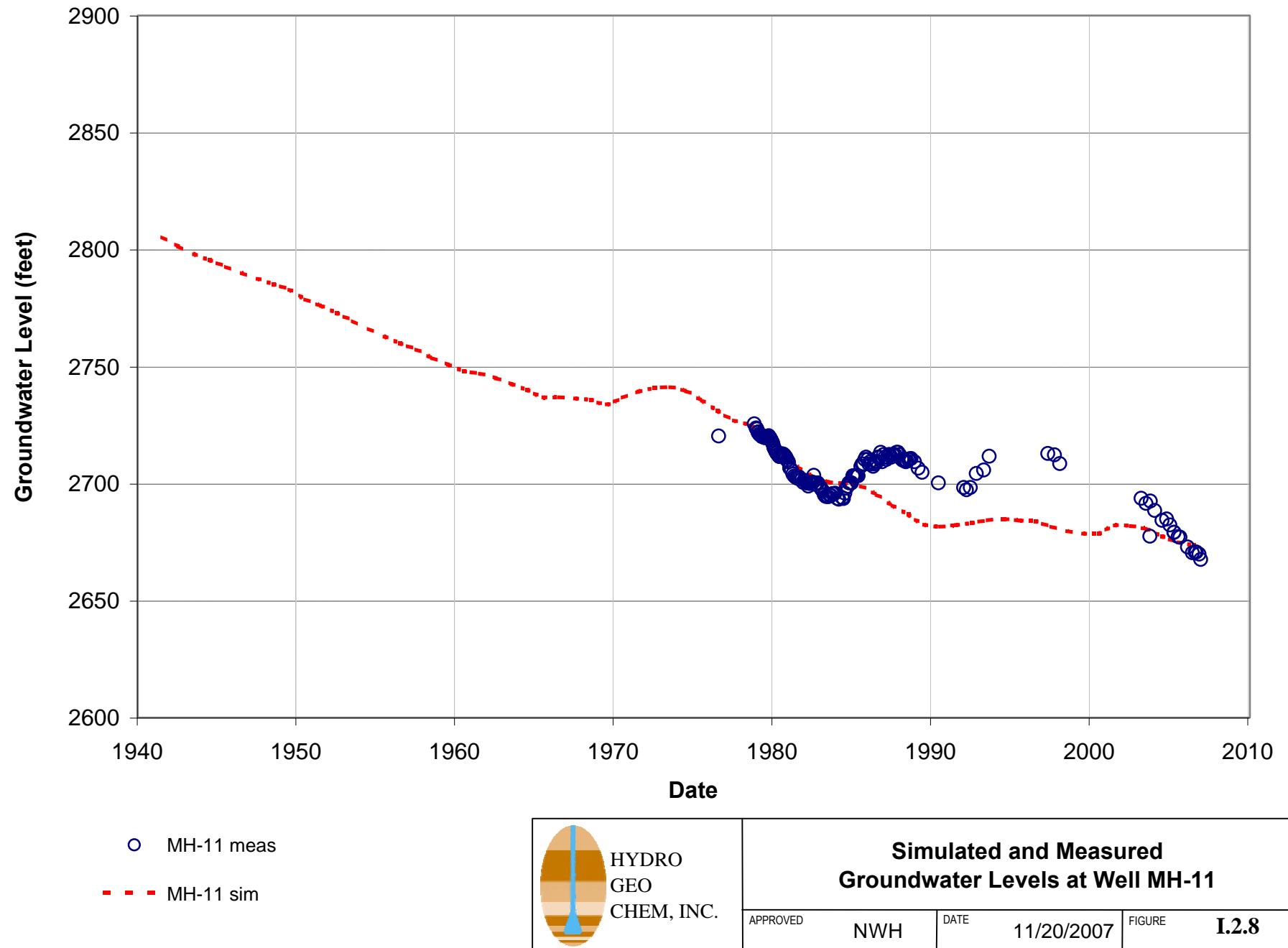


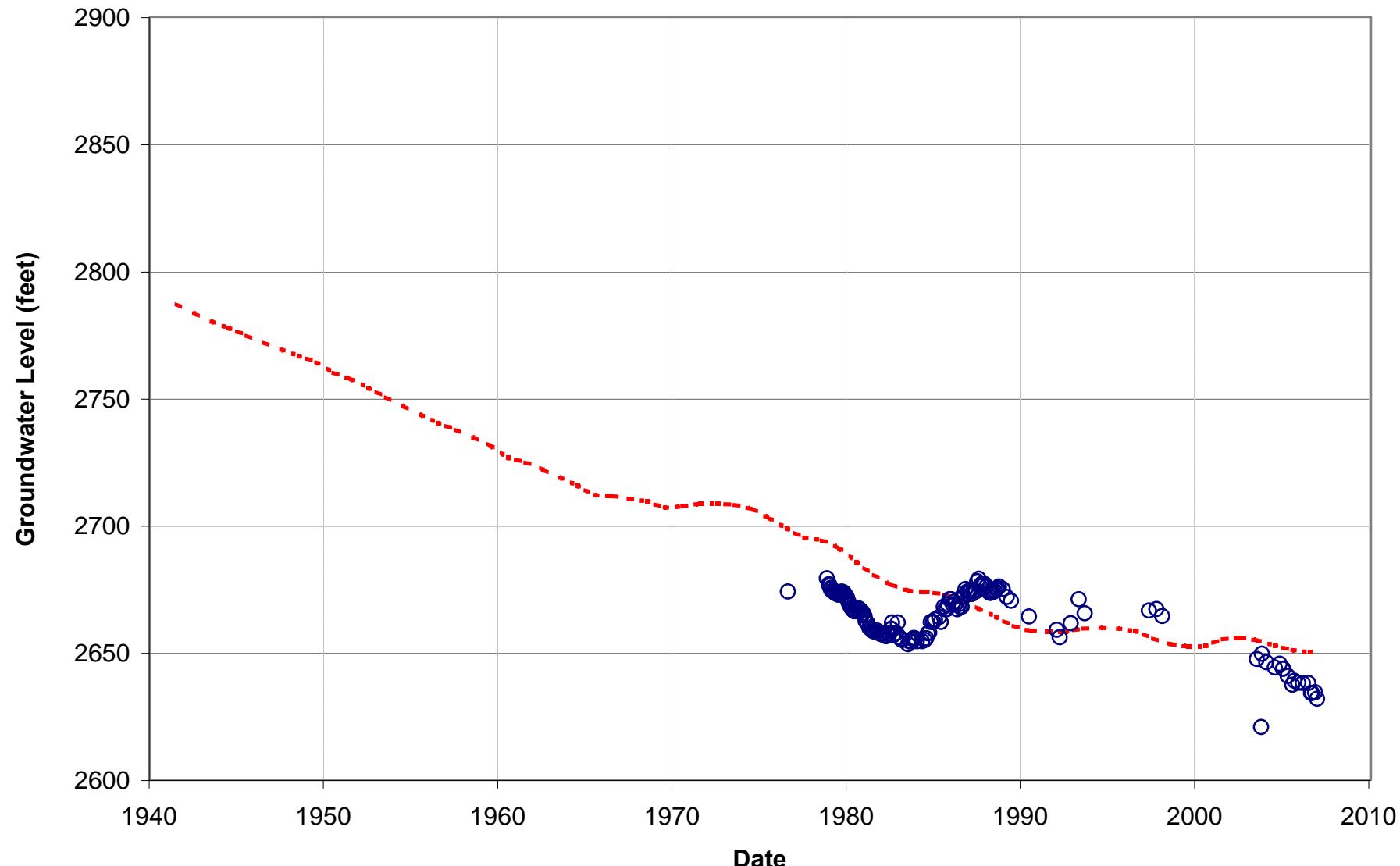
○ MH-16E meas      ◊ MH-16W meas  
- - - MH-16E sim      - - - MH-16W sim



### Simulated and Measured Groundwater Levels at Wells MH-16E and MH-16W

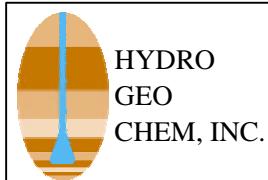
|          |     |      |            |        |       |
|----------|-----|------|------------|--------|-------|
| APPROVED | NWH | DATE | 11/20/2007 | FIGURE | I.2.7 |
|----------|-----|------|------------|--------|-------|





○ MH-12 meas

- - MH-12 sim

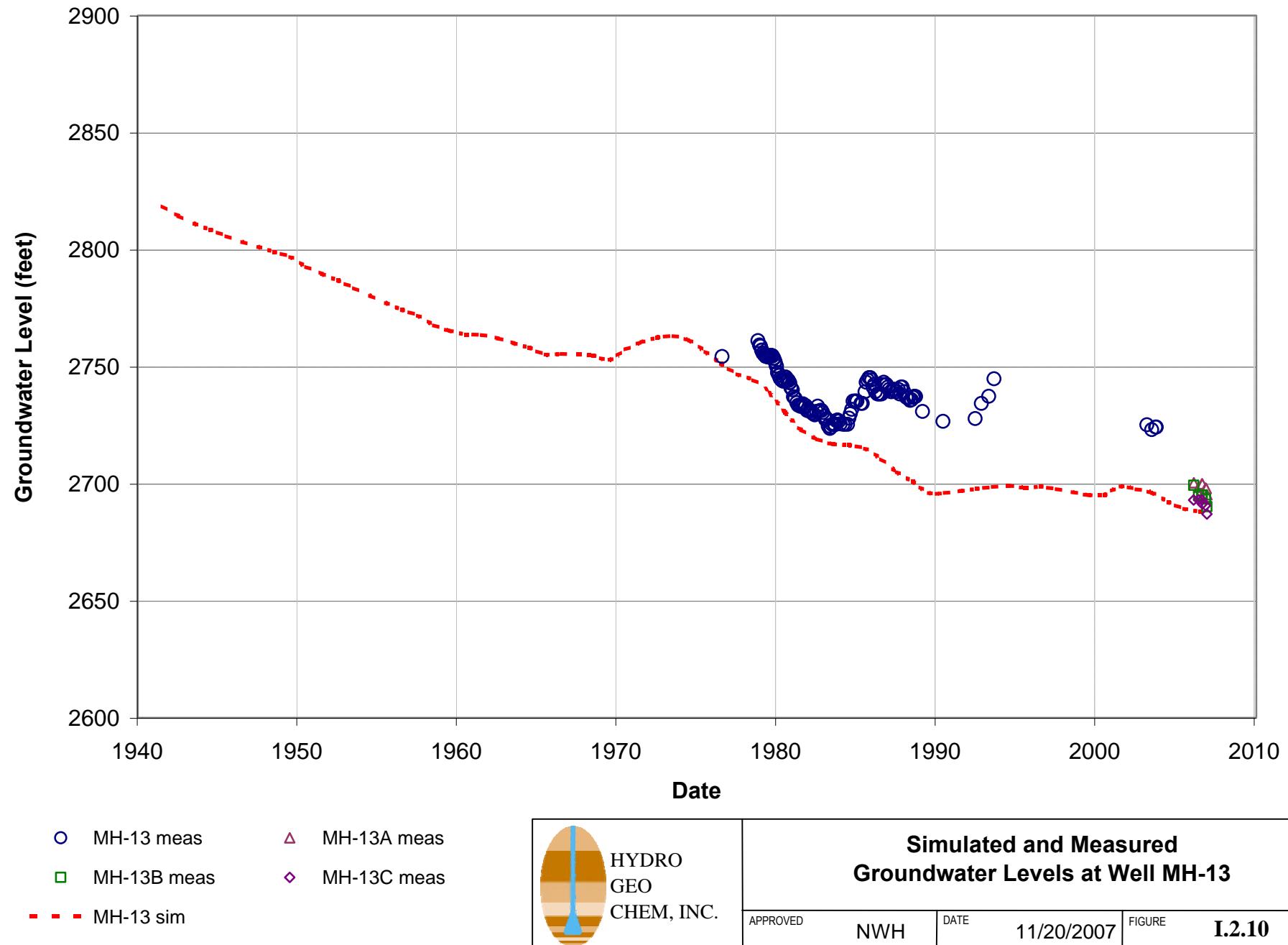


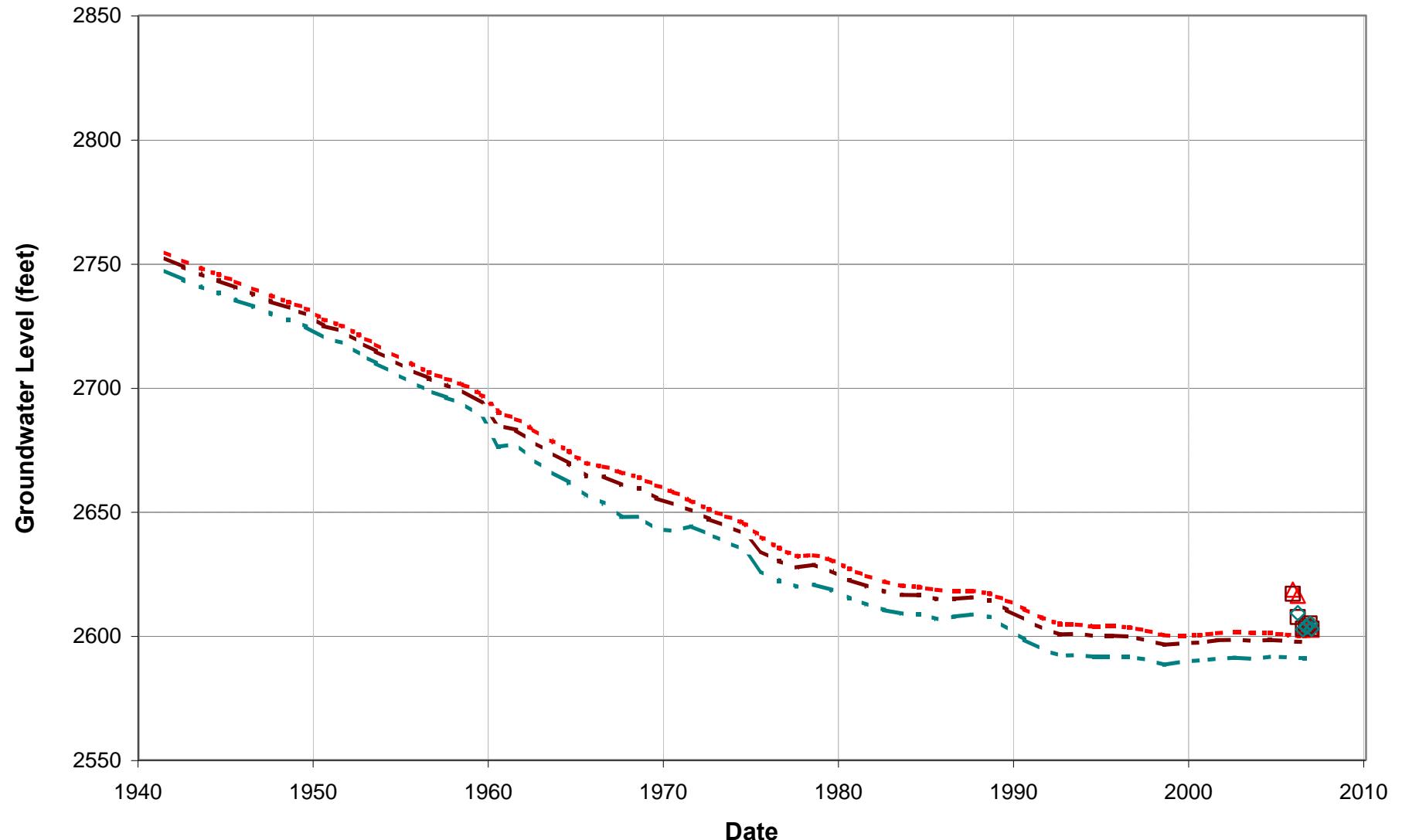
### Simulated and Measured Groundwater Levels at Well MH-12

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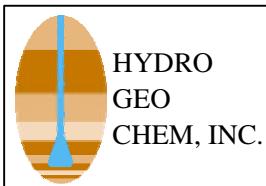
FIGURE

I.2.9



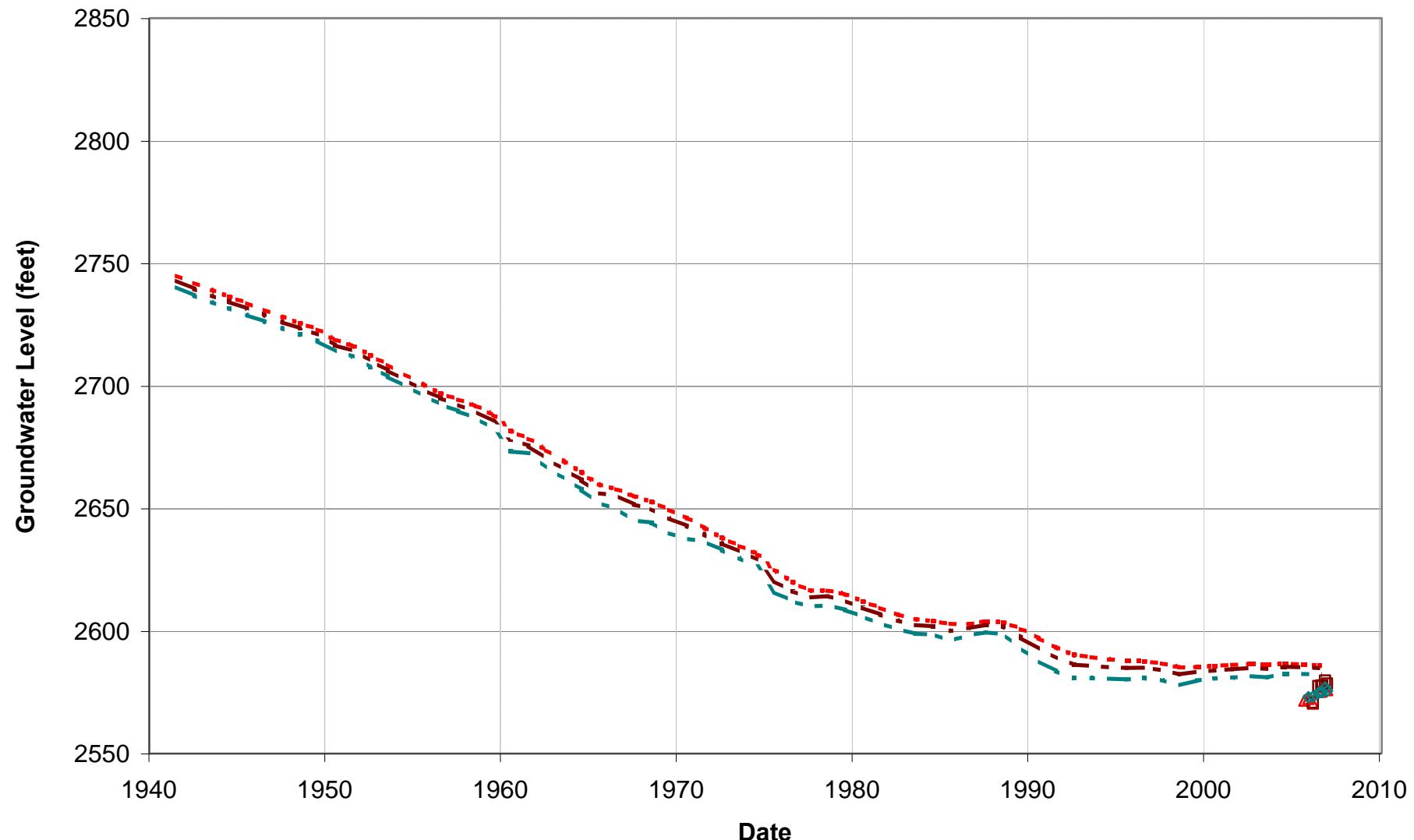


△ MH-25A meas      □ MH-25B meas  
◆ MH-25C meas      - - - MH-25A sim  
— MH-25B sim      — MH-25C sim

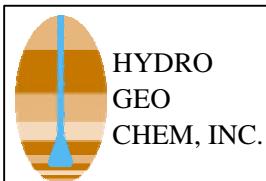


### Simulated and Measured Groundwater Levels at Well Nest MH-25

APPROVED      NWH      DATE      11/20/2007      FIGURE      I.2.11



▲ MH-26A meas      □ MH-26B meas  
 ◆ MH-26C meas      - - - MH-26A sim  
 — MH-26B sim      - - - MH-26C sim

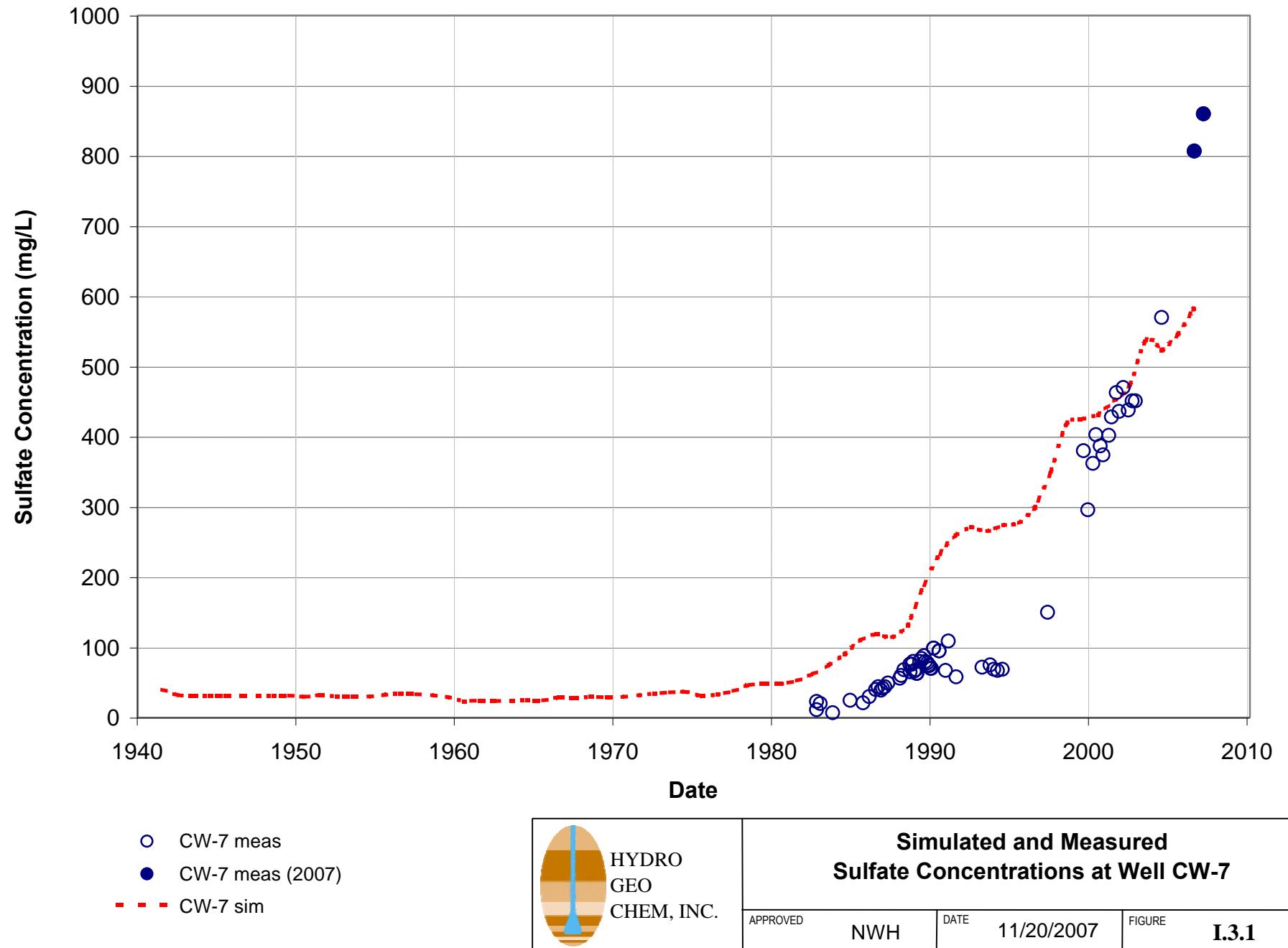


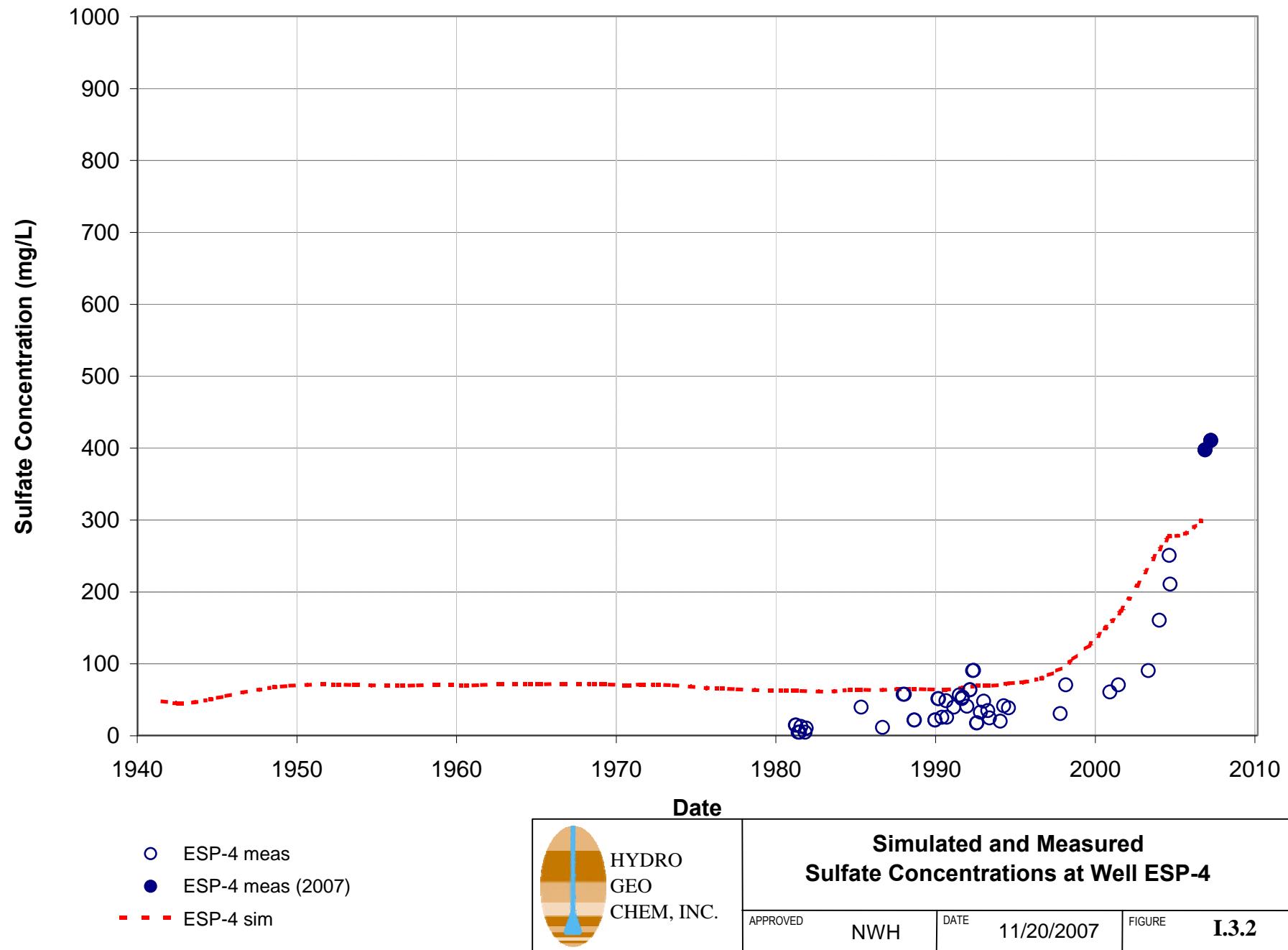
### Simulated and Measured Groundwater Levels at Well Nest MH-26

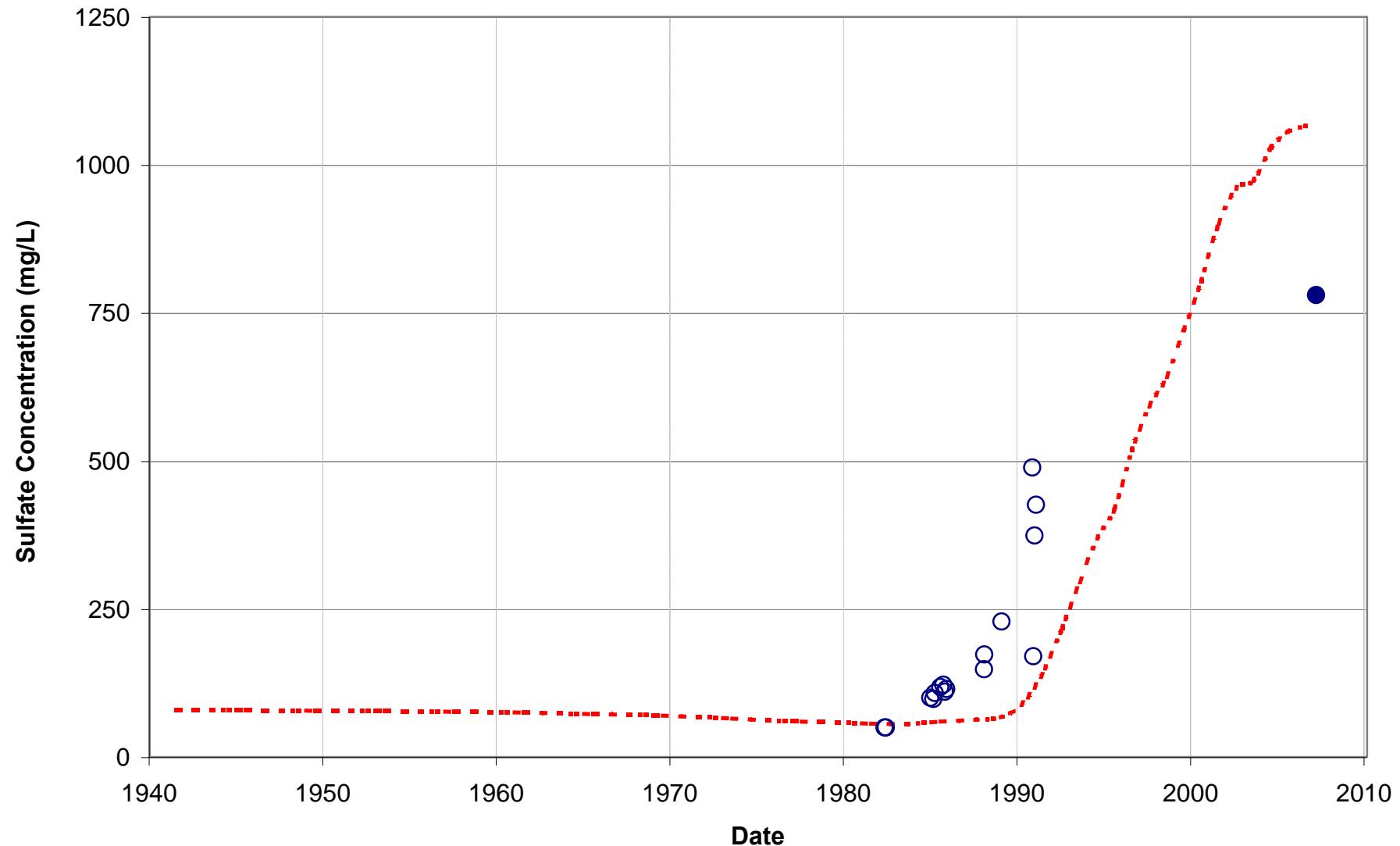
APPROVED NWH DATE 11/20/2007 FIGURE I.2.12

### **APPENDIX I.3**

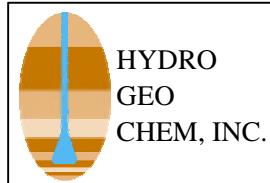
#### **MEASURED AND SIMULATED CHEMOGRAPHS AT SELECT WELLS**





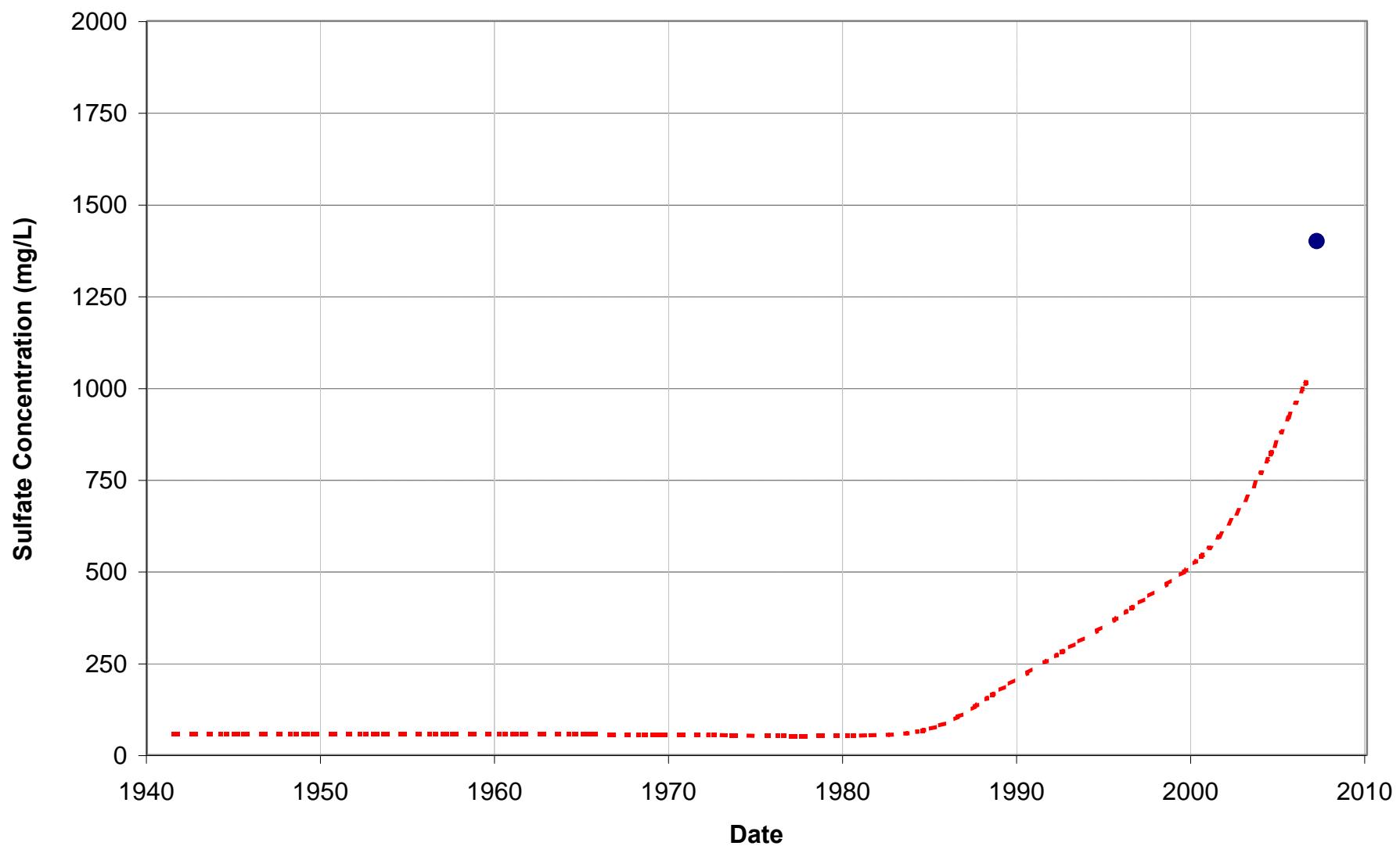


- I-12 meas
- I-12 meas (2007)
- - - I-12 sim



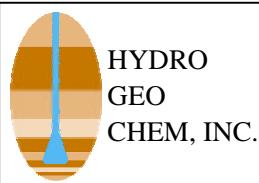
**Simulated and Measured  
Sulfate Concentrations at Well I-12**

APPROVED NWH DATE 11/20/2007 FIGURE I.3.3



● M-20 meas (2007)

- - - M-20 sim

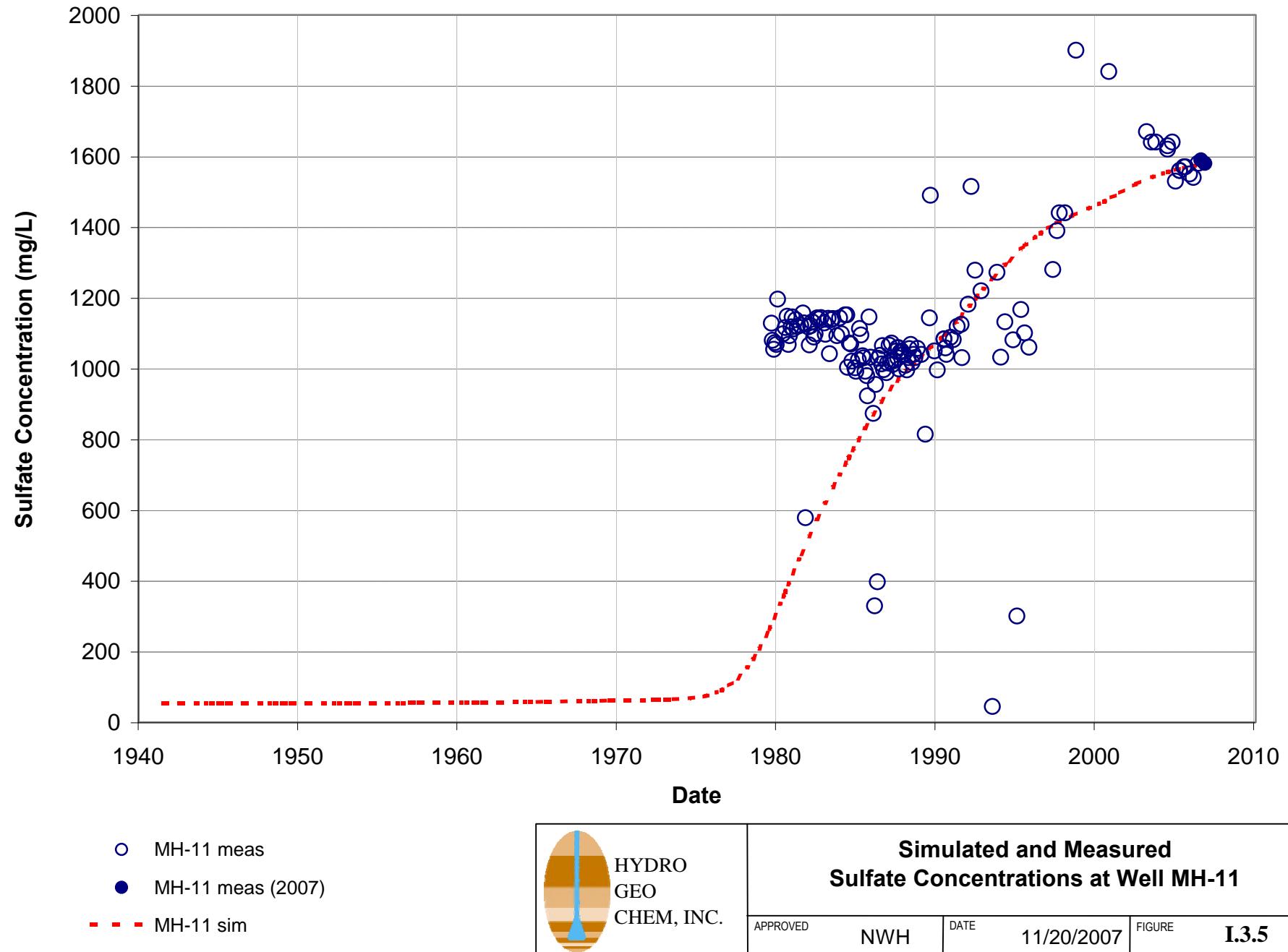


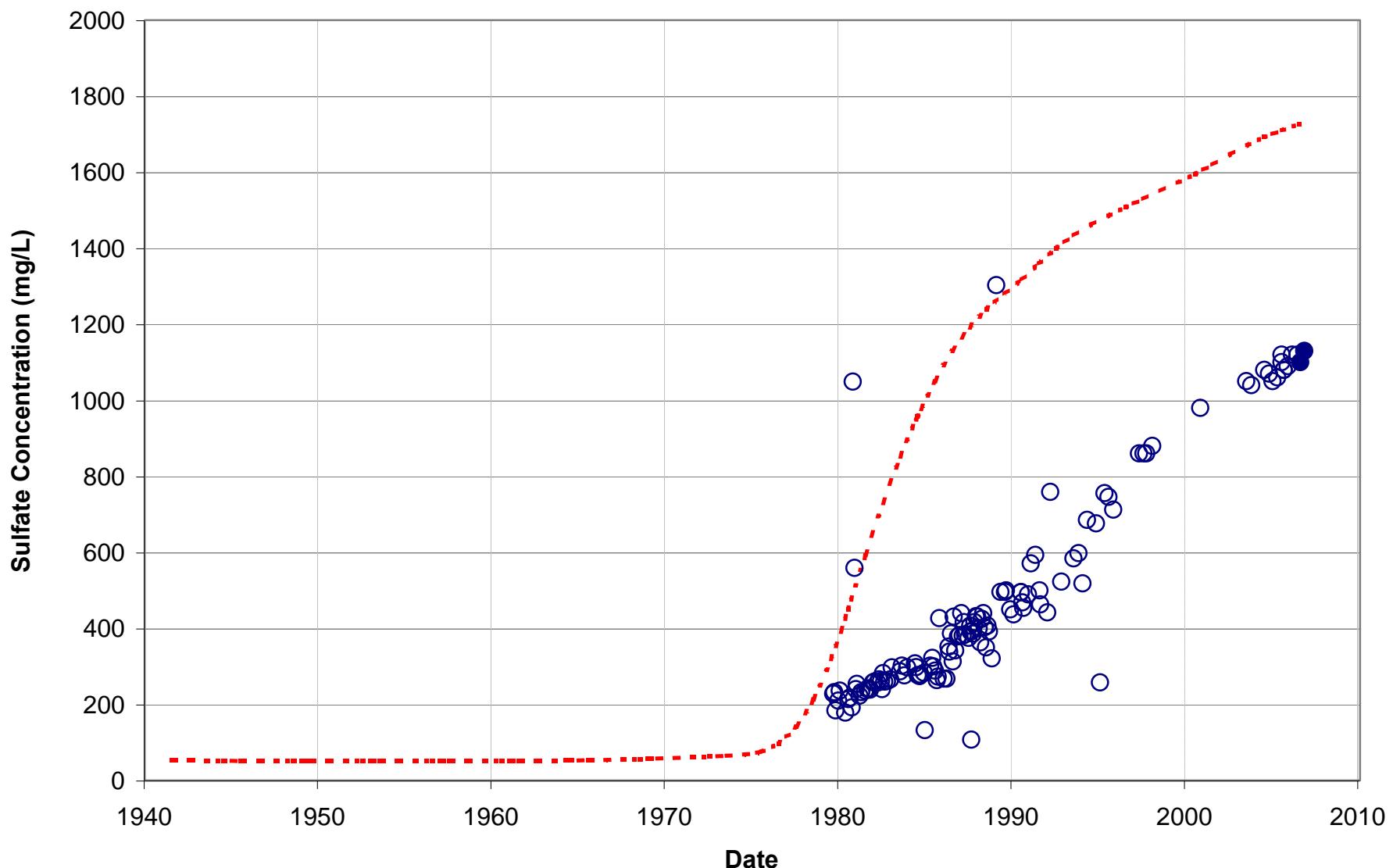
**Simulated and Measured  
Sulfate Concentrations at Well M-20**

APPROVED NWH DATE 11/20/2007

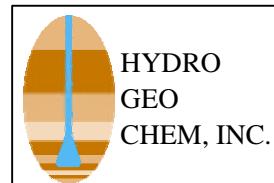
FIGURE

I.3.4





- MH-12 meas
- MH-12 meas (2007)
- - MH-12 sim



### Simulated and Measured Sulfate Concentrations at Well MH-12

APPROVED NWH DATE 11/20/2007 FIGURE

I.3.6

